

November, 2011

MODELLING AND SIMULATION OF LIQUID-VAPOR PHASE TRANSITION

A CONTRIBUTION TO THE STUDY OF THE BOILING CRISIS

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OUTLINE

1 Context

2 Model

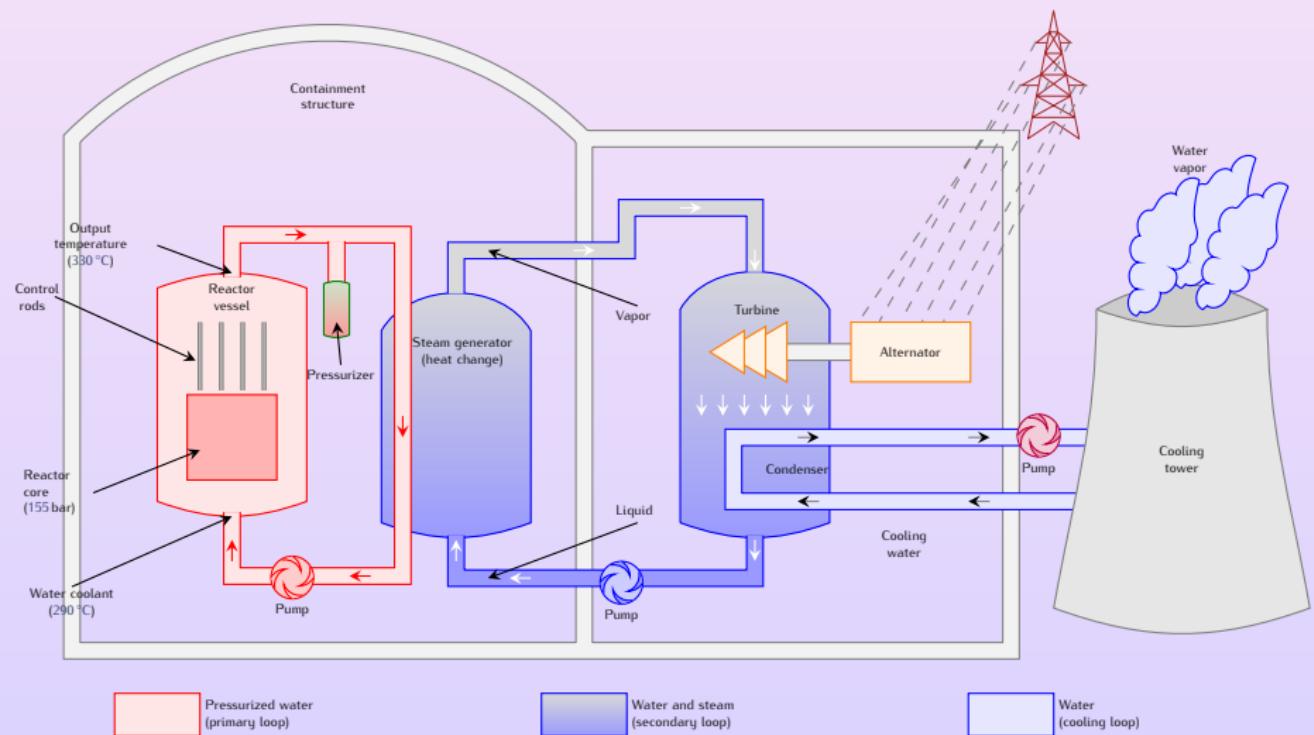
- Governing equations
- Equation of State

3 Numerical Approximation and Example

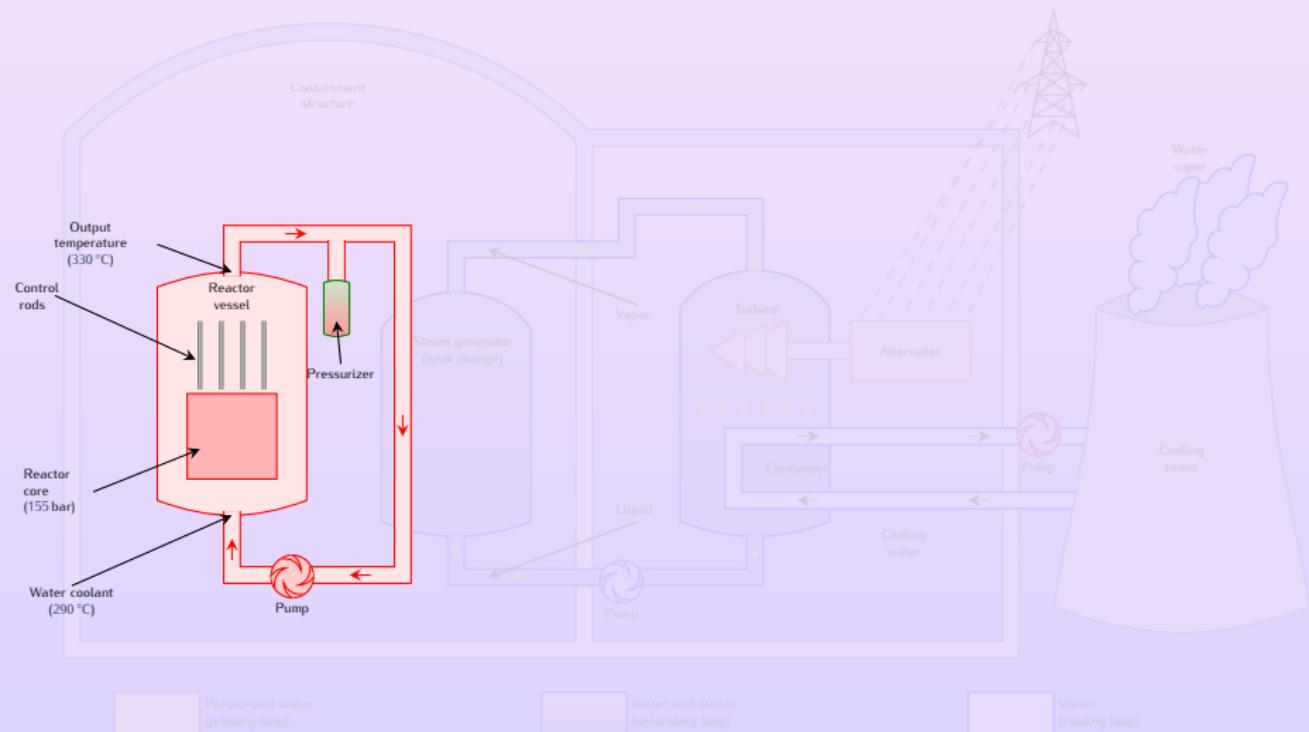
- Conservation Laws
- Numerical Scheme
- Numerical Example

4 Conclusion

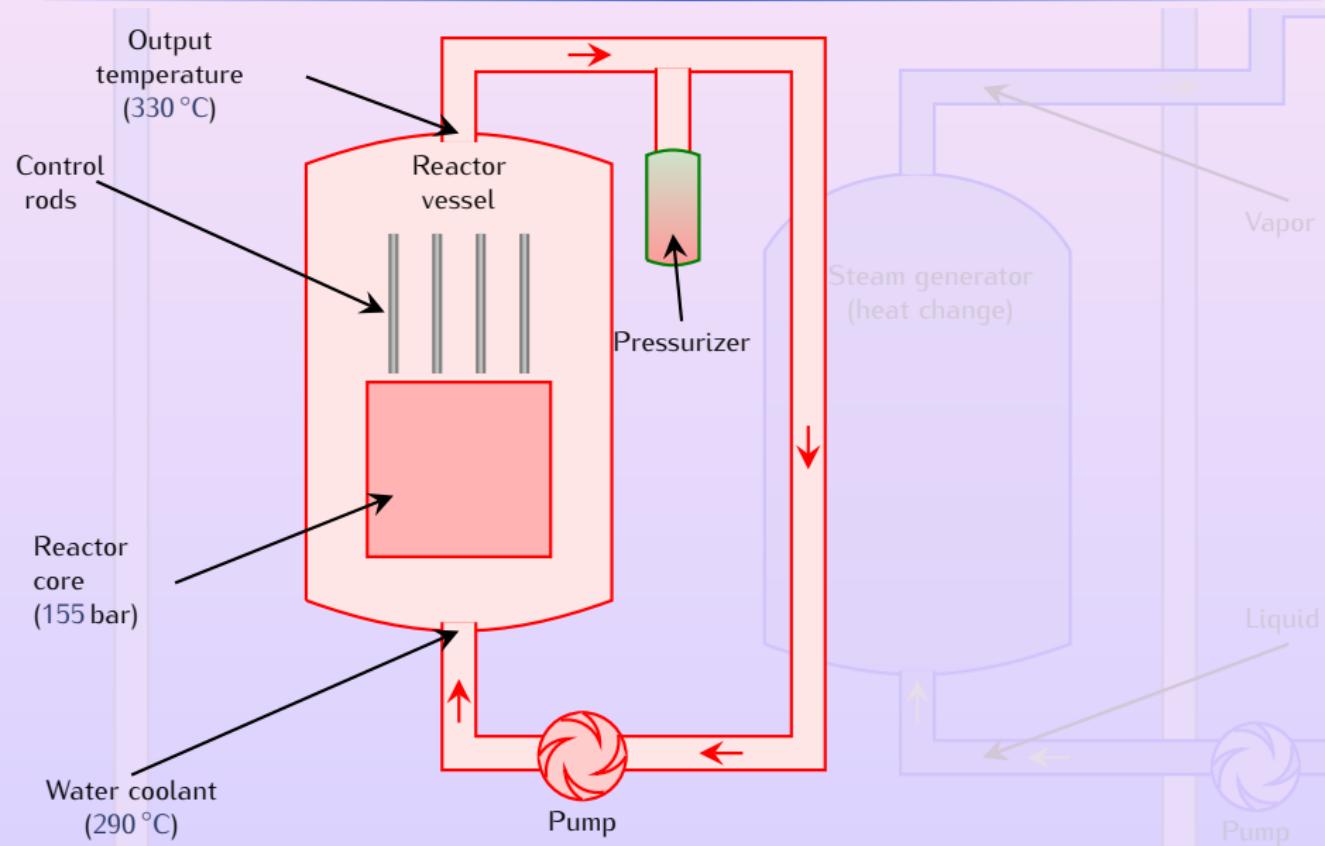
PRESSURIZED WATER REACTOR



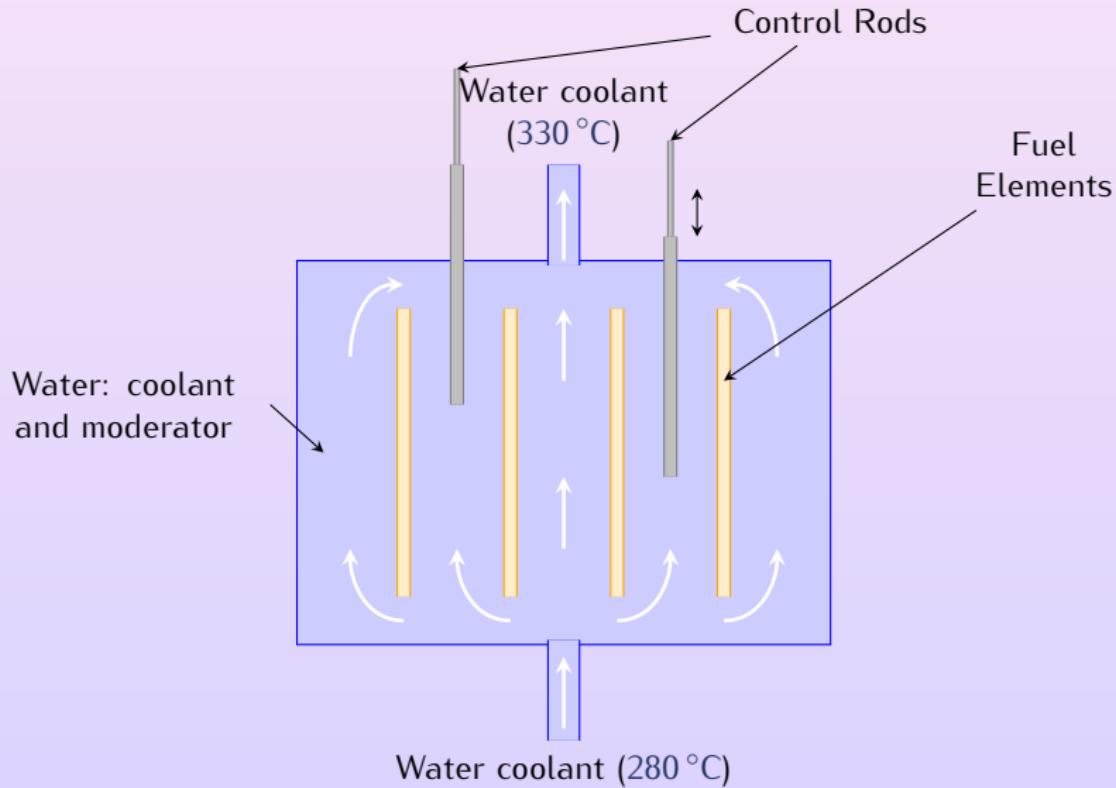
PRESSURIZED WATER REACTOR



PRESSURIZED WATER REACTOR



CORE OF A PRESSURIZED WATER REACTOR

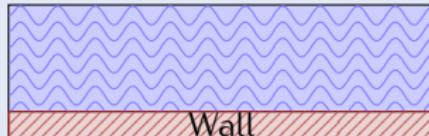


BOILING CRISIS

PHENOMENON

Liquid phase heated by a wall at a fixed temperature T^{wall} .

When T^{wall} increases, we switch from a **Nucleate Boiling** to a **Film Boiling**.

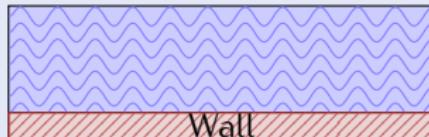


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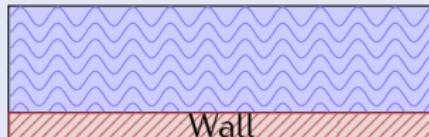
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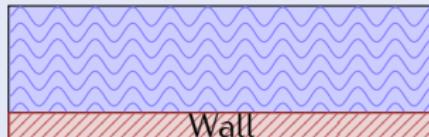
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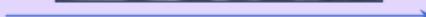
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Nucleate Boiling



Film Boiling

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“INGREDIENTS” OF THE MODEL

- Simulating all bubbles (no mixture),
- System of PDEs for the fluid flow (monophasic or diphasic),
- Phase transition (pressure and/or temperature variations),
- Heat Diffusion,
- Surface Tension,
- Gravity.

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EULER SYSTEM

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0, \\ \partial_t (\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = \mathfrak{V}_{\text{vf}} - \mathfrak{S}_{\text{sf}}, \\ \partial_t \left(\varrho \left(\frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \right) + \operatorname{div} \left(\varrho \left(\frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \mathbf{u} + P \mathbf{u} \right) = (\mathfrak{V}_{\text{vf}} - \mathfrak{S}_{\text{sf}}) \cdot \mathbf{u} - \operatorname{div}(q). \end{cases}$$

Unknowns:

- $(\mathbf{x}, t) \mapsto \varrho$ specific density,
- $(\mathbf{x}, t) \mapsto \varepsilon$ specific internal energy,
- $(\mathbf{x}, t) \mapsto \mathbf{u}$ velocity;

Source terms:

- $(\varrho, \varepsilon) \mapsto \mathfrak{V}_{\text{vf}}$ body forces,
- $(\varrho, \varepsilon) \mapsto \mathfrak{S}_{\text{sf}}$ surface forces,
- $(\varrho, \varepsilon) \mapsto \operatorname{div}(q)$ heat transfer.

EOS: $(\varrho, \varepsilon) \mapsto P$

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EOS OF EACH PHASE $\alpha = \text{liq}, \text{vap}$

$\tau = 1/\varrho$ specific volume

ε specific internal energy

$(\tau, \varepsilon) \mapsto s_\alpha$ specific entropy (Hessian matrix neg. def.);

$$\Downarrow \left\{ \begin{array}{ll} T_\alpha \stackrel{\text{def}}{=} \left(\frac{\partial s_\alpha}{\partial \varepsilon} \Big|_\tau \right)^{-1} > 0 & \text{temperature,} \\ P_\alpha \stackrel{\text{def}}{=} T_\alpha \frac{\partial s_\alpha}{\partial \tau} \Big|_\varepsilon > 0 & \text{pressure,} \\ g_\alpha \stackrel{\text{def}}{=} \varepsilon + P_\alpha \tau - T_\alpha s_\alpha & \text{free enthalpy (Gibbs potential),} \\ (c_\alpha)^2 \stackrel{\text{def}}{=} \tau^2 \left(P_\alpha \frac{\partial P_\alpha}{\partial \varepsilon} \Big|_\tau - \frac{\partial P_\alpha}{\partial \tau} \Big|_\varepsilon \right) & \text{speed of sound.} \end{array} \right.$$

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EXAMPLE: STIFFENED GAS

$$(\tau, \varepsilon) \mapsto s_\alpha = c_{v_\alpha} \ln(\varepsilon - q_\alpha - \pi_\alpha \tau) + c_{v_\alpha} (\gamma_\alpha - 1) \ln \tau + m_\alpha$$

$$T_\alpha = \frac{\varepsilon - q_\alpha - \pi_\alpha \tau}{c_{v_\alpha}},$$

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$$g_\alpha = q_\alpha + (\varepsilon - q_\alpha - \pi_\alpha \tau) \left(\gamma_\alpha - \frac{m_\alpha}{c_{v_\alpha}} - \ln \left((\varepsilon - q_\alpha - \pi_\alpha \tau) \tau^{(\gamma_\alpha - 1)} \right) \right),$$

$$c_\alpha^2 = \gamma_\alpha (\gamma_\alpha - 1) (\varepsilon - q_\alpha - \pi_\alpha \tau) = \gamma_\alpha (P_\alpha + \pi_\alpha) \tau = \gamma_\alpha (\gamma_\alpha - 1) c_{v_\alpha} T_\alpha > 0.$$

Phase	c_v [J kg ⁻¹ K ⁻¹]	γ	π [Pa]	q [J kg ⁻¹]	m [J kg ⁻¹ K ⁻¹]
Liquid	1816.2	2.35	10^9	-1167.056×10^3	-32765.55596
Vapor	1040.14	1.43	0	2030.255×10^3	-33265.65947

Table: Parameters proposed by [O. LE METAYER] for water and steam: $\gamma > 1$ adiabatic coefficient, π molecular attraction, q binding energy.

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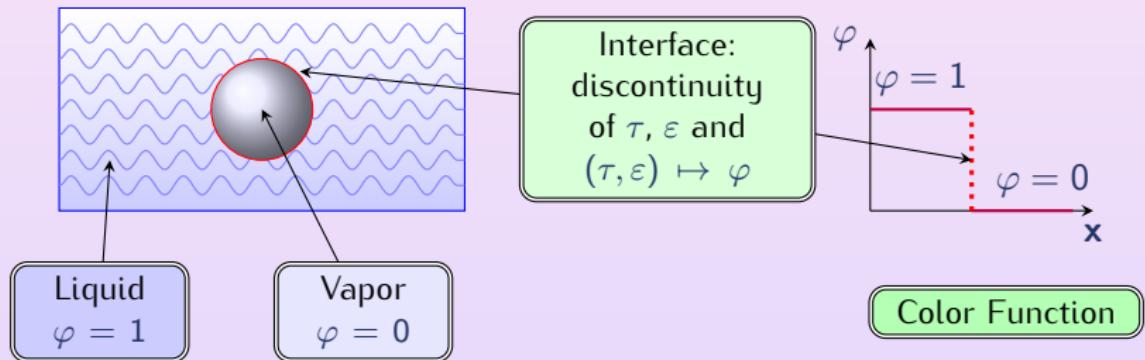
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LIQUID-VAPOR INTERFACE



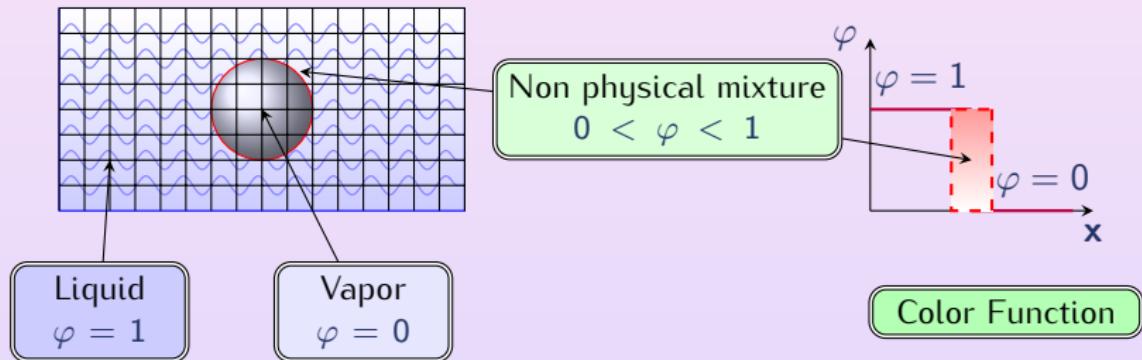
$$(\tau, \varepsilon) \mapsto s = \begin{cases} s^{\text{liq}} & \text{if } \varphi = 1; \\ s^{\text{vap}} & \text{if } \varphi = 0. \end{cases} \implies (\tau, \varepsilon) \mapsto P = \begin{cases} P^{\text{liq}} & \text{if } \varphi = 1; \\ P^{\text{vap}} & \text{if } \varphi = 0. \end{cases}$$

► Goal ①: define $(\tau, \varepsilon) \mapsto \varphi$ for physical values of (τ, ε)

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► Goal ③: define $(\tau, \varepsilon) \mapsto s$

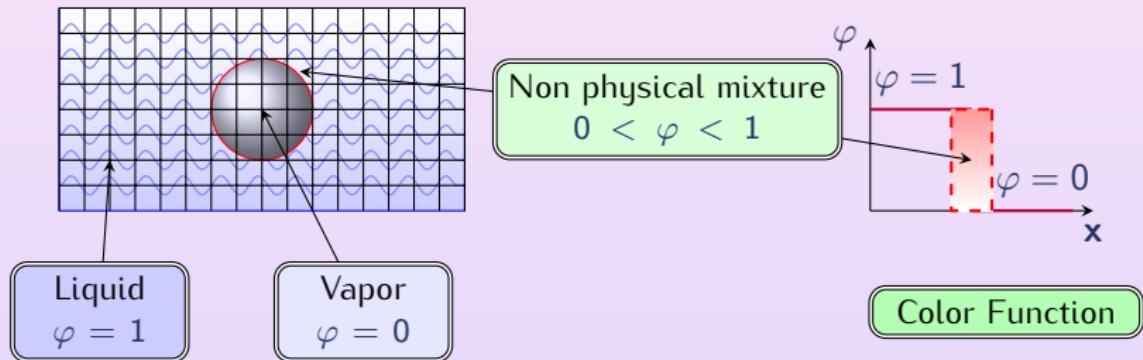
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EOS OF A MIXTURE

- y mass fraction

- $\begin{cases} \tau \stackrel{\text{def}}{=} y\tau_{\text{liq}} + (1-y)\tau_{\text{vap}} \\ \varepsilon \stackrel{\text{def}}{=} y\varepsilon_{\text{liq}} + (1-y)\varepsilon_{\text{vap}} \end{cases}$

- z volume fraction s.t. $y\tau_{\text{liq}} = z\tau$

- ψ energy fraction s.t. $y\varepsilon_{\text{liq}} = \psi\varepsilon$

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ENTROPY WITHOUT PHASE CHANGE

$$\begin{aligned} \sigma &\stackrel{\text{def}}{=} y s_{\text{liq}}(\tau_{\text{liq}}, \varepsilon_{\text{liq}}) + (1-y)s_{\text{vap}}(\tau_{\text{vap}}, \varepsilon_{\text{vap}}) \\ &= y s_{\text{liq}}\left(\frac{z}{y}\tau, \frac{\psi}{y}\varepsilon\right) + (1-y)s_{\text{vap}}\left(\frac{1-z}{1-y}\tau, \frac{1-\psi}{1-y}\varepsilon\right) \\ P &= \left(\frac{\partial \sigma}{\partial \varepsilon}\Bigg|_{\tau,y,z,\psi}\right)^{-1} \frac{\partial \sigma}{\partial \tau}\Bigg|_{\varepsilon;y,z,\psi} \end{aligned}$$

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EOS OF PHASE CHANGE

ENTROPY AT EQUILIBRIUM

$$(\tau, \varepsilon) \mapsto s^{\text{eq}}(\tau, \varepsilon) = \sigma(\tau, \varepsilon, z^{\text{eq}}(\tau, \varepsilon), y^{\text{eq}}(\tau, \varepsilon), \psi^{\text{eq}}(\tau, \varepsilon))$$

DEFINITION [H. CALLEN, PH. HELLUY ...]

Optimization Problem:

$$s^{\text{eq}}(\tau, \varepsilon) \stackrel{\text{def}}{=} \max_{z, y, \psi \in [0, 1]^3} \sigma(\tau, \varepsilon, z, y, \psi)$$

Optimality Condition: $\begin{cases} T_{\text{liq}}(z, y, \psi) = T_{\text{vap}}(z, y, \psi) \\ P_{\text{liq}}(z, y, \psi) = P_{\text{vap}}(z, y, \psi) \\ g_{\text{liq}}(z, y, \psi) = g_{\text{vap}}(z, y, \psi) \end{cases}$

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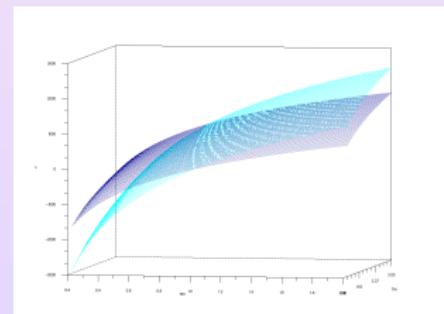
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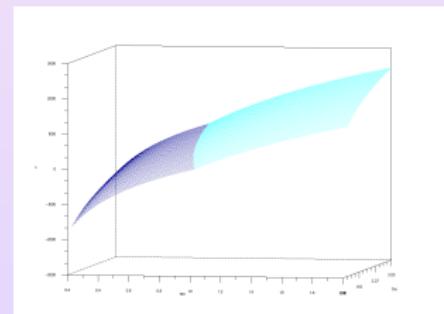
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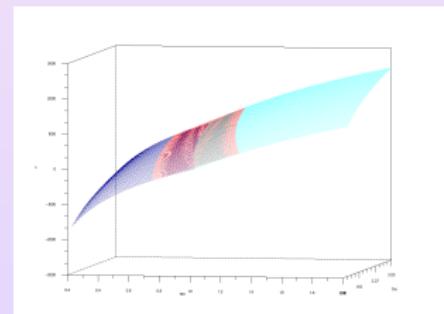
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EOS OF PHASE CHANGE

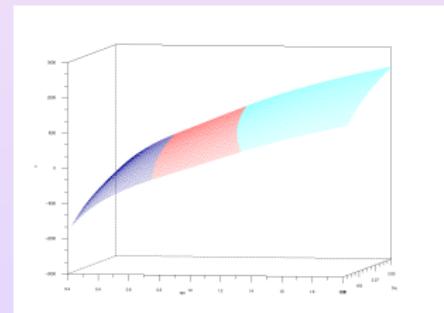
ENTROPY AT EQUILIBRIUM

$$(\tau, \varepsilon) \mapsto s^{\text{eq}}(\tau, \varepsilon) = \sigma(\tau, \varepsilon, z^{\text{eq}}(\tau, \varepsilon), y^{\text{eq}}(\tau, \varepsilon), \psi^{\text{eq}}(\tau, \varepsilon))$$

DEFINITION [H. CALLEN, PH. HELLUY ...]

Optimization Problem:

$$\begin{aligned} s^{\text{eq}}(\tau, \varepsilon) &\stackrel{\text{def}}{=} \max_{z, y, \psi \in [0, 1]^3} \sigma(\tau, \varepsilon, z, y, \psi) \\ &= \text{co} \left\{ \max \left\{ s_{\text{liq}}(\tau, \varepsilon), s_{\text{vap}}(\tau, \varepsilon) \right\} \right\} \end{aligned}$$



Optimality Condition: $\begin{cases} T_{\text{liq}}(z, y, \psi) = T_{\text{vap}}(z, y, \psi) \\ P_{\text{liq}}(z, y, \psi) = P_{\text{vap}}(z, y, \psi) \\ g_{\text{liq}}(z, y, \psi) = g_{\text{vap}}(z, y, \psi) \end{cases}$

ANALYTICAL EOS

(τ, ε) fixed

$(\tau_{\text{liq}}, \varepsilon_{\text{liq}}, \tau_{\text{vap}}, \varepsilon_{\text{vap}}, y)$ SOLUTION OF

$$\begin{cases} P_{\text{liq}}(\tau_{\text{liq}}, \varepsilon_{\text{liq}}) = P_{\text{vap}}(\tau_{\text{vap}}, \varepsilon_{\text{vap}}) \\ T_{\text{liq}}(\tau_{\text{liq}}, \varepsilon_{\text{liq}}) = T_{\text{vap}}(\tau_{\text{vap}}, \varepsilon_{\text{vap}}) \\ g_{\text{liq}}(\tau_{\text{liq}}, \varepsilon_{\text{liq}}) = g_{\text{vap}}(\tau_{\text{vap}}, \varepsilon_{\text{vap}}) \\ \tau = y\tau_{\text{liq}} + (1-y)\tau_{\text{vap}} \\ \varepsilon = y\varepsilon_{\text{liq}} + (1-y)\varepsilon_{\text{vap}} \end{cases}$$

(P, T) SOLUTION OF

$$\begin{cases} \tau_\alpha = \tau_\alpha(P, T) \\ \varepsilon_\alpha = \varepsilon_\alpha(P, T) \\ g_{\text{liq}}(P, T) = g_{\text{vap}}(P, T) \\ y = \frac{\tau - \tau_{\text{vap}}(P, T)}{\tau_{\text{liq}}(P, T) - \tau_{\text{vap}}(P, T)} = \frac{\varepsilon - \varepsilon_{\text{vap}}(P, T)}{\varepsilon_{\text{liq}}(P, T) - \varepsilon_{\text{vap}}(P, T)} \end{cases}$$

$T \mapsto P = P^{\text{sat}}(T)$

T SOLUTION OF

$$\frac{\tau - \tau_{\text{vap}}^{\text{sat}}(T)}{\tau_{\text{liq}}^{\text{sat}}(T) - \tau_{\text{vap}}^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_{\text{vap}}^{\text{sat}}(T)}{\varepsilon_{\text{liq}}^{\text{sat}}(T) - \varepsilon_{\text{vap}}^{\text{sat}}(T)} \quad \text{where } \left(\begin{matrix} \tau \\ \varepsilon \end{matrix}\right)_\alpha^{\text{sat}}(T) \stackrel{\text{def}}{=} \left(\begin{matrix} \tau \\ \varepsilon \end{matrix}\right)_\alpha(P^{\text{sat}}(T), T)$$

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SPEED OF SOUND

Theorem

If $\tau_{\text{liq}}^* \neq \tau_{\text{vap}}^*$ and $\varepsilon_{\text{liq}}^* \neq \varepsilon_{\text{vap}}^*$ (first order phase transition) then $c^{\text{eq}}(\tau, \varepsilon) > 0$.

$$(c^{\text{eq}})^2 \stackrel{\text{def}}{=} \tau^2 \left(P^{\text{eq}} \frac{\partial P^{\text{eq}}}{\partial \varepsilon} \Big|_\tau - \frac{\partial P^{\text{eq}}}{\partial \tau} \Big|_\varepsilon \right) = \begin{matrix} \circlearrowleft \\ \nabla \end{matrix} \boxed{P^{\text{eq}}, -1} \begin{bmatrix} S_{\varepsilon\varepsilon}^{\text{eq}} & S_{T\varepsilon}^{\text{eq}} \\ S_{T\varepsilon}^{\text{eq}} & S_{TT}^{\text{eq}} \end{bmatrix} \boxed{\begin{bmatrix} P^{\text{eq}} \\ -1 \end{bmatrix}} \leq 0$$

HESSIAN MATRIX OF $(\tau, \varepsilon) \mapsto s^{\text{eq}}$

- for all (τ, ε) pure phase state

$$\mathbf{v}^T d^2 s^{\text{eq}}(\tau, \varepsilon) \mathbf{v} < 0 \quad \forall \mathbf{v} \neq 0,$$

- for all (τ, ε) equilibrium mixture state

$$\exists \mathbf{v}(\tau, \varepsilon) \neq \mathbf{0} \text{ s.t. } \mathbf{v}^T d^2 s^{\text{eq}}(\tau, \varepsilon) \mathbf{v} = 0.$$

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$$\forall (\tau, \varepsilon) \text{ equilibrium mixture state, } \mathbf{v}(\tau, \varepsilon) \stackrel{?}{\equiv} [P^{\text{eq}}(\tau, \varepsilon), -1]$$

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$\forall (\tau, \varepsilon) \text{ equilibrium mixture state, } \mathbf{v}(\tau, \varepsilon) \stackrel{?}{\not\propto} [P^{\text{eq}}(\tau, \varepsilon), -1]$

OUTLINE

1 Context

2 Model

- Governing equations
- Equation of State

3 Numerical Approximation and Example

- Conservation Laws
- Numerical Scheme
- Numerical Example

4 Conclusion

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DYNAMIC LIQUID-VAPOR PHASE CHANGE

EULER SYSTEM

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0, \\ \partial_t (\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t \left(\varrho \left(\frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \right) + \operatorname{div} \left(\varrho \left(\frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \mathbf{u} + P^{\text{eq}} \mathbf{u} \right) = 0 \end{cases} \quad \text{with } P^{\text{eq}} \stackrel{\text{def}}{=} \frac{s_{\tau}^{\text{eq}}}{s_{\varepsilon}^{\text{eq}}}.$$

MATHEMATICAL PROPERTIES

If $\tau_{\text{liq}}^* \neq \tau_{\text{vap}}^*$ and $\varepsilon_{\text{liq}}^* \neq \varepsilon_{\text{vap}}^*$ (first order phase transition) then

- The Euler system is a hyperbolic 3x3 system.

- The eigenvalues are constant along the characteristic curves, which are parabolas.

DYNAMIC LIQUID-VAPOR PHASE CHANGE

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MATHEMATICAL PROPERTIES

If $\tau_{\text{liq}}^* \neq \tau_{\text{vap}}^*$ and $\varepsilon_{\text{liq}}^* \neq \varepsilon_{\text{vap}}^*$ (first order phase transition) then

- ① Euler system: strict hyperbolicity ($\neq p$ -system),
- ② Riemann problem: multitude of entropy (Lax) solutions [R. MENIKOFF, B. J. PLOHR], uniqueness of Liu solution.

DYNAMIC LIQUID-VAPOR PHASE CHANGE

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If $\tau_{\text{liq}}^* \neq \tau_{\text{vap}}^*$ and $\varepsilon_{\text{liq}}^* \neq \varepsilon_{\text{vap}}^*$ (first order phase transition) then

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NUMERICAL SCHEME BASED ON RELAXATION APPROACH

$$\sigma(y, z, \psi, \tau, \varepsilon)$$

Optimization

$$s^{\text{eq}}(\tau, \varepsilon)$$

Off Equilibrium

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0 \\ \partial_t(\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = 0 \\ \partial_t(\varrho e) + \operatorname{div}((\varrho e + P)\mathbf{u}) = 0 \\ \partial_t z + \mathbf{u} \cdot \nabla z - z = \\ \quad \mu_j - P \quad z = \\ \quad y \quad y = \\ \varrho \psi + P \varrho \psi - \psi = \end{cases}$$

$$\mu_j \rightarrow \infty$$

Equilibrium

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0 \\ \partial_t(\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t(\varrho e) + \operatorname{div}((\varrho e + P^{\text{eq}})\mathbf{u}) = 0 \\ P^{\text{eq}}(\varrho, \varepsilon) = \frac{s_{\tau}^{\text{eq}}}{s_{\varepsilon}^{\text{eq}}} \end{cases}$$

Two Steps:

- ① Hydrodynamic (+ gravity, surface tension, heat diffusion, ...)
- ② Projection by solving the Phase-Change Equation

NUMERICAL SCHEME BASED ON RELAXATION APPROACH

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$\xrightarrow{\mu_j \rightarrow \infty}$

Equilibrium

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0 \\ \partial_t(\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t(\varrho e) + \operatorname{div}((\varrho e + P^{\text{eq}})\mathbf{u}) = 0 \\ P^{\text{eq}}(\varrho, \varepsilon) = \frac{s_\tau^{\text{eq}}}{s_\varepsilon^{\text{eq}}} \end{cases}$$

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NUMERICAL SCHEME BASED ON RELAXATION APPROACH

$$\sigma(y, z, \psi, \tau, \varepsilon)$$

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$$P(\varrho, \varepsilon, z, y, \psi) = \frac{\sigma_z}{\sigma_\varepsilon}$$

$$\mu_j \rightarrow \infty$$

Equilibrium

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0 \\ \partial_t(\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t(\varrho e) + \operatorname{div}((\varrho e + P^{\text{eq}})\mathbf{u}) = 0 \\ P^{\text{eq}}(\varrho, \varepsilon) = \frac{s_\tau^{\text{eq}}}{s_\varepsilon^{\text{eq}}} \end{cases}$$

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- ➋ Projection by solving the Phase-Change Equation

OFF EQUILIBRIUM SYSTEMS

❶ Lagrangian: $\mathcal{L}(\varrho, \mathbf{u}, \sigma, y, z, \psi) \stackrel{\text{def}}{=} \varrho \left(\frac{|\mathbf{u}|^2}{2} - \varepsilon(\varrho, \sigma, y, z, \psi) \right)$

Action: $\mathcal{A}(\nu) \stackrel{\text{def}}{=} \int_{t_1}^{t_2} \int_{\widehat{\Omega}(t; \nu)} \mathcal{L}(\widehat{\varrho}, \widehat{\varrho \mathbf{u}}, \widehat{s}, \widehat{y}, \widehat{z}, \widehat{\psi})(\widehat{\mathbf{x}}, t; \nu) d\widehat{\mathbf{x}} dt$

Minimization of the Action: $\frac{d\mathcal{A}}{d\nu}(\nu = 0) = 0$

❷ Energy: $\varepsilon \stackrel{\text{def}}{=} \sum_{\alpha} y_{\alpha} \varepsilon_{\alpha} \left(\frac{z_{\alpha}}{y_{\alpha}} \frac{1}{\varrho}, \frac{\psi_{\alpha}}{y_{\alpha}} \sigma \right)$

❸ Positive Entropy Production: $D_t \sigma \geq 0$

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0 \\ \partial_t (\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = 0 \\ \partial_t (\varrho e) + \operatorname{div}((\varrho e + P) \mathbf{u}) = 0 \\ \partial_t z + \mathbf{u} \cdot \operatorname{grad} z = \mu_z(z^{\text{eq}} - z) \\ \partial_t y + \mathbf{u} \cdot \operatorname{grad} y = \mu_y(y^{\text{eq}} - y) \\ \partial_t \psi + \mathbf{u} \cdot \operatorname{grad} \psi = \mu_{\psi}(\psi^{\text{eq}} - \psi) \end{cases}$$

$$P(\varrho, \varepsilon, z, y, \psi) = \frac{\sigma_{\tau}}{\sigma_{\varepsilon}}$$

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$$P(\tau, \varepsilon, z, y, \psi^{\text{eq}}(\tau, \varepsilon)) = \frac{\sigma_{\tau}}{\sigma_{\varepsilon}}$$

OFF EQUILIBRIUM SYSTEMS

❶ Lagrangian: $\mathcal{L}(\varrho, \mathbf{u}, \sigma, y, z, \psi) \stackrel{\text{def}}{=} \varrho \left(\frac{|\mathbf{u}|^2}{2} - \varepsilon(\varrho, \sigma, y, z, \psi) \right)$

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HYDRODYNAMIC STEP

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0 \\ \partial_t (\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = 0 \\ \partial_t (\varrho e) + \operatorname{div}((\varrho e + P) \mathbf{u}) = 0 \\ \partial_t z + \mathbf{u} \cdot \operatorname{\mathbf{grad}} z = 0 \\ \partial_t y + \mathbf{u} \cdot \operatorname{\mathbf{grad}} y = 0 \end{cases}$$

$T^{\text{liq}} = T^{\text{vap}}$ in the mixture

$$P(\varrho, \varepsilon, z, y) = \frac{\sigma_\tau}{\sigma_\varepsilon}$$

Scheme:
Roe quasi-conservative [S. Kokh]

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$$P(\varrho, \varepsilon, z, y) = \frac{\sigma_\tau}{\sigma_\varepsilon}$$

Scheme:
antidiffusive [Lagoutière and Kokh]

PROJECTION STEP

In each cell, (τ, ε) is computed in the hydrodynamic step and we update the fractions as follows:

1. T^* : solution of the Phase-Change Equation:

$$\frac{\tau - \tau_{\text{vap}}(T, P^{\text{sat}}(T))}{\tau_{\text{liq}}(T, P^{\text{sat}}(T)) - \tau_{\text{vap}}(T, P^{\text{sat}}(T))} = \frac{\varepsilon - \varepsilon_{\text{vap}}(T, P^{\text{sat}}(T))}{\varepsilon_{\text{liq}}(T, P^{\text{sat}}(T)) - \varepsilon_{\text{vap}}(T, P^{\text{sat}}(T))}$$

2. $\tau_\alpha^* \stackrel{\text{def}}{=} \tau_\alpha(T^*, P^{\text{sat}}(T^*))$, $\varepsilon_\alpha^* \stackrel{\text{def}}{=} \varepsilon_\alpha(T^*, P^{\text{sat}}(T^*))$, $y^* = y(T^*, P^{\text{sat}}(T^*))$.

3. 3.1. if $0 < y^* < 1$ then (τ, ε) is a saturated state and we set

$$y^{\text{eq}} = y^*, \quad z^{\text{eq}} = y^* \tau_{\text{liq}}^*/\tau, \quad \psi^{\text{eq}} = y^* \varepsilon_{\text{liq}}^*/\varepsilon,$$

3.2. otherwise, if y^* is outside the range $(0, 1)$,

3.2.1. if $s_{\text{liq}}(\tau, \varepsilon) > s_{\text{vap}}(\tau, \varepsilon)$ then (τ, ε) is a liquid state, therefore we set

$$y^{\text{eq}}(\tau, \varepsilon) = 1, \quad z^{\text{eq}}(\tau, \varepsilon) = 1, \quad \psi^{\text{eq}}(\tau, \varepsilon) = 1,$$

3.2.2. if $s_{\text{liq}}(\tau, \varepsilon) < s_{\text{vap}}(\tau, \varepsilon)$ then τ, ε is a vapor state, therefore we set

$$y^{\text{eq}}(\tau, \varepsilon) = 0, \quad z^{\text{eq}}(\tau, \varepsilon) = 0, \quad \psi^{\text{eq}}(\tau, \varepsilon) = 0,$$

OUTLINE

1 Context

2 Model

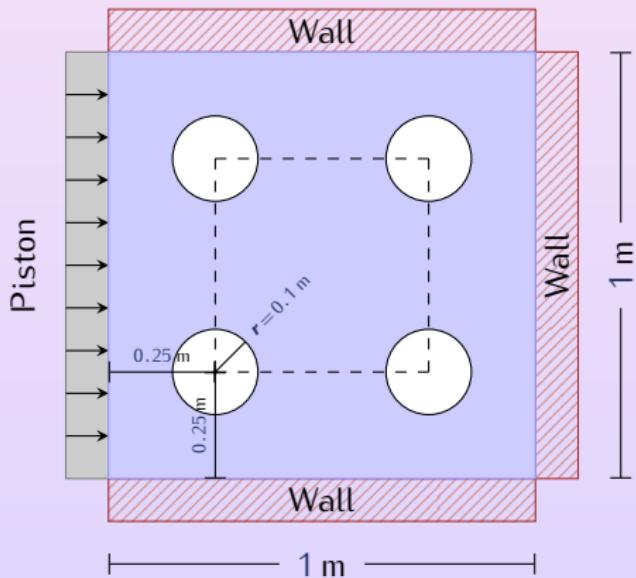
- Governing equations
- Equation of State

3 Numerical Approximation and Example

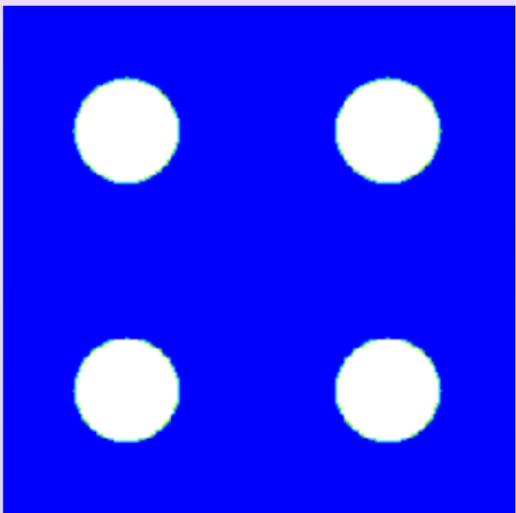
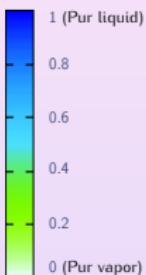
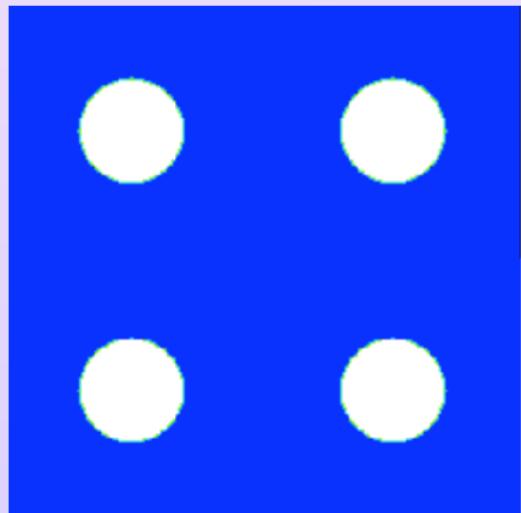
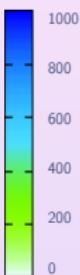
- Conservation Laws
- Numerical Scheme
- Numerical Example

4 Conclusion

COMPRESSION OF VAPOR BUBBLES



COMPRESSION OF VAPOR BUBBLES

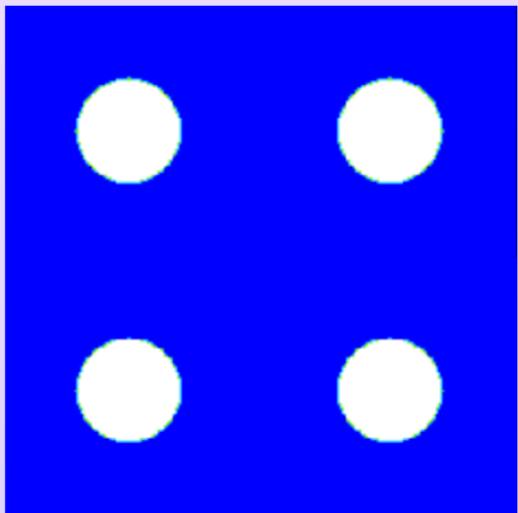
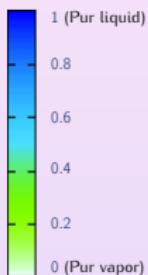
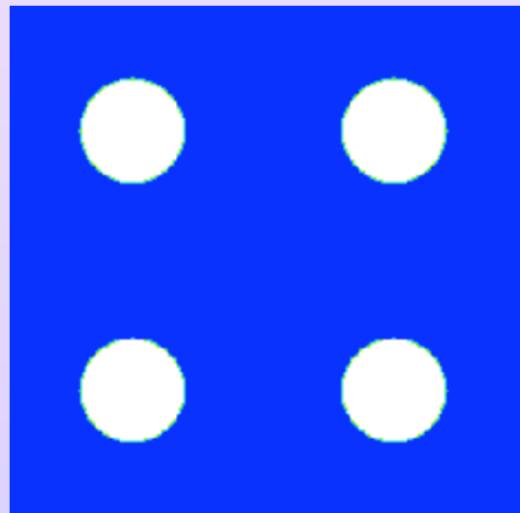
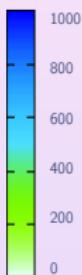
Massee fraction y Density ϱ 

◀ Geometry

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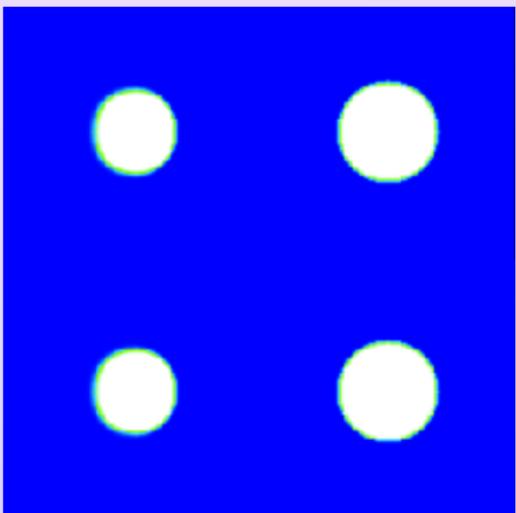
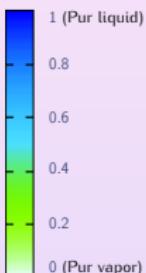
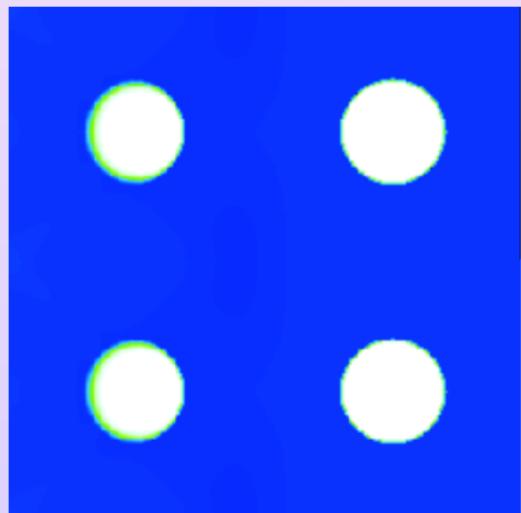
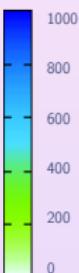
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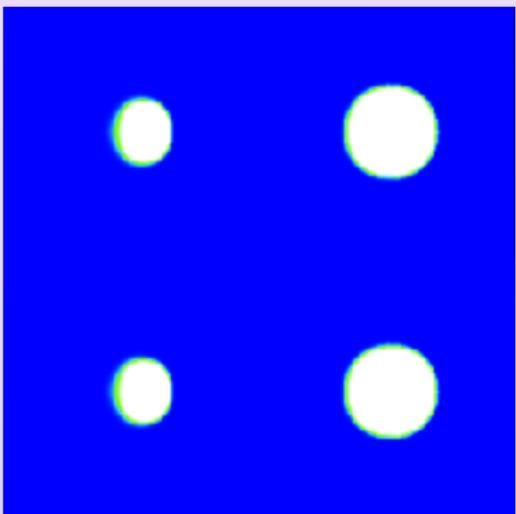
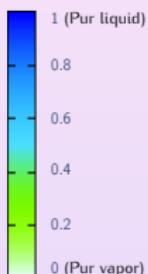
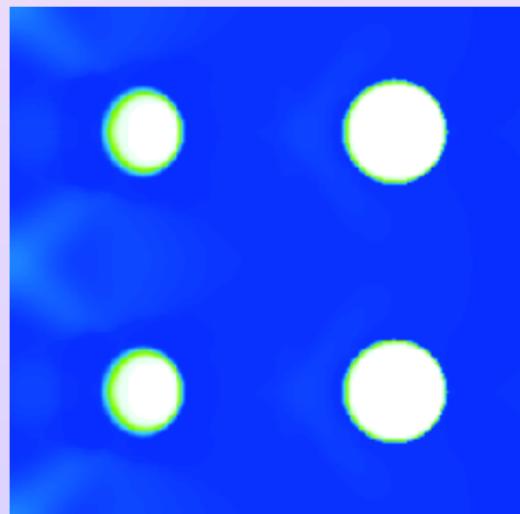
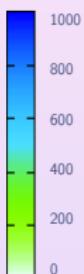
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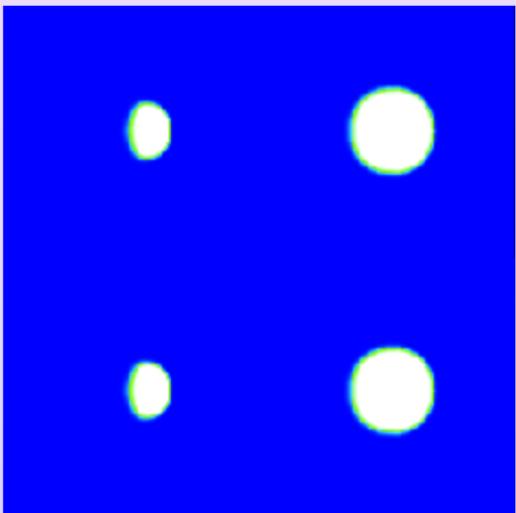
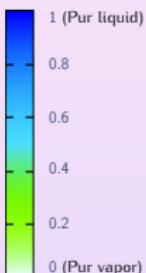
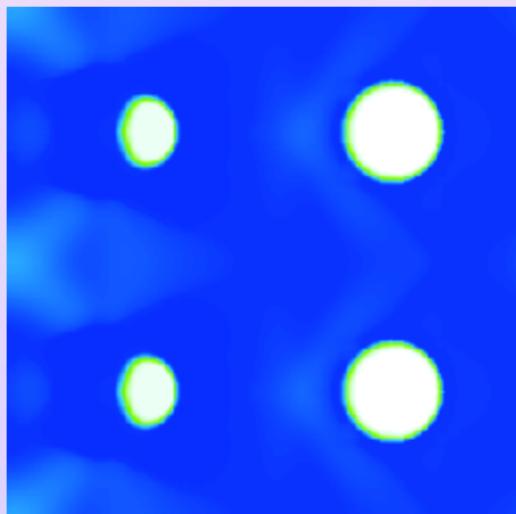
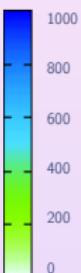
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◀ Geometry

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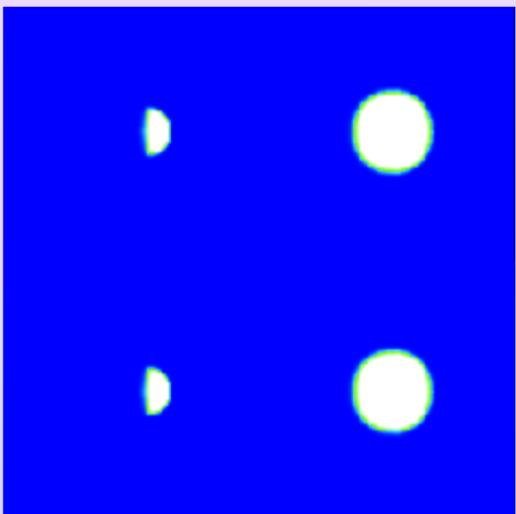
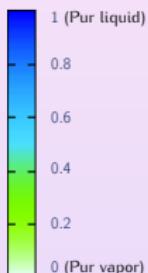
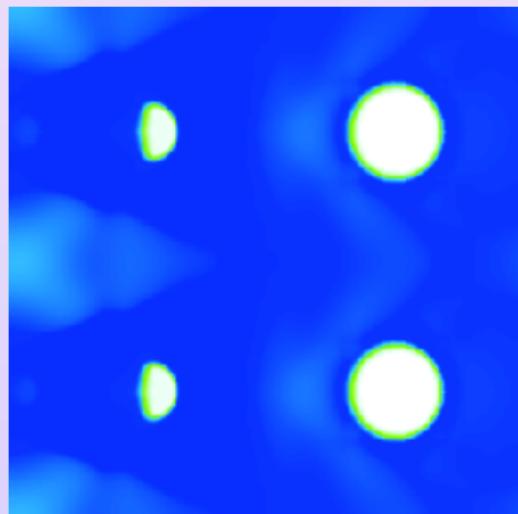
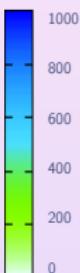
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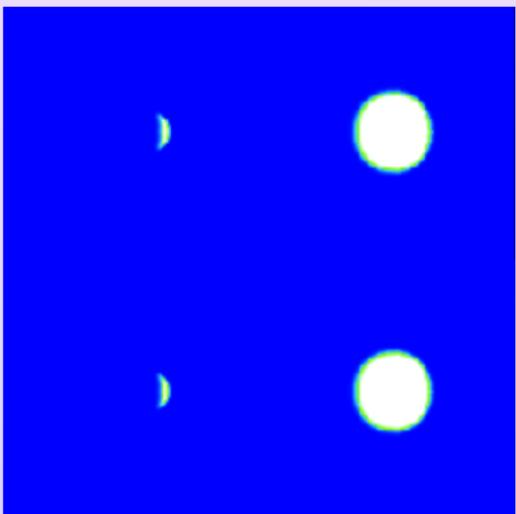
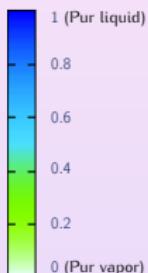
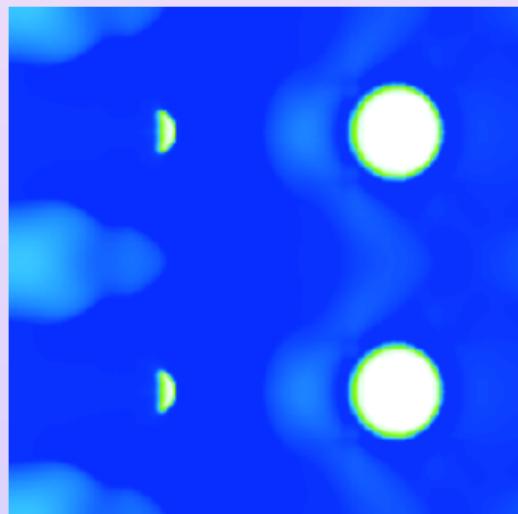
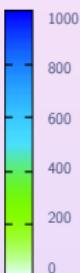
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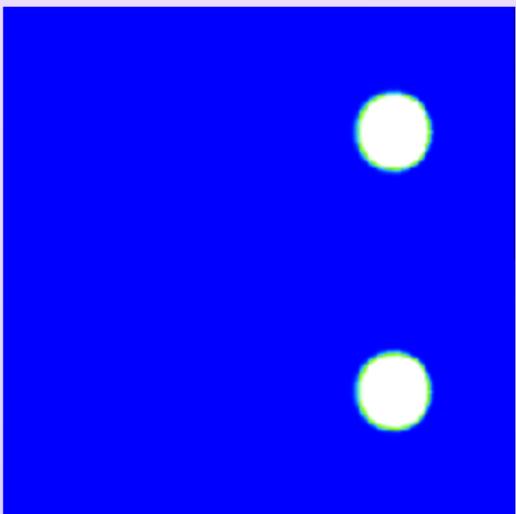
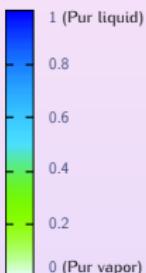
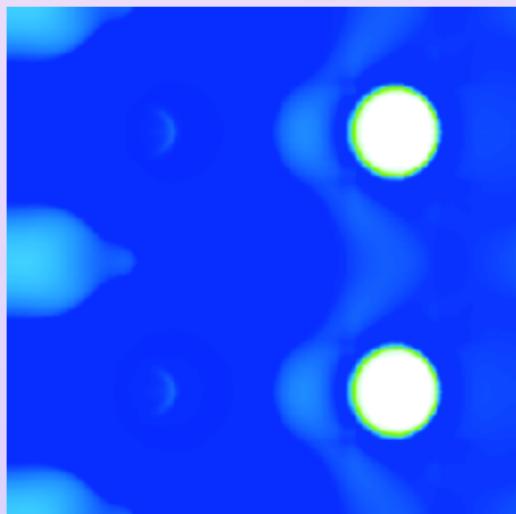
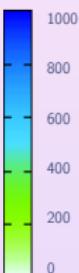
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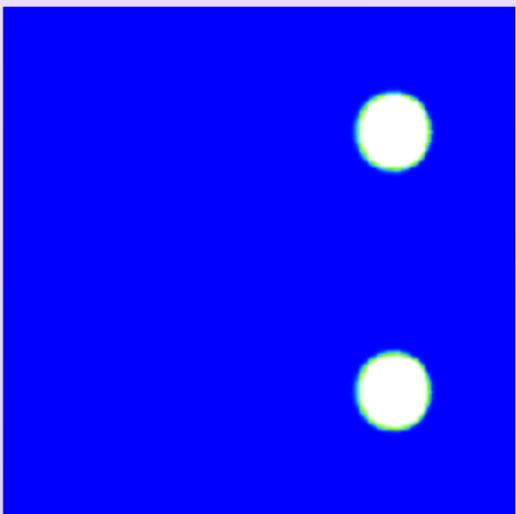
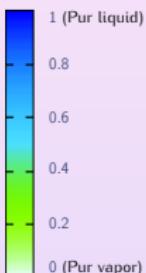
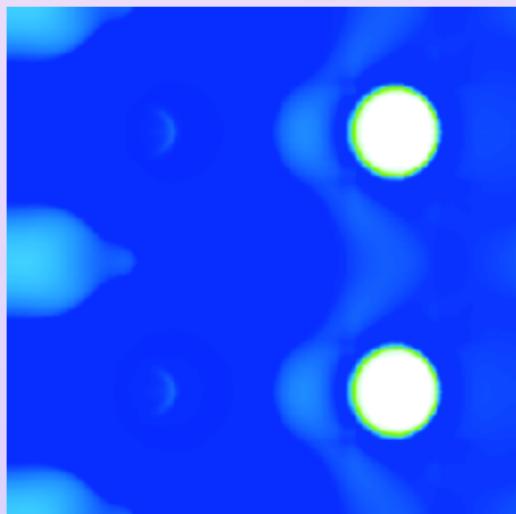
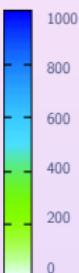
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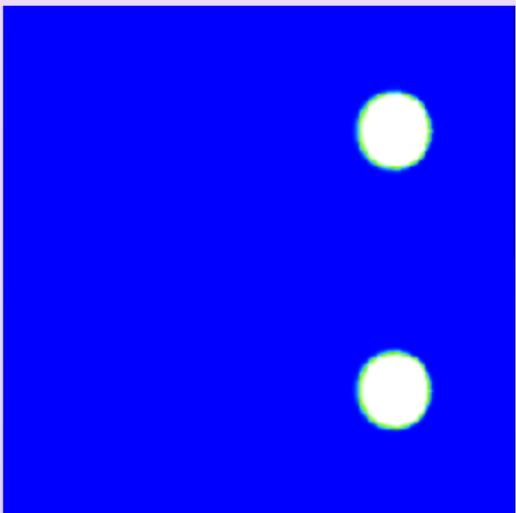
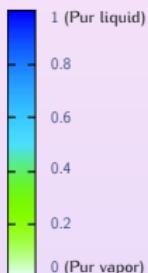
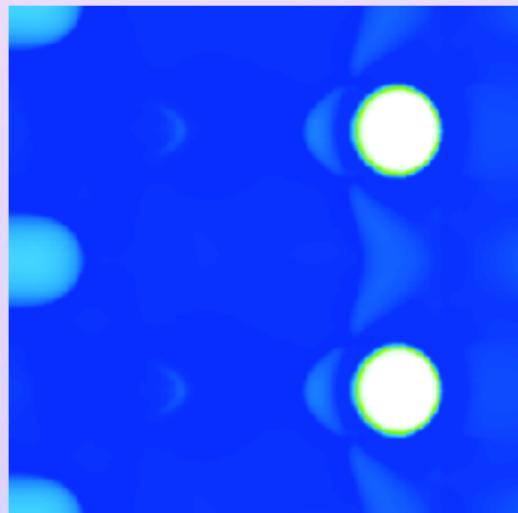
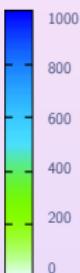
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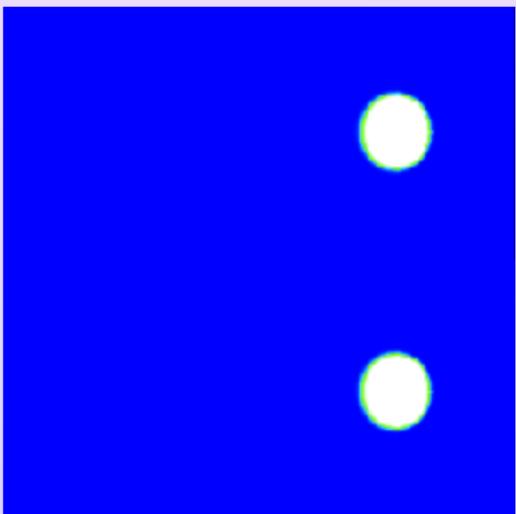
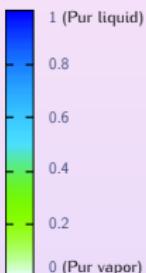
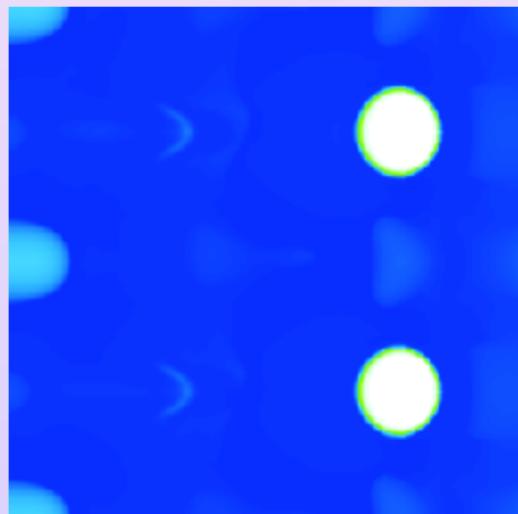
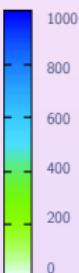
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◀ Geometry

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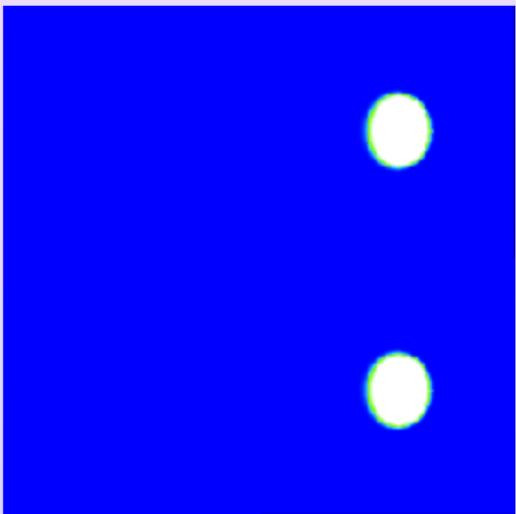
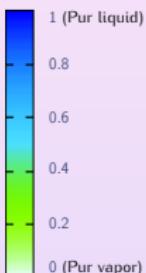
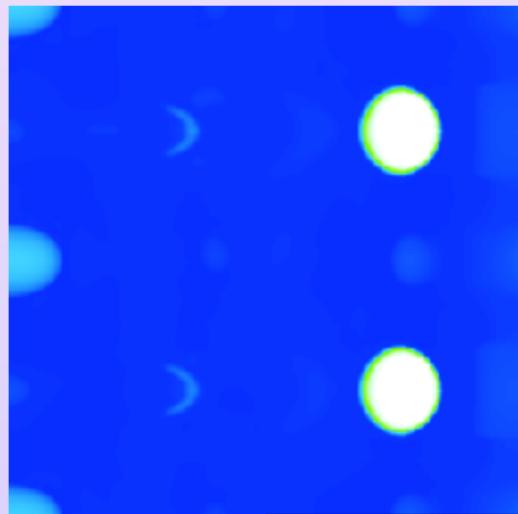
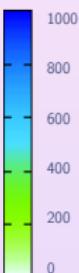
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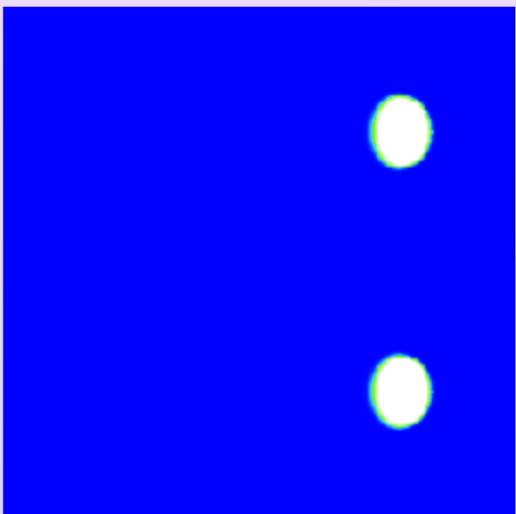
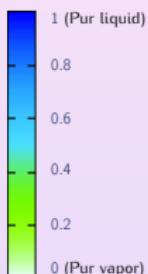
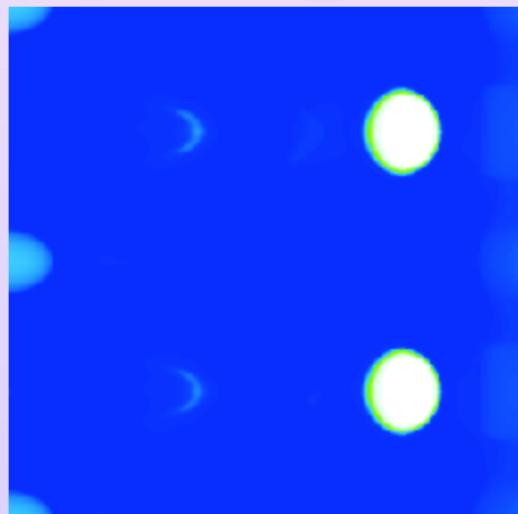
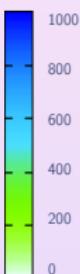
Massee fraction y Density ϱ 

◀ Geometry

▶ Play

▶ Skip

COMPRESSION OF VAPOR BUBBLES

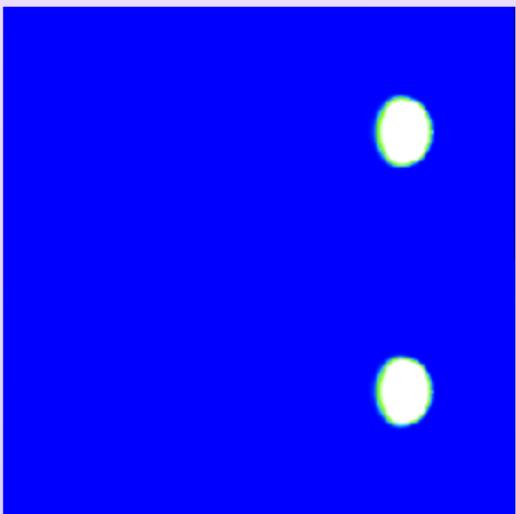
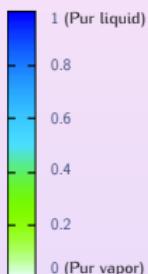
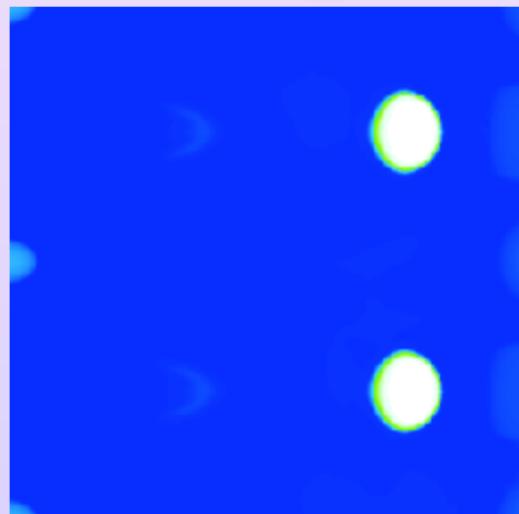
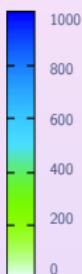
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◀ Geometry

▶ Play

▶ Skip

COMPRESSION OF VAPOR BUBBLES

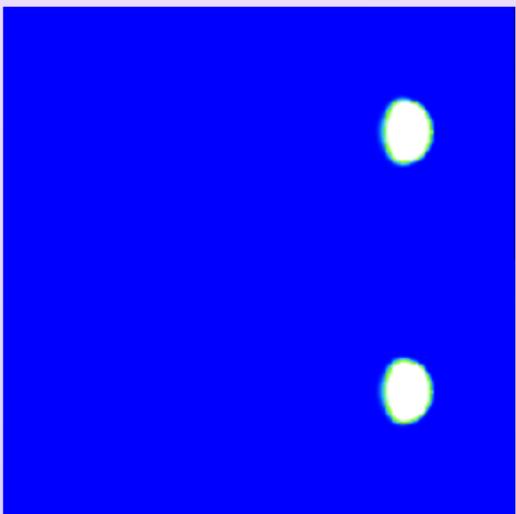
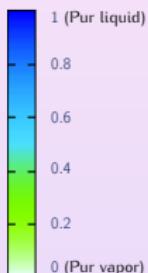
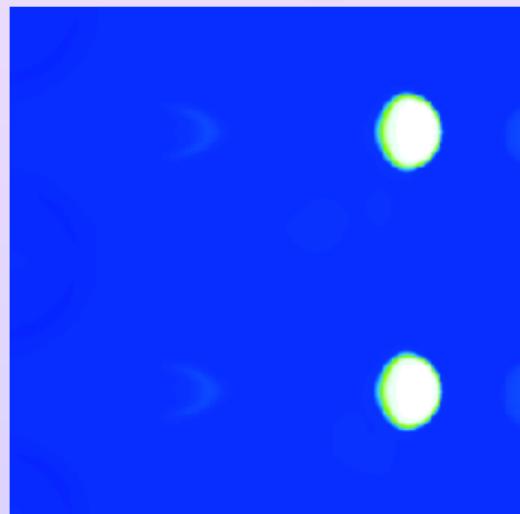
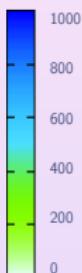
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◀ Geometry

▶ Play

▶ Skip

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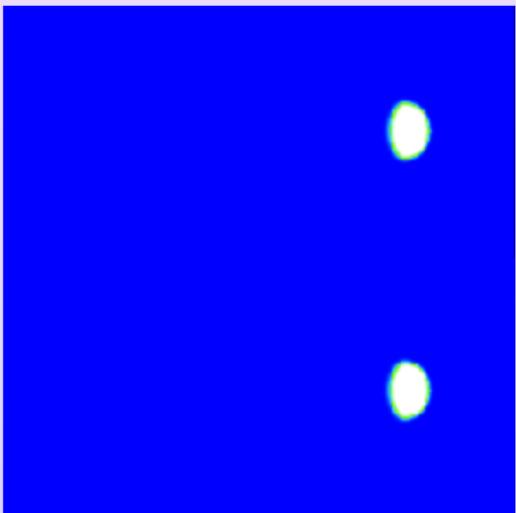
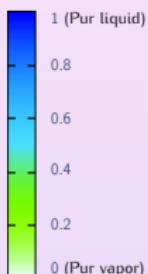
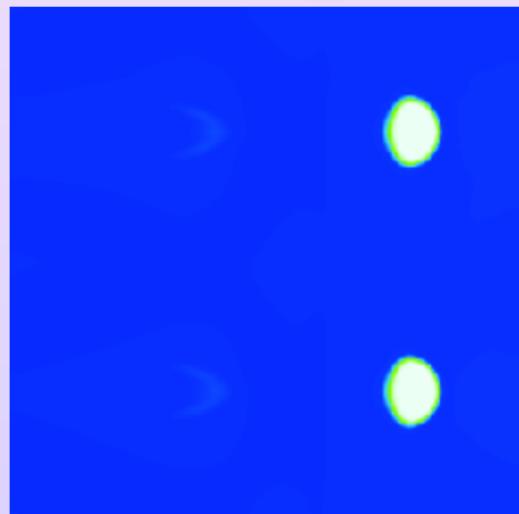
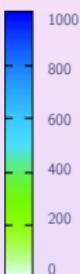
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◀ Geometry

▶ Play

▶ Skip

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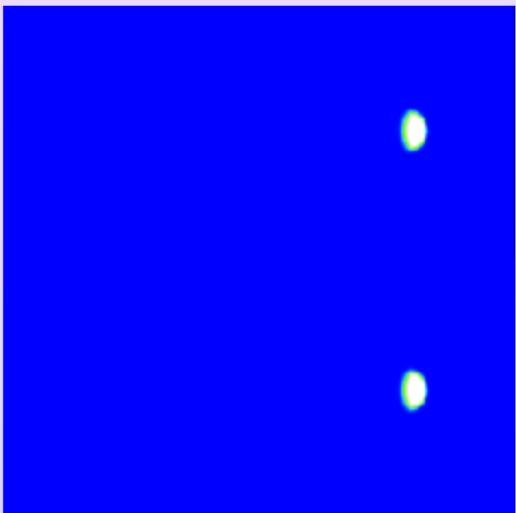
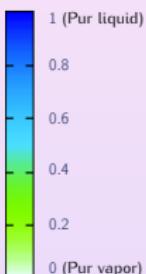
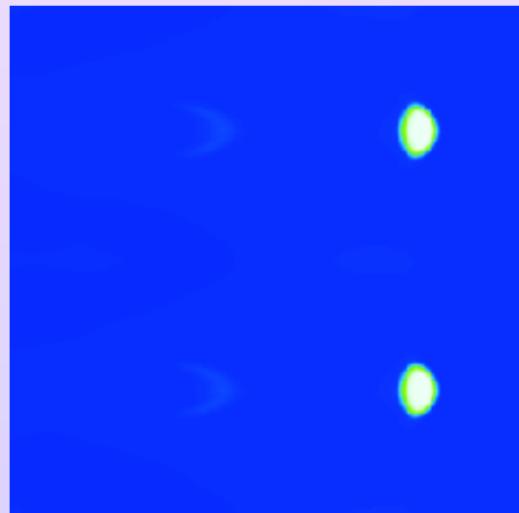
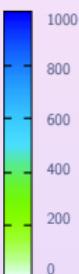
Massee fraction y Density ϱ 

◀ Geometry

▶ Play

▶ Skip

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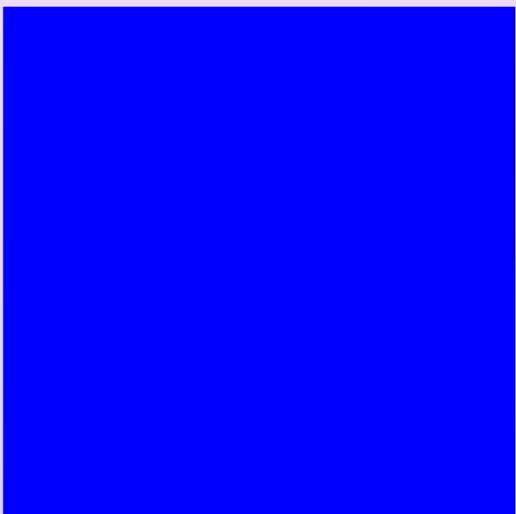
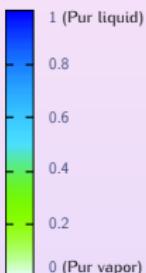
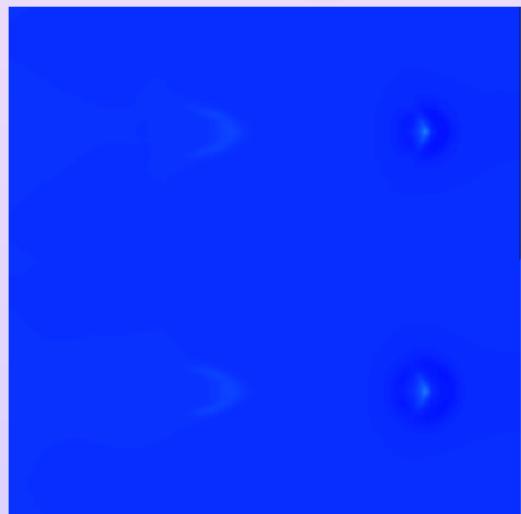
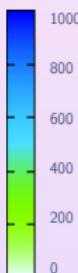
Massee fraction y Density ϱ 

◀ Geometry

▶ Play

▶ Skip

COMPRESSION OF VAPOR BUBBLES

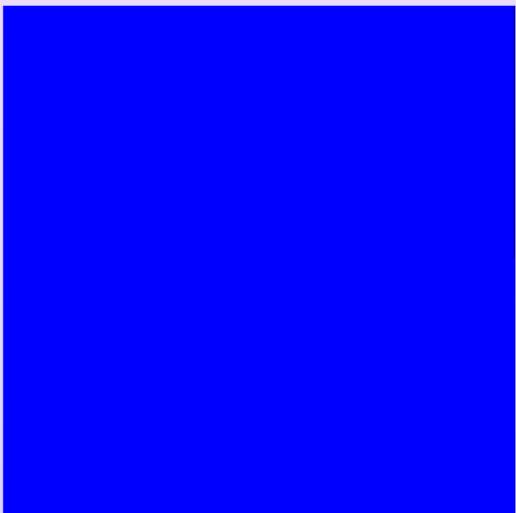
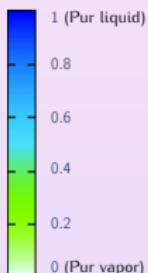
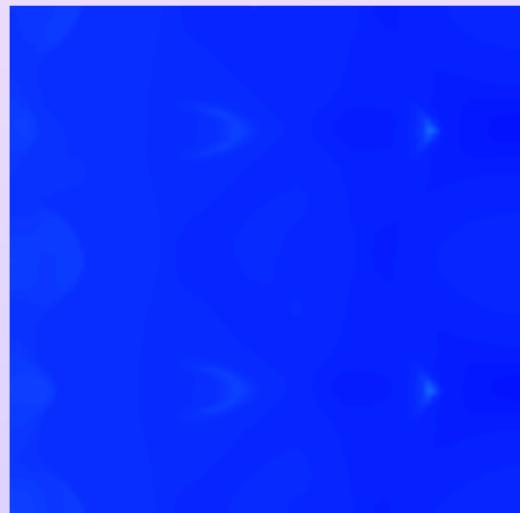
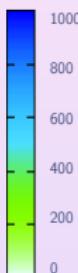
Massee fraction y Density ϱ 

◀ Geometry

▶ Play

▶ Skip

COMPRESSION OF VAPOR BUBBLES

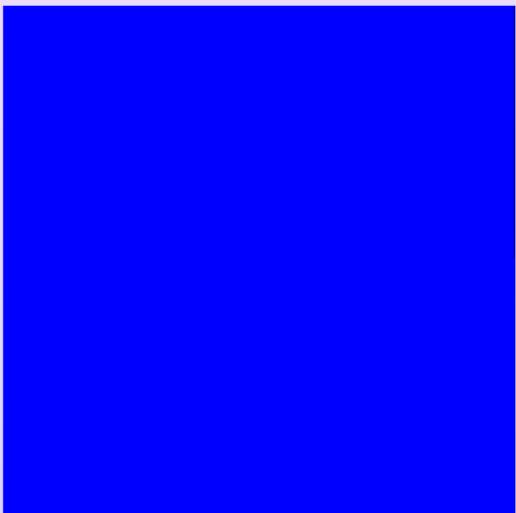
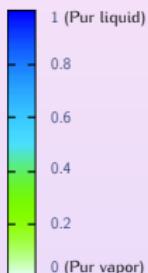
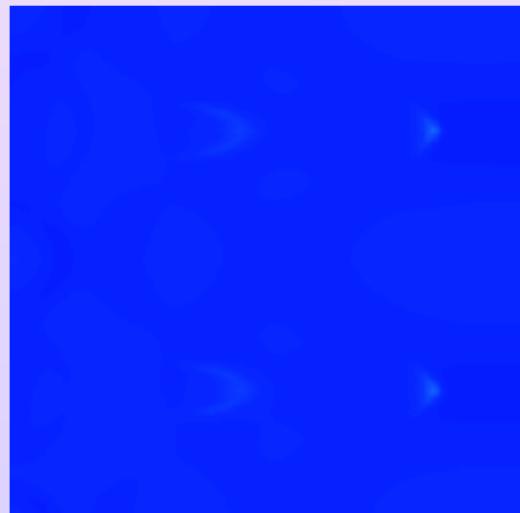
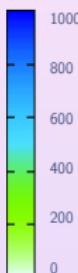
Massee fraction y Density ϱ 

◀ Geometry

▶ Play

▶ Skip

COMPRESSION OF VAPOR BUBBLES

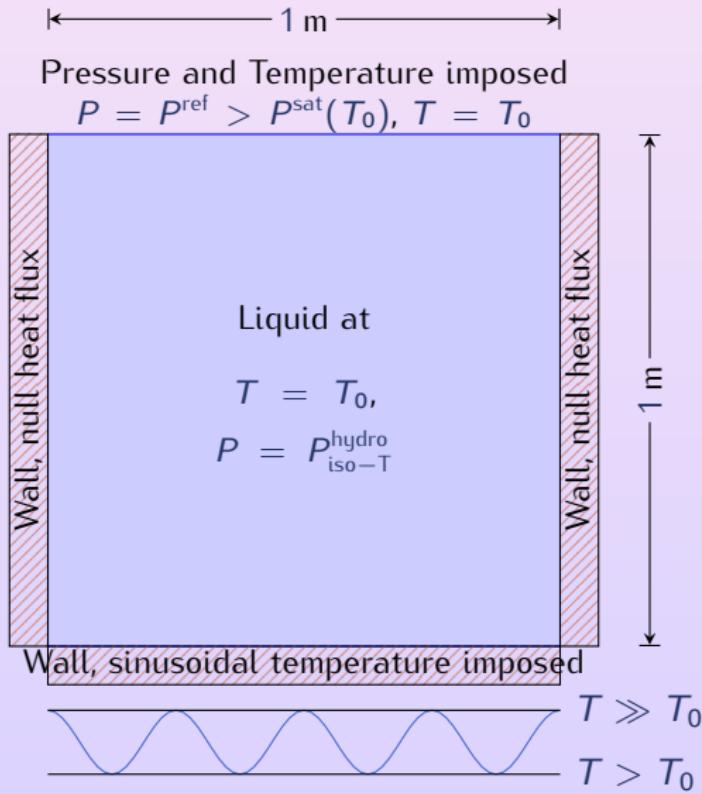
Massee fraction y Density ϱ 

◀ Geometry

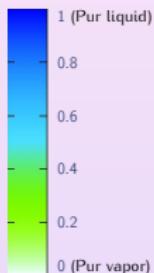
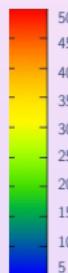
▶ Play

▶ Skip

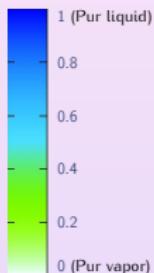
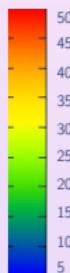
TRANSITION TO A FILM BOILING



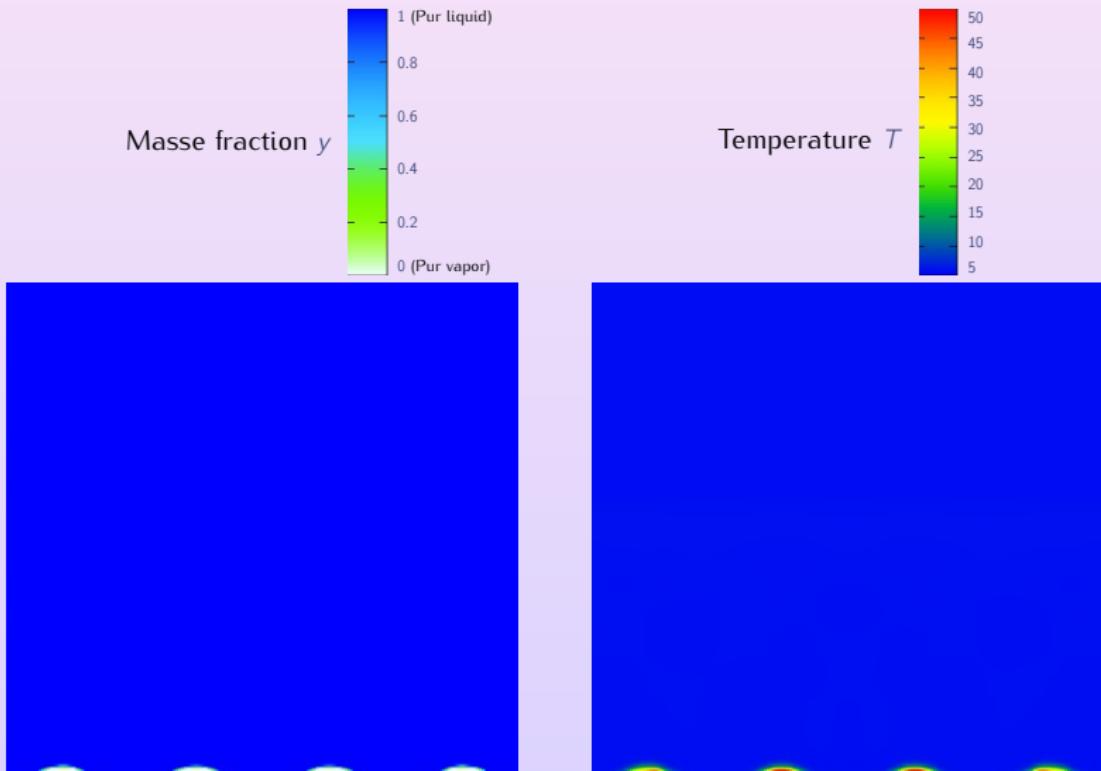
TRANSITION TO A FILM BOILING

Massee fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶ Skip](#)

TRANSITION TO A FILM BOILING

Massee fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶ Skip](#)

TRANSITION TO A FILM BOILING

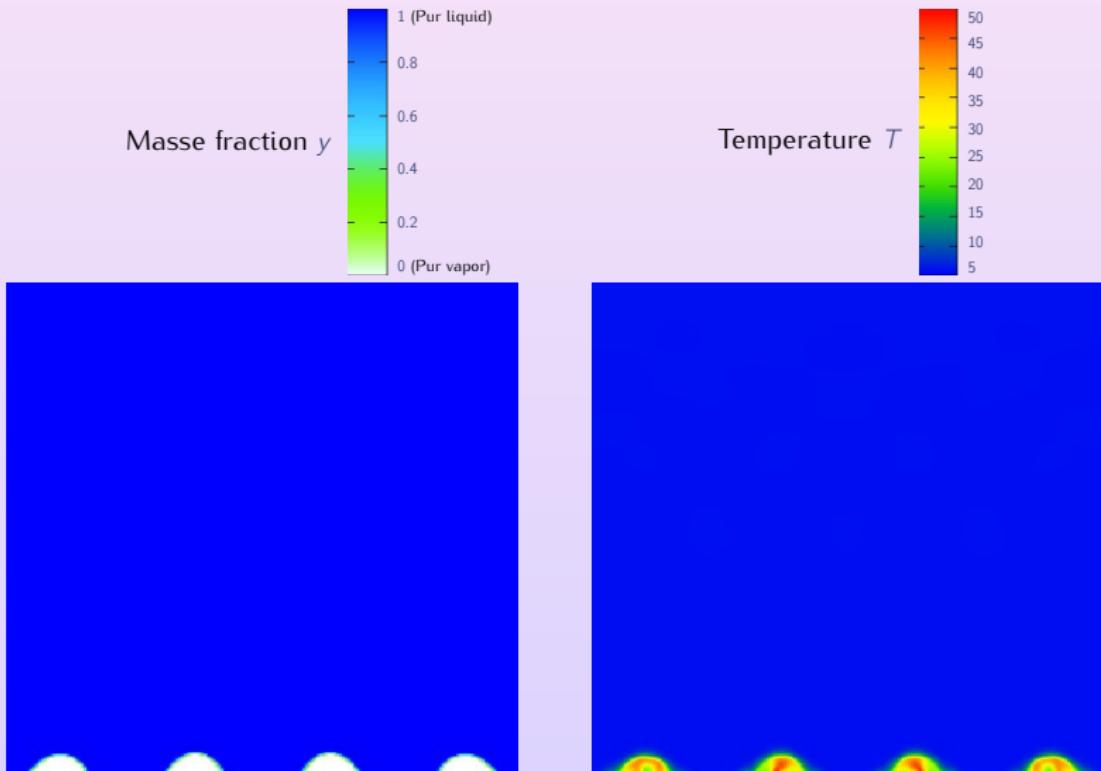


◀ Geometry

▶ Play

▶ Skip

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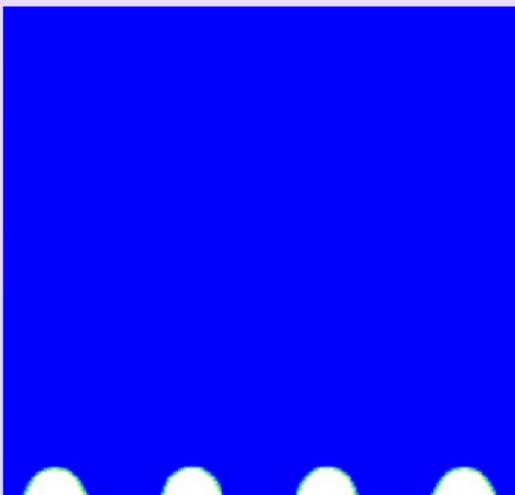
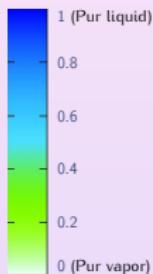
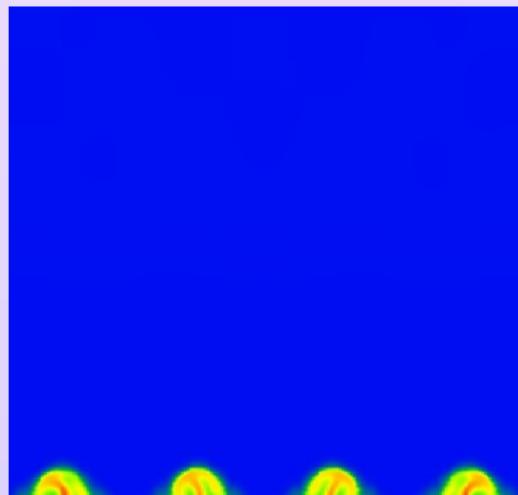
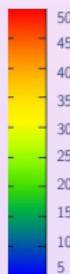


◀ Geometry

▶ Play

▶ Skip

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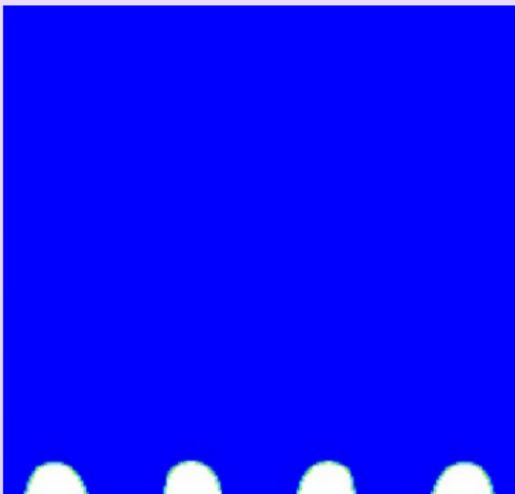
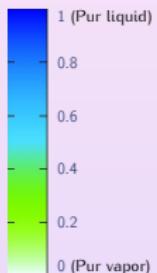
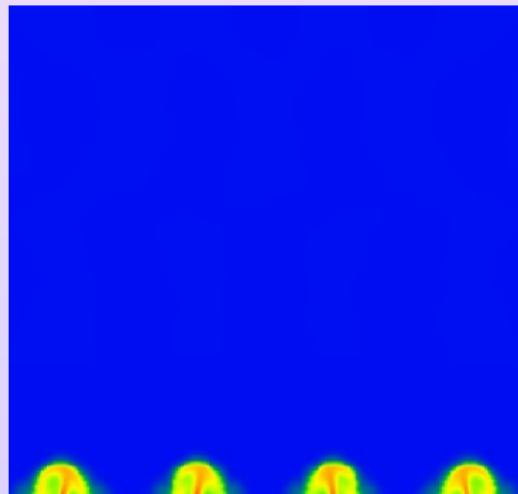
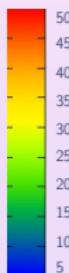
Massee fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

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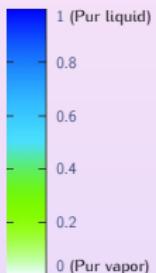
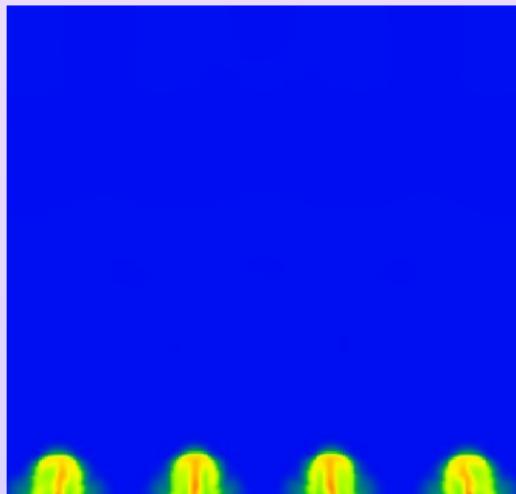
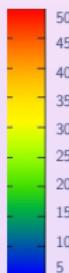
Massee fraction y Temperatuure T 

◀ Geometry

▶ Play

▶ Skip

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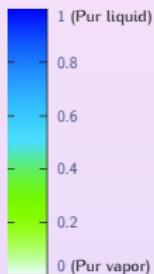
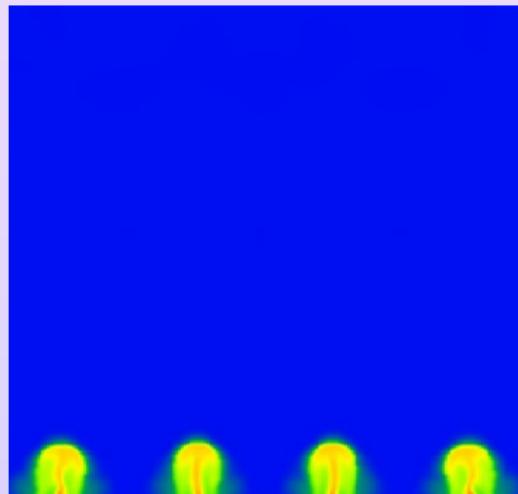
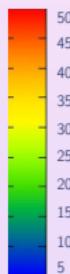
Massee fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

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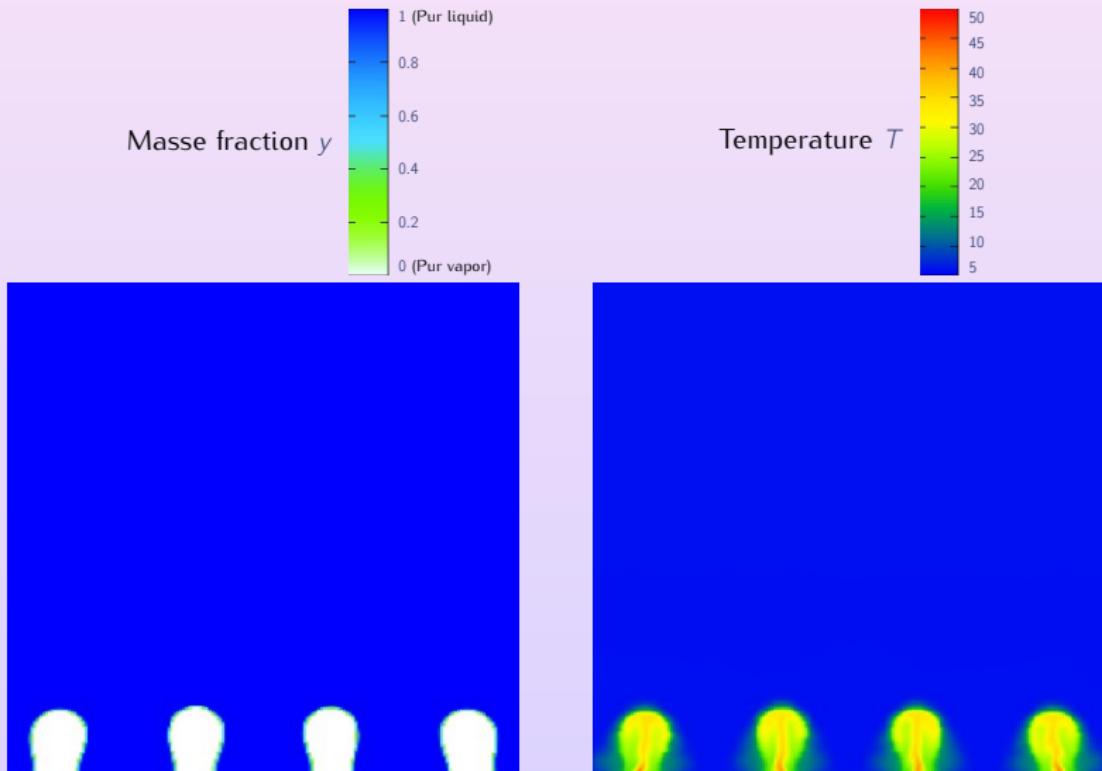
Massee fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

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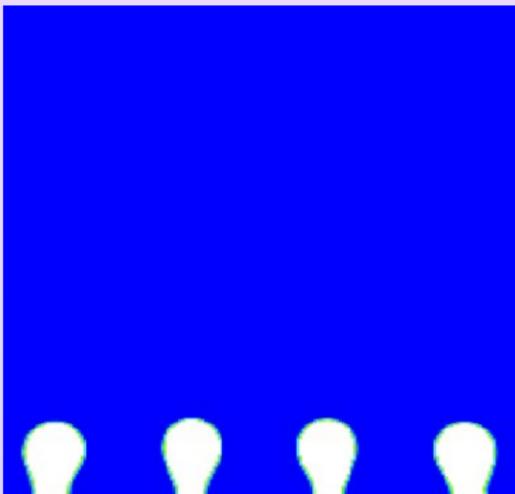
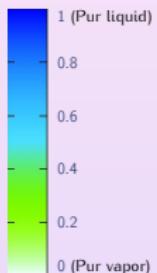
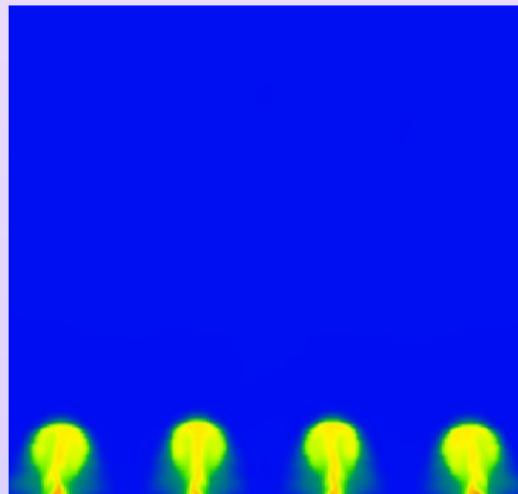
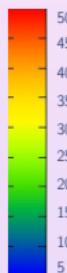


◀ Geometry

▶ Play

▶ Skip

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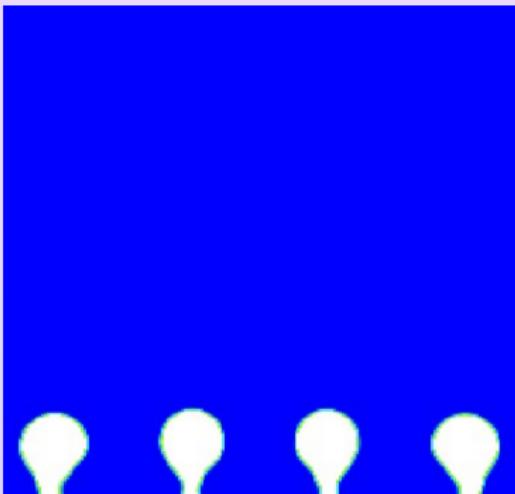
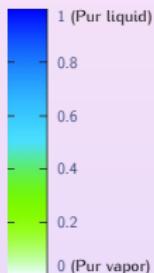
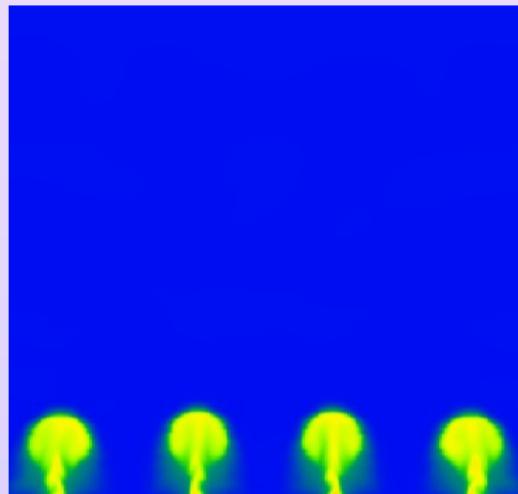
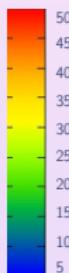
Massee fraction y Temperature T 

◀ Geometry

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▶ Skip

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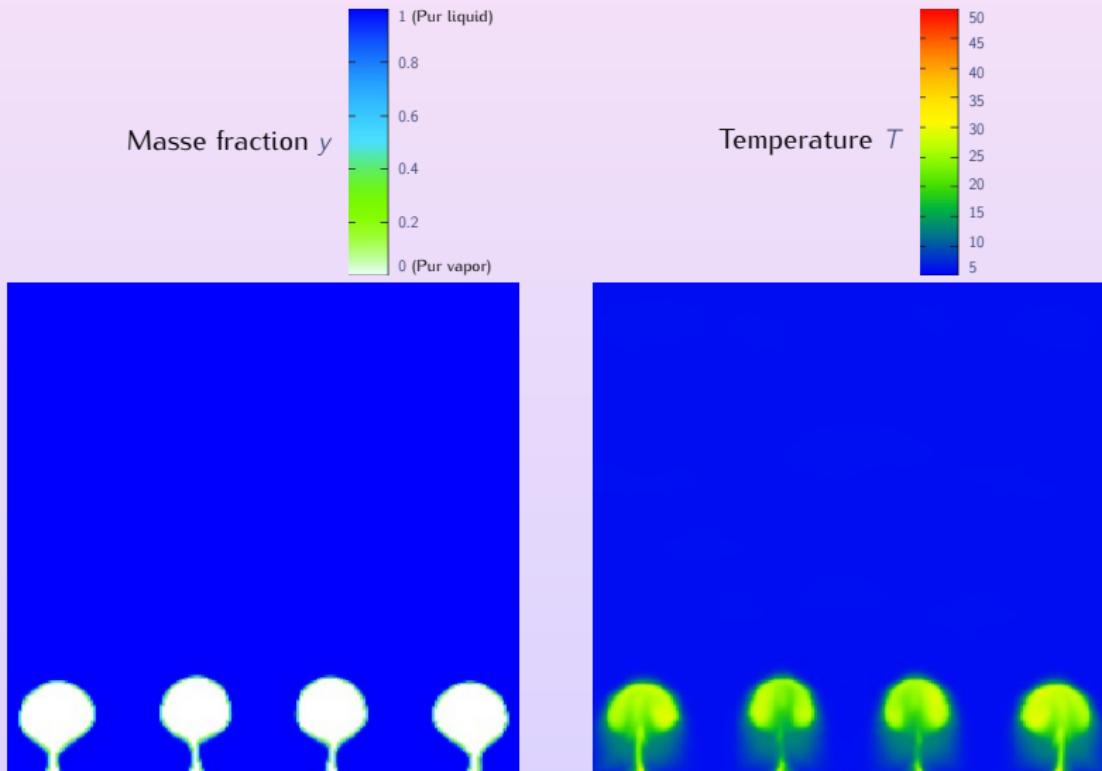
Massee fraction y Temperature T 

◀ Geometry

▶ Play

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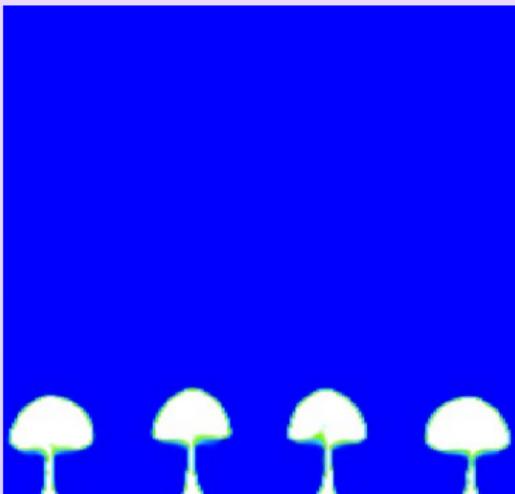
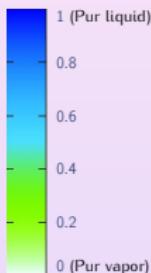
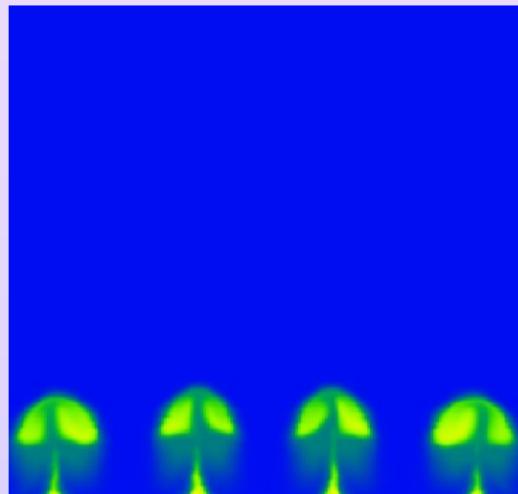
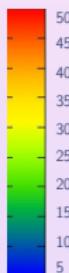


◀ Geometry

▶ Play

▶ Skip

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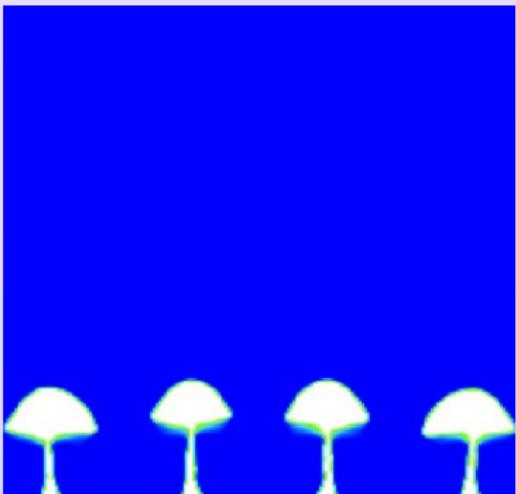
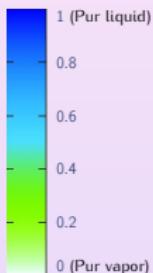
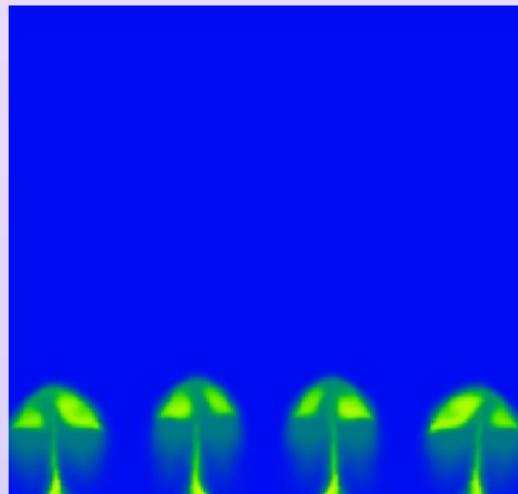
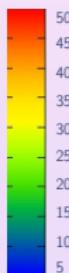
Mass fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

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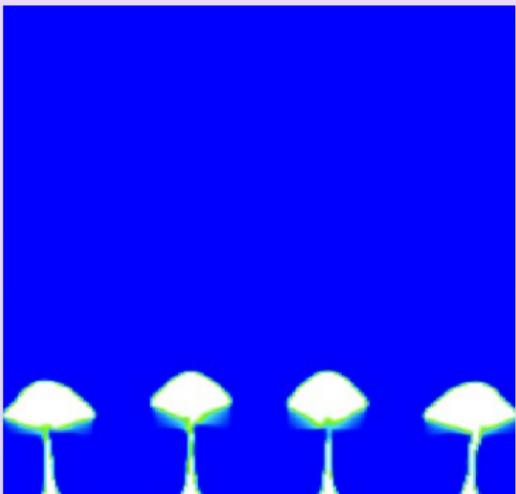
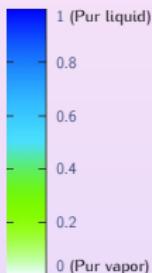
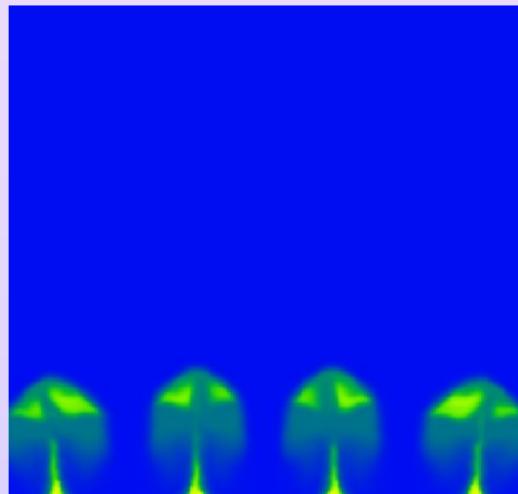
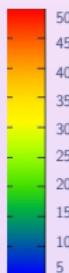
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◀ Geometry

▶ Play

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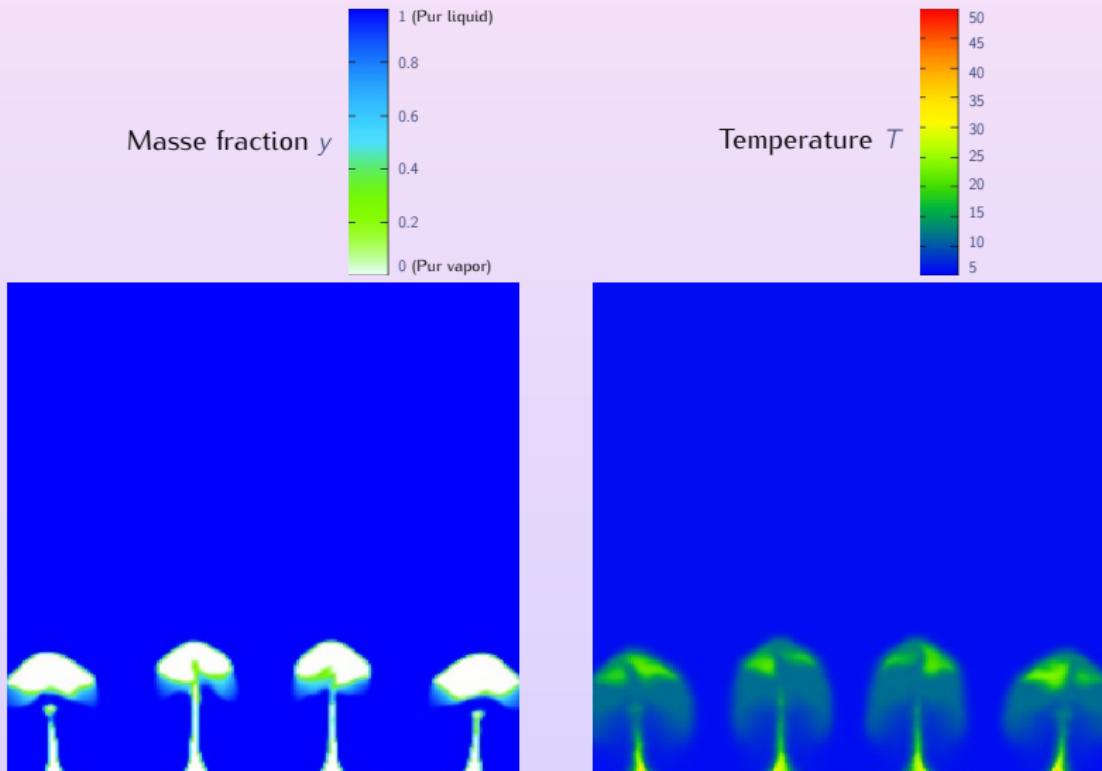
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◀ Geometry

▶ Play

▶ Skip

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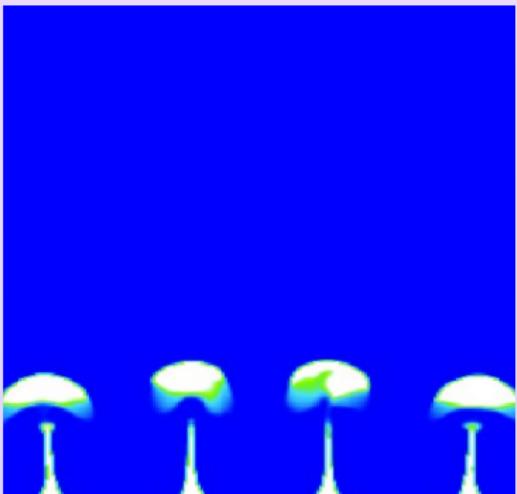
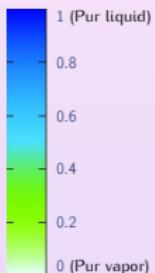
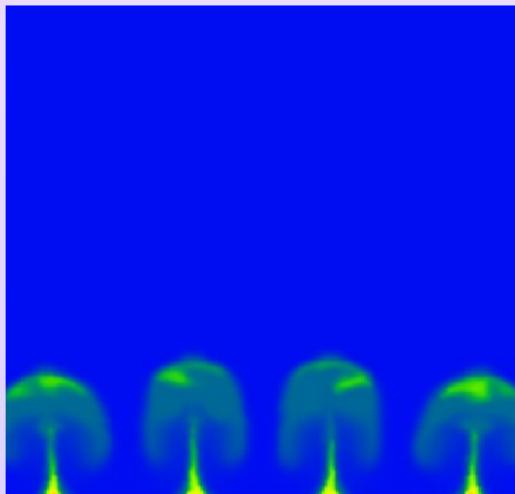
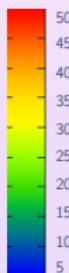


◀ Geometry

▶ Play

▶ Skip

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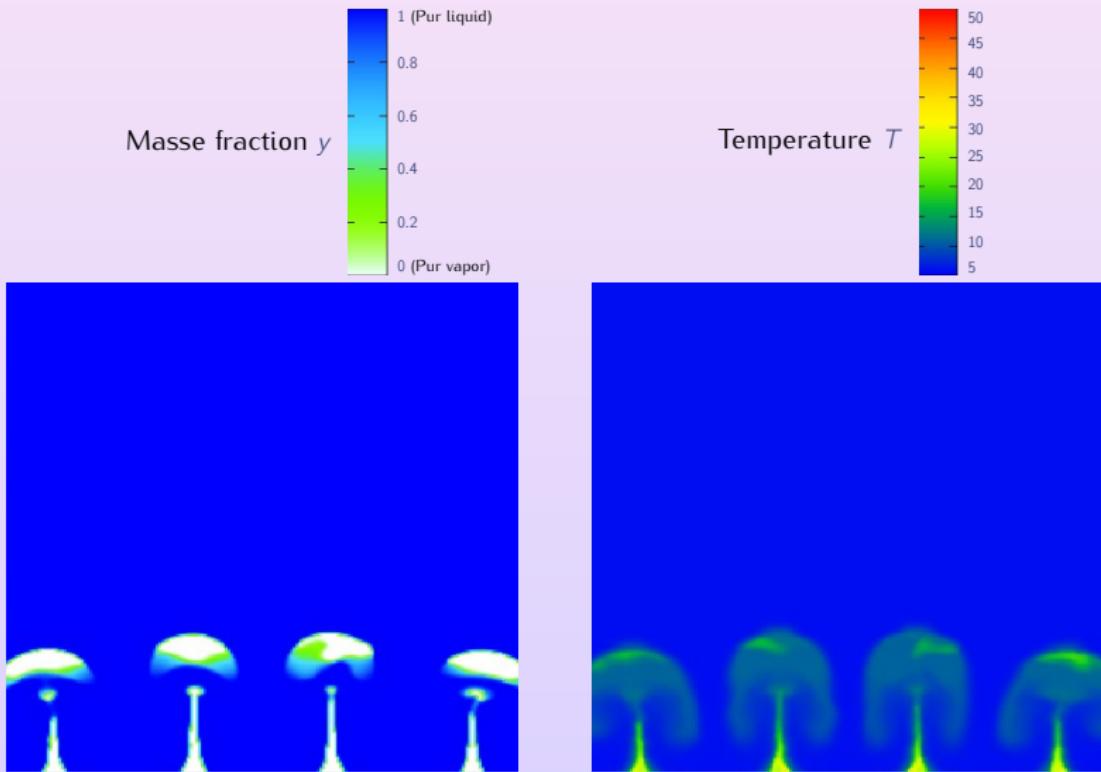
Massee fraction y Temperature T 

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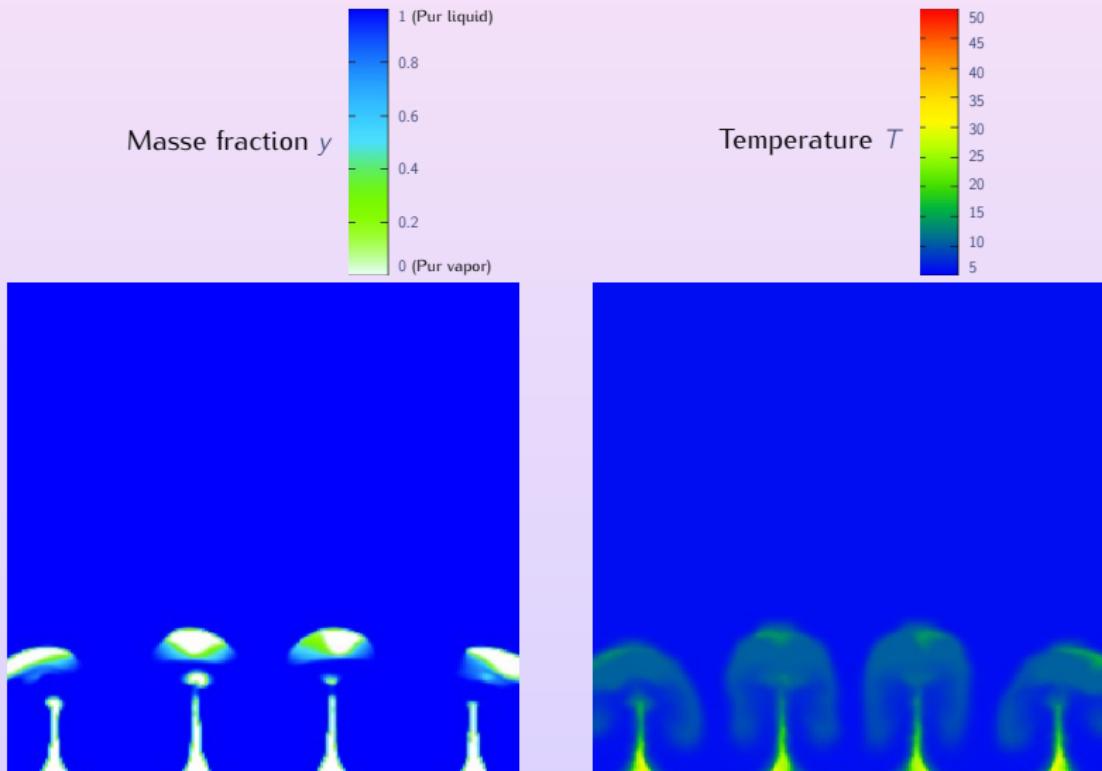


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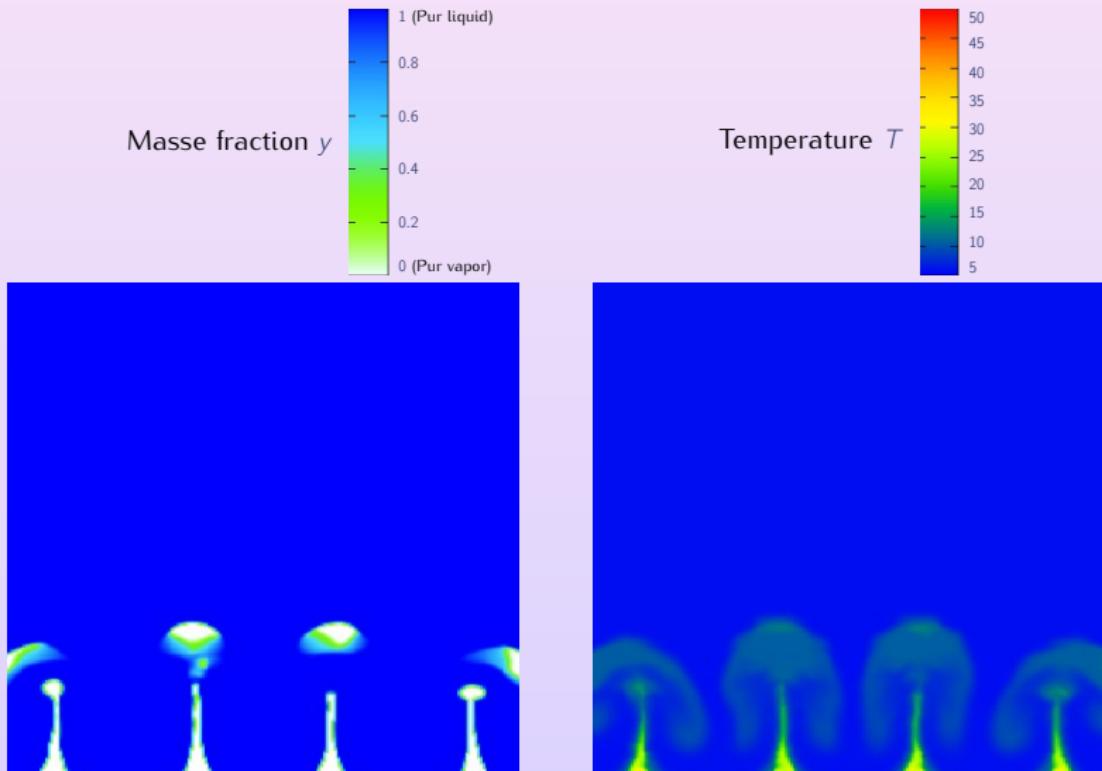


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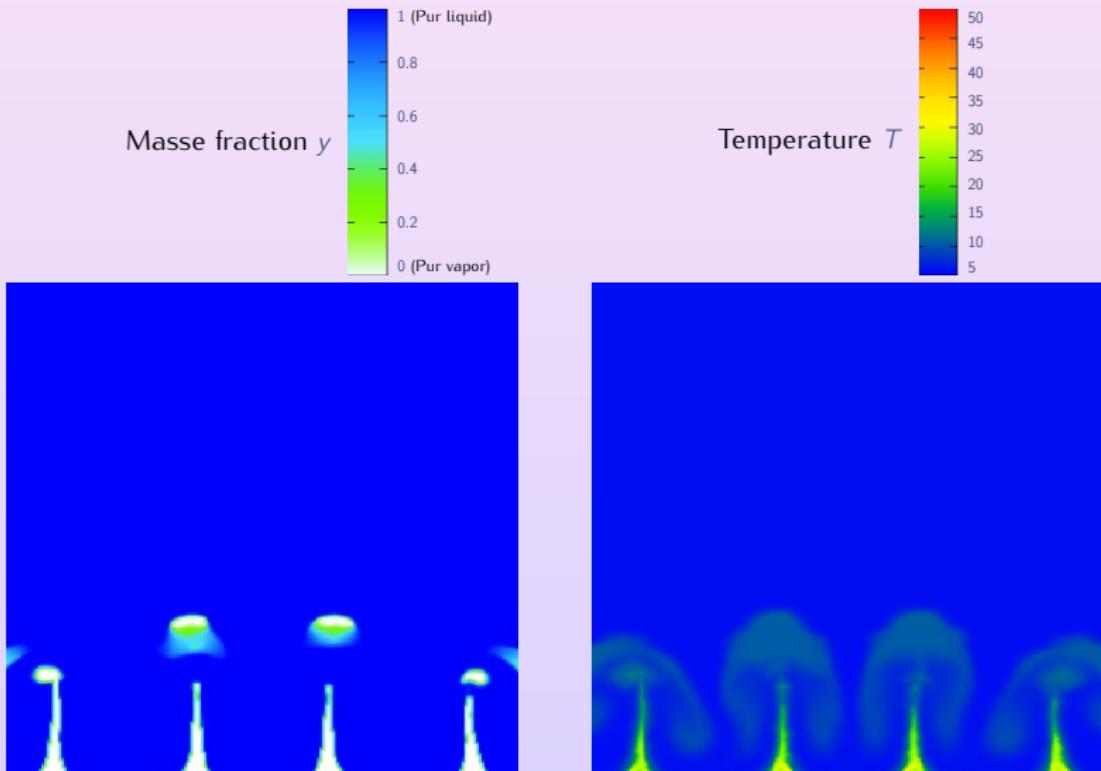


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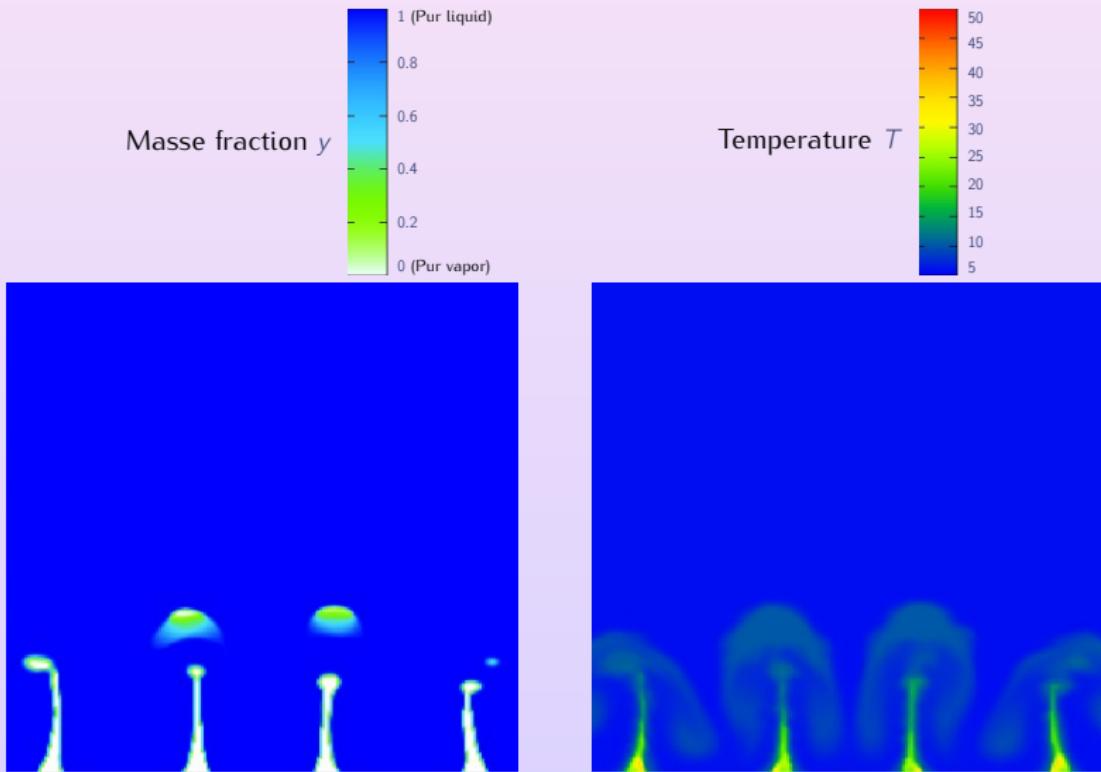


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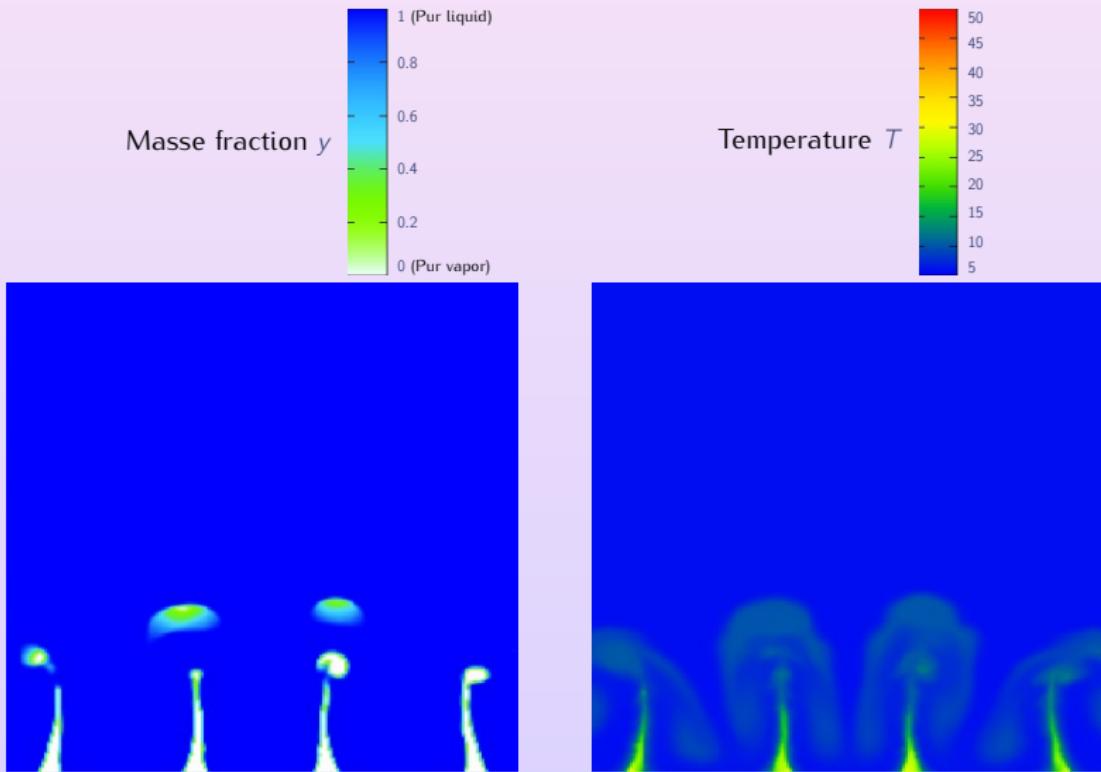


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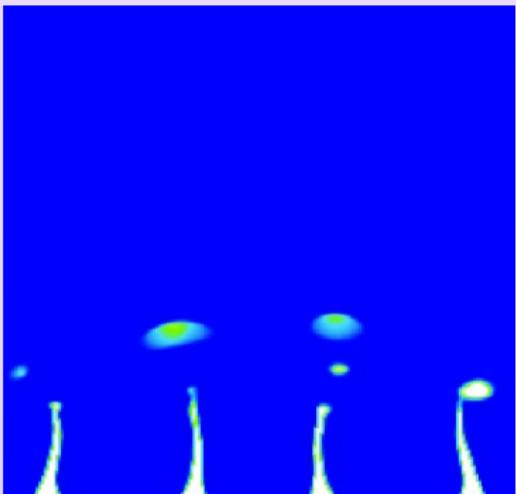
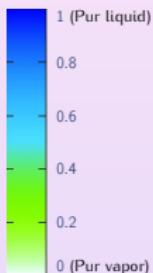
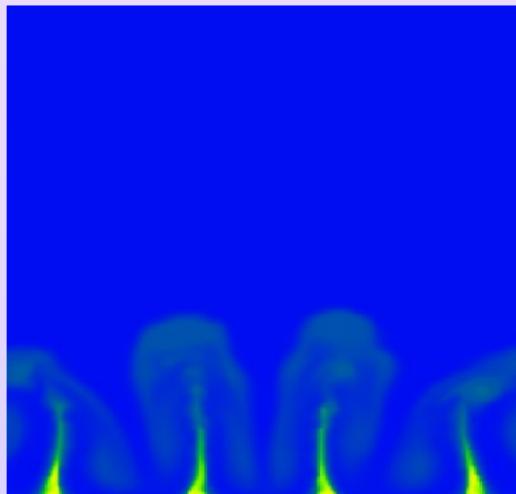
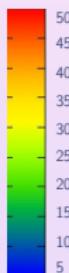


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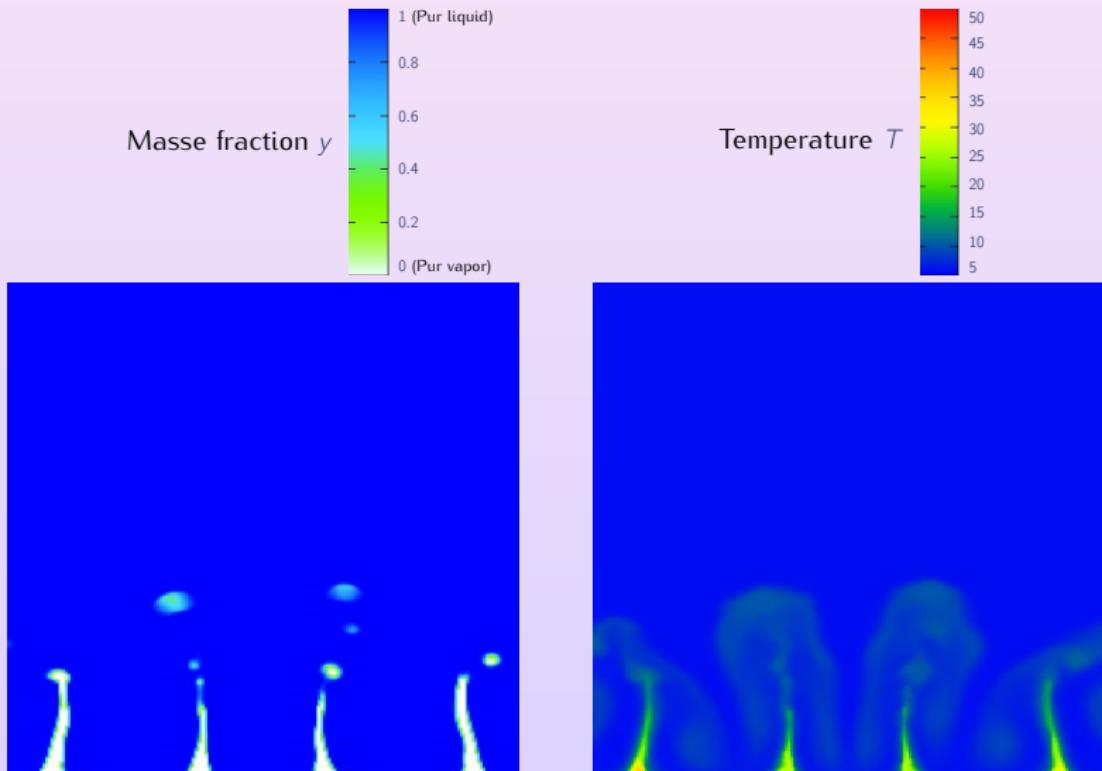
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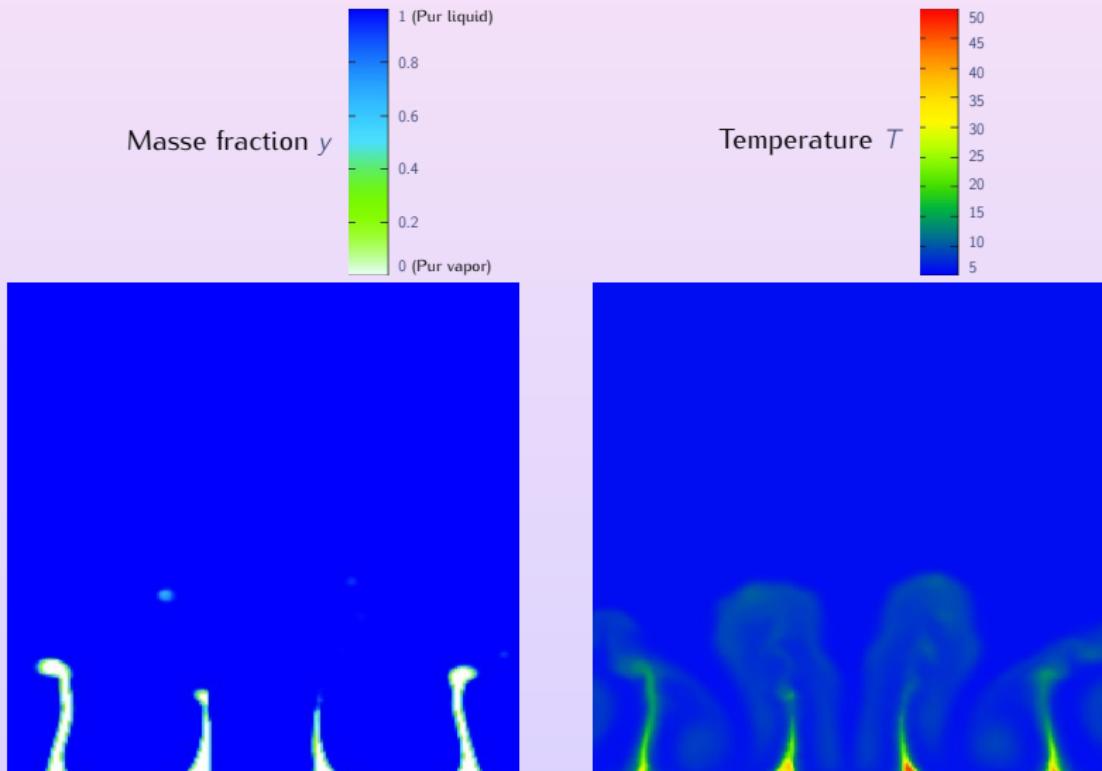


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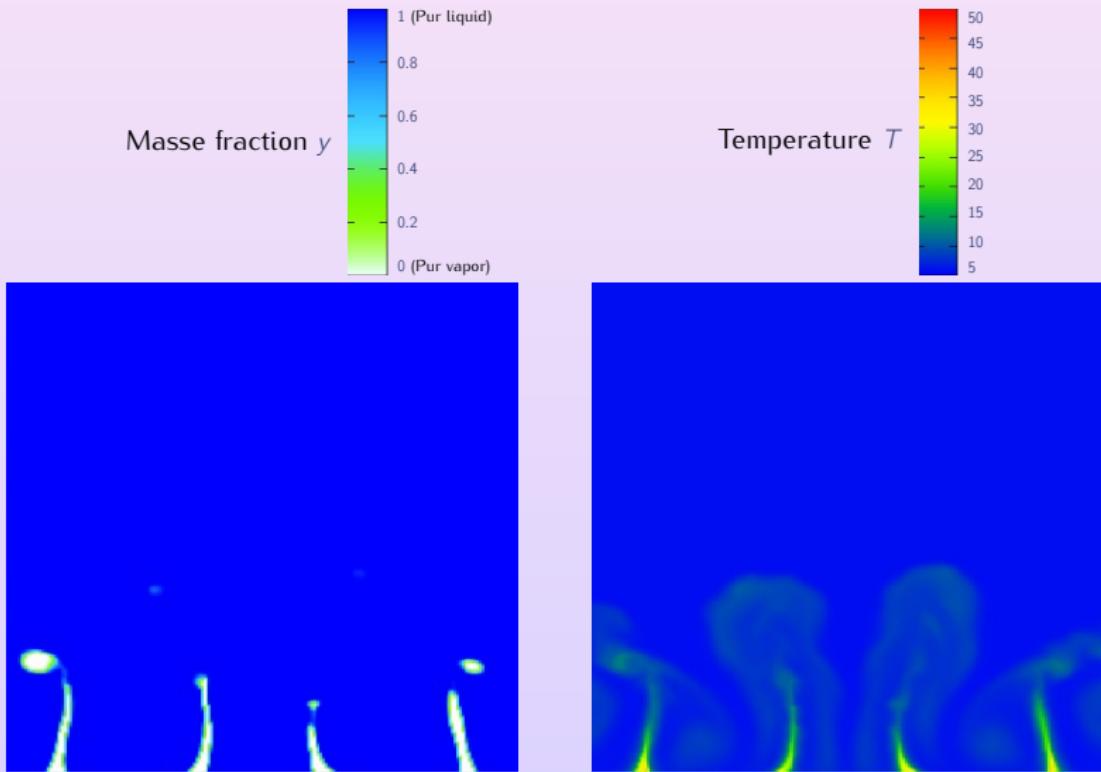


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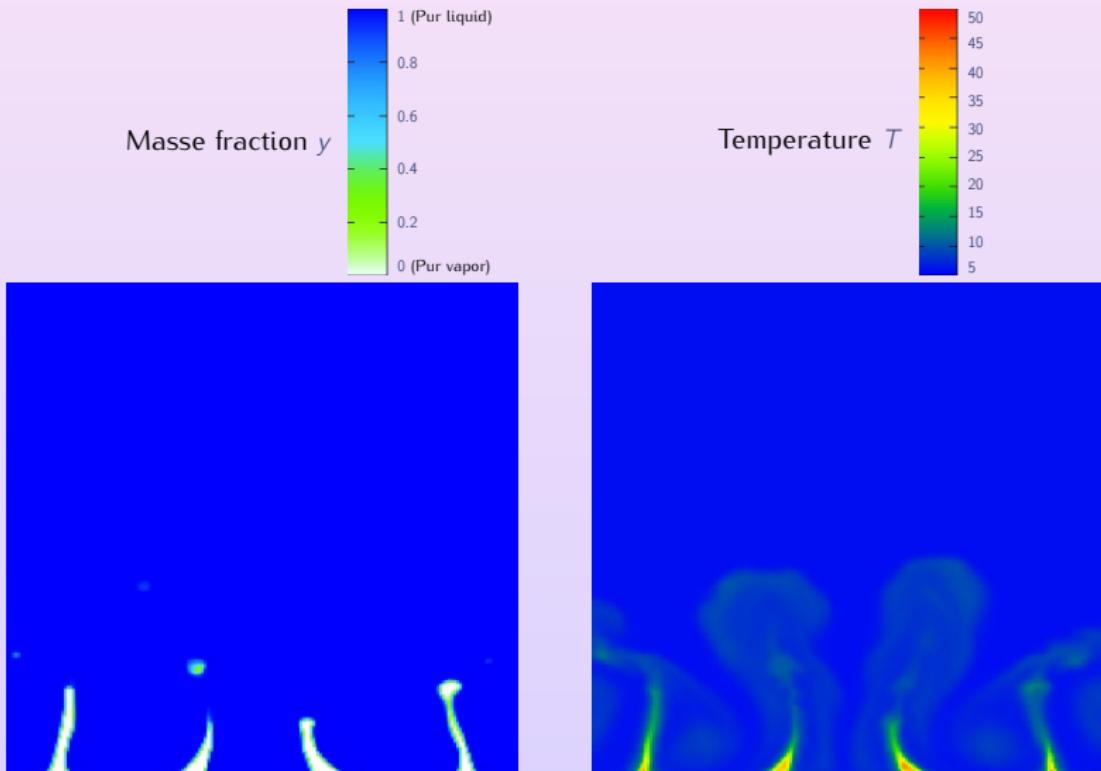


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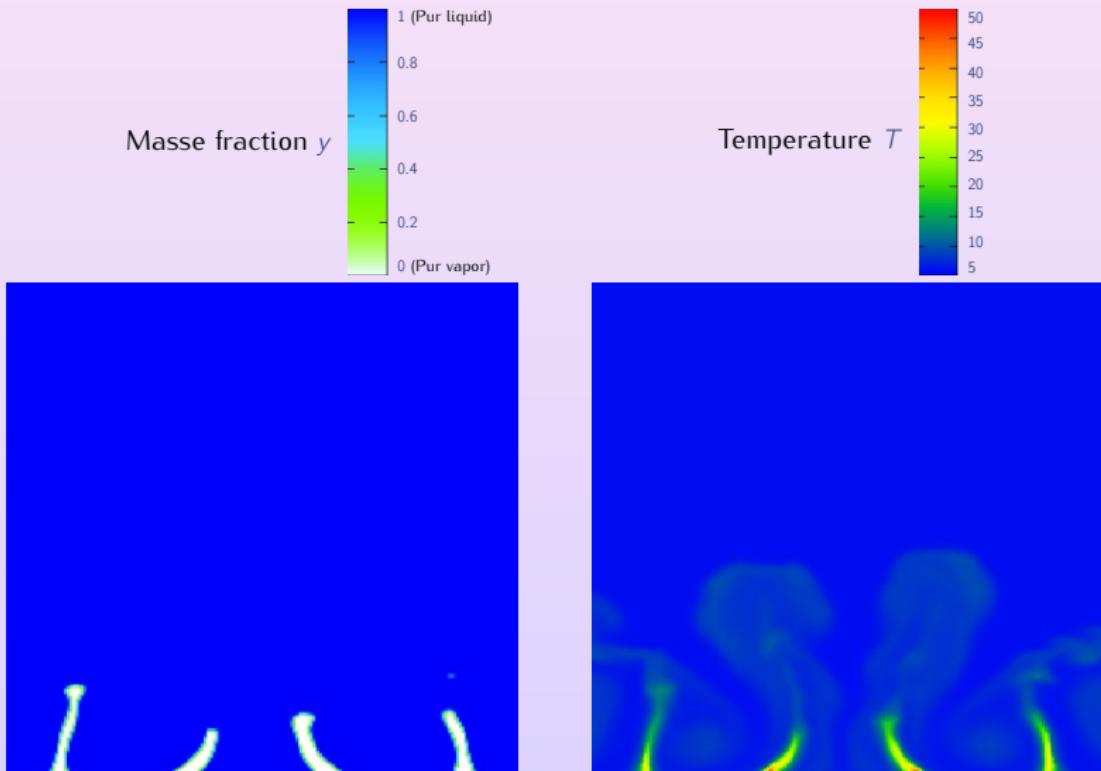


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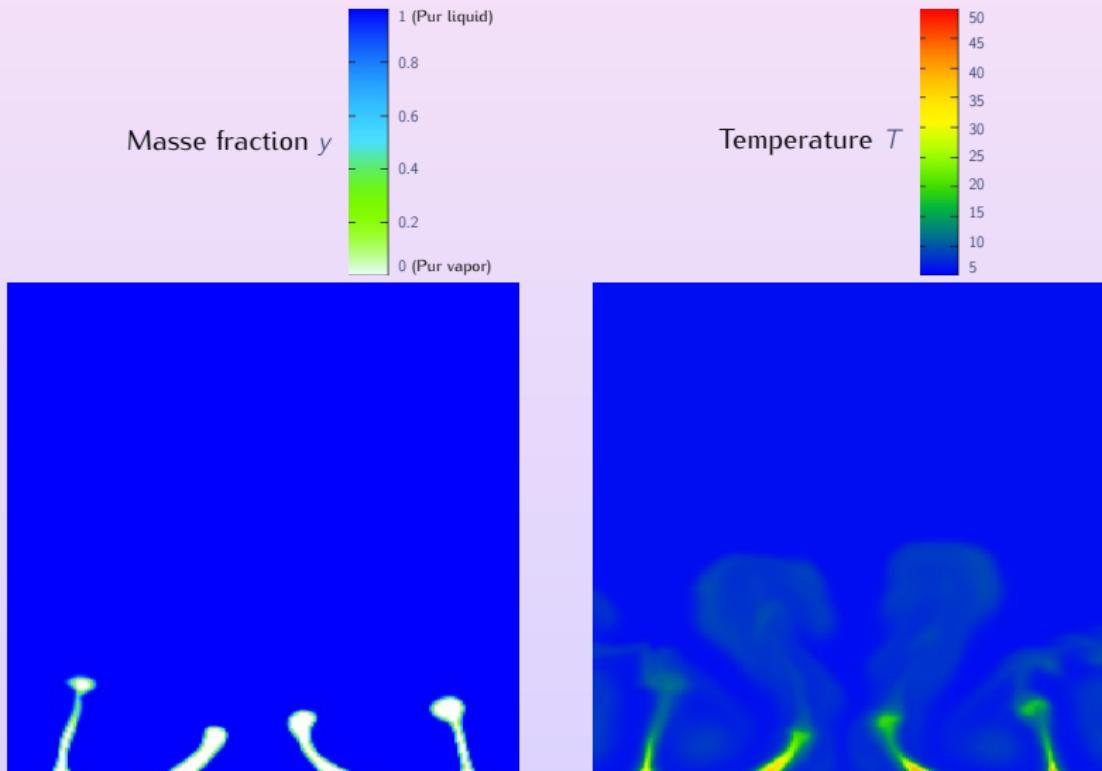


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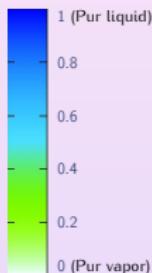
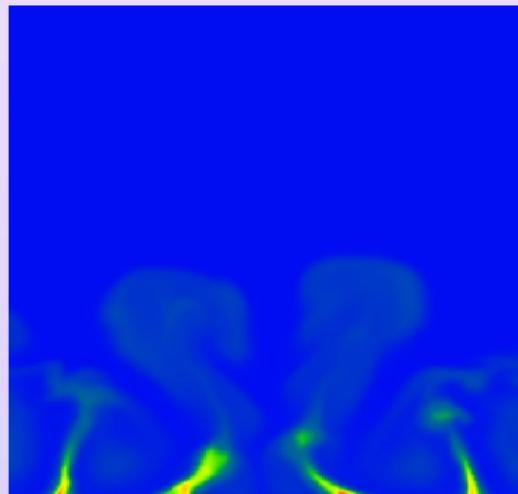
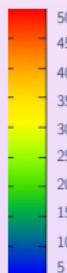


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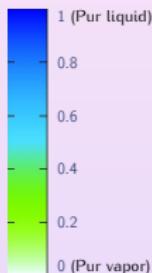
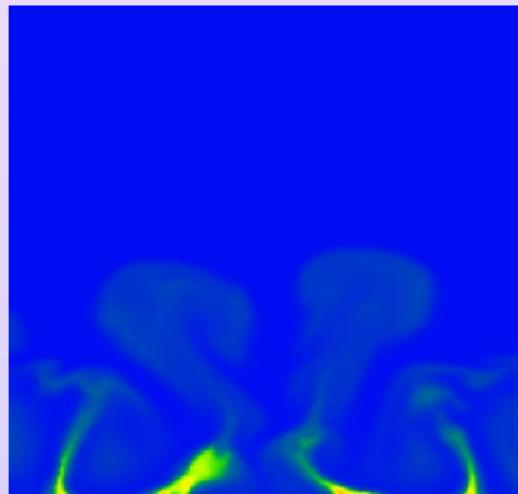
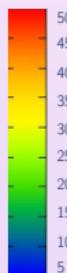
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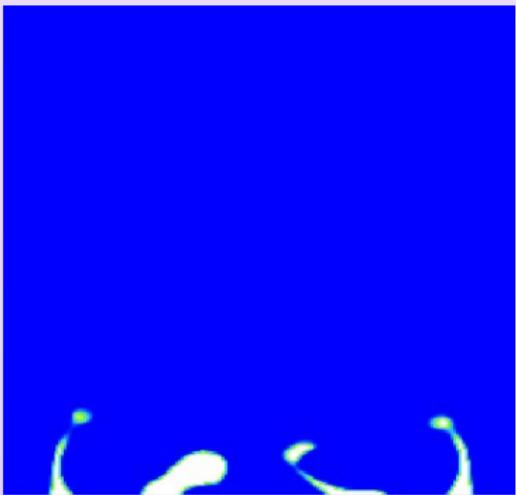
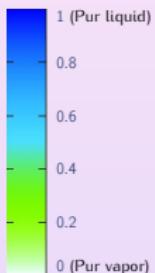
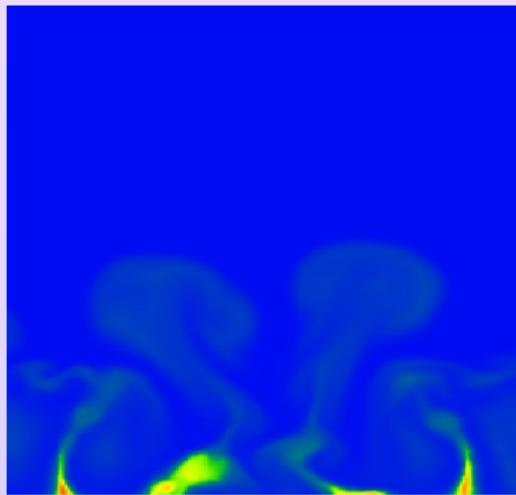
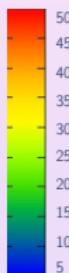
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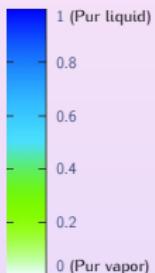
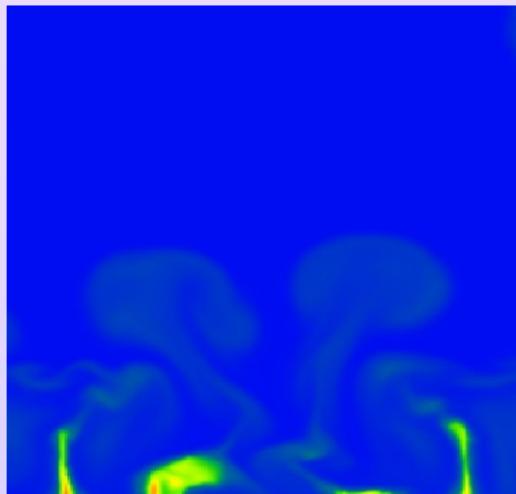
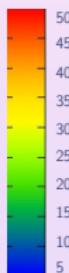
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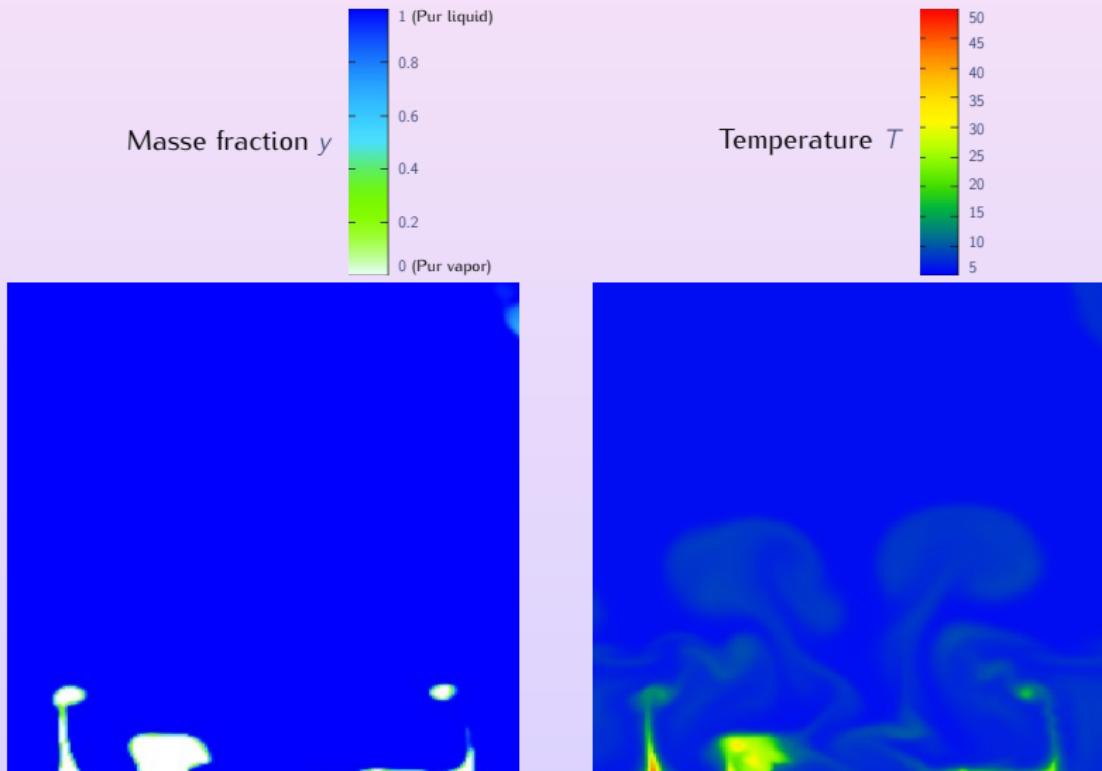
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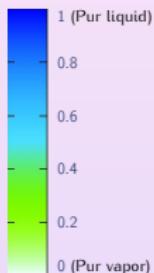
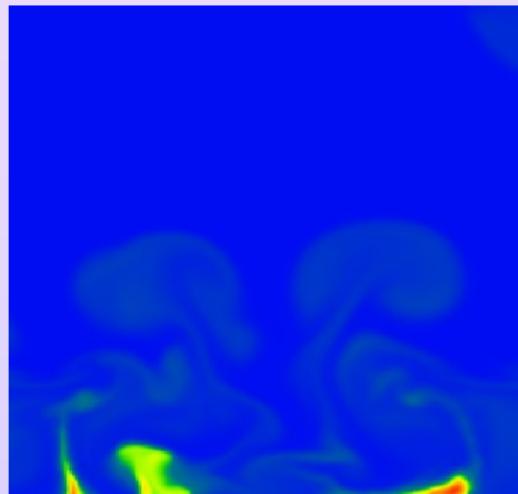
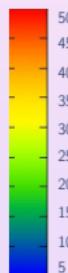


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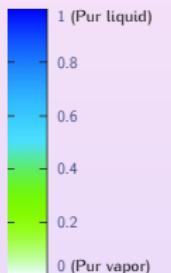
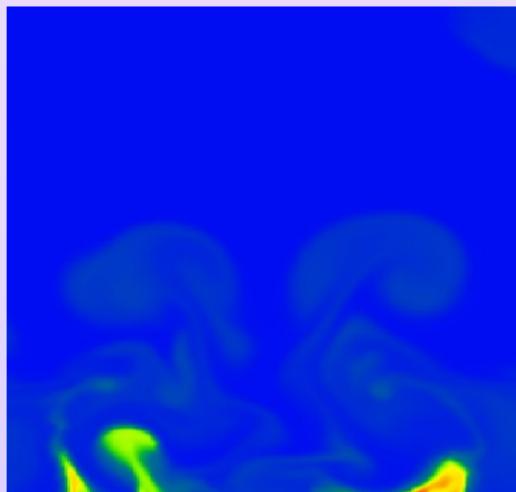
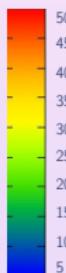
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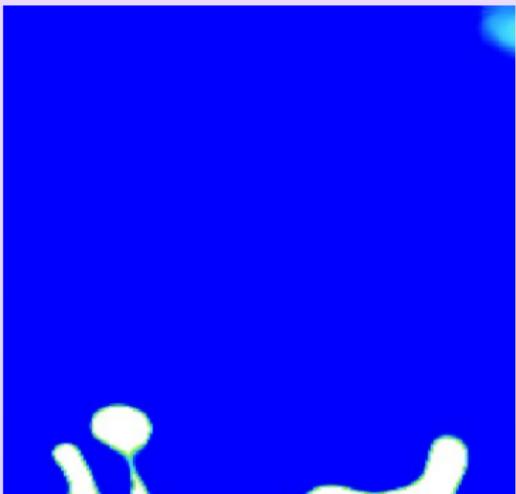
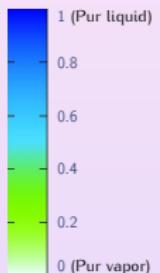
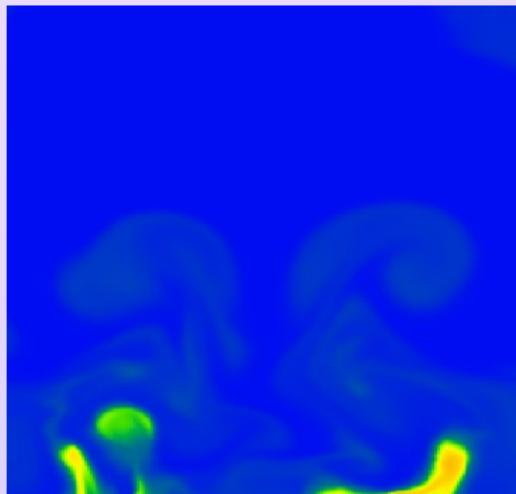
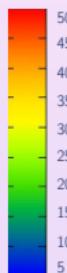
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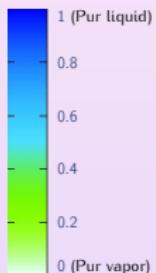
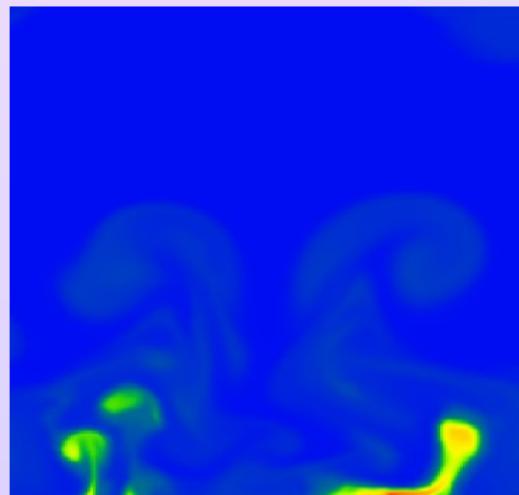
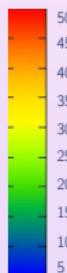
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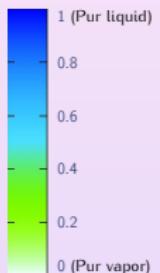
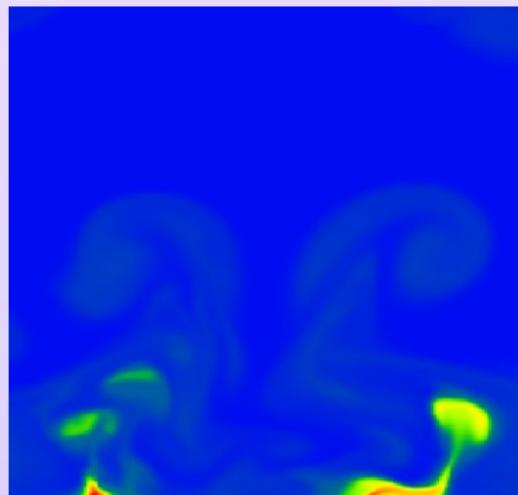
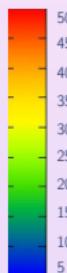
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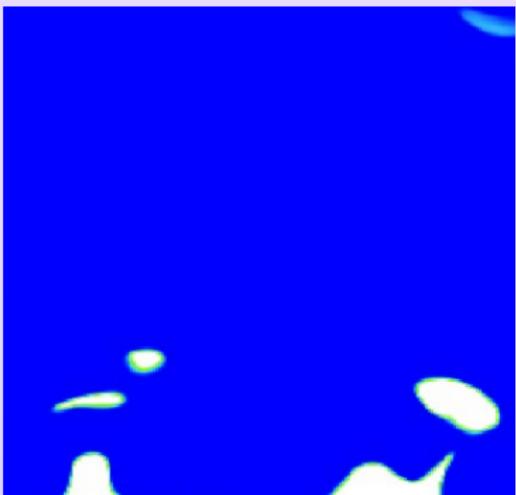
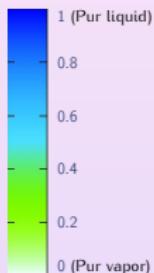
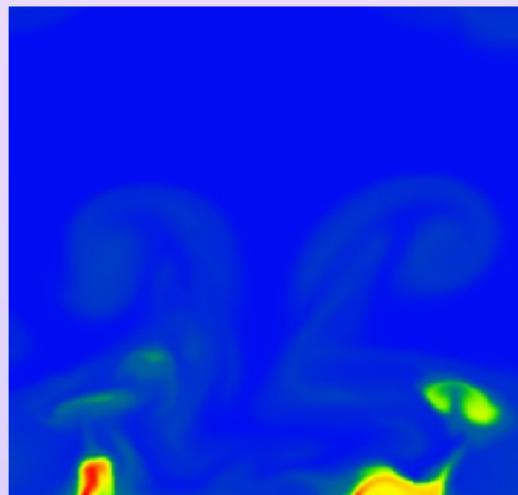
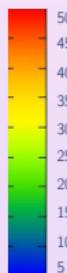
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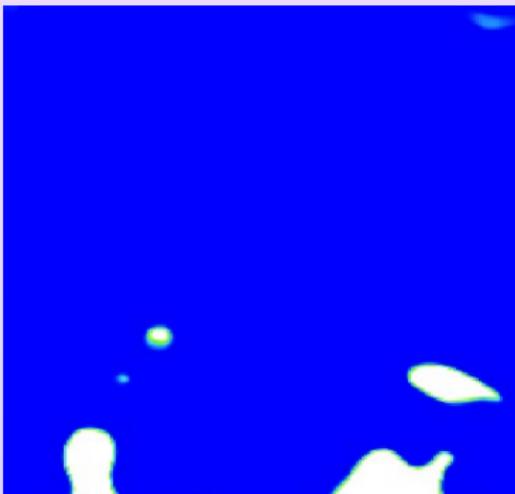
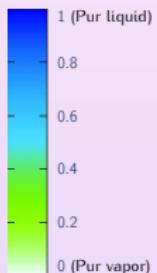
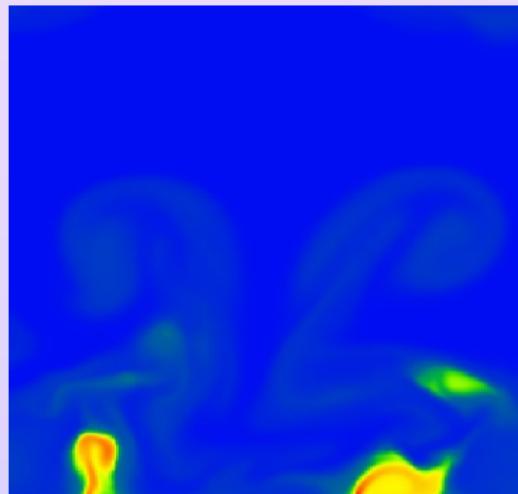
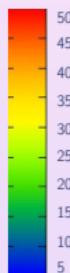
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OUTLINE

1 Context

2 Model

- Governing equations
- Equation of State

3 Numerical Approximation and Example

- Conservation Laws
- Numerical Scheme
- Numerical Example

4 Conclusion

SUMMARY & PERSPECTIVES

• Model

- ✓ based on a general construction of the Equilibrium EOS (also for tabulated data),
- Numerical Method based on the relaxation approach: off-equilibrium systems with relaxation terms
 - ✓ preliminary results: dynamic generation of a phase in a 2D-flow in a pure phase with surface tension, gravity and heat diffusion,
 - ✓ transition: liquid phase → nucleating boiling → "film" boiling

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- ✓ transition: liquid phase → nucleating boiling → “film” boiling
- ✗ quantitative simulations: tabulated EOS for pure phases, implicit transport step or Adam-Bashfort refinement (CFL condition), 3D (parallelization).

APPENDIX

- ▶ From $\mathbf{w} \mapsto s^{\text{eq}}$ to $\mathbf{w} \mapsto P^{\text{eq}}$
- ▶ Projection step with analytical EOS
- ▶ Projection step with tabulated EOS
- ▶ Stiffened Gas for Water
- ▶ Tabulated EOS for Water
- ▶ Isentropic Curves
- ▶ Surface Tension
- ▶ Metastability
- ▶ Critical Point
- ▶ Summary & To Do

FROM $\mathbf{w} \mapsto s^{\text{eq}}$ TO $\mathbf{w} \mapsto P^{\text{eq}}$

For all $\tilde{\mathbf{w}}$ fixed, we seek $(\mathbf{w}_{\text{liq}}^*, \mathbf{w}_{\text{vap}}^*, y^*)$ as the solution of the system

$$\begin{cases} P_{\text{liq}}(\mathbf{w}_{\text{liq}}) = P_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ T_{\text{liq}}(\mathbf{w}_{\text{liq}}) = T_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ g_{\text{liq}}(\mathbf{w}_{\text{liq}}) = g_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ \tilde{\mathbf{w}} = y\mathbf{w}_{\text{liq}} + (1 - y)\mathbf{w}_{\text{vap}} \end{cases}$$

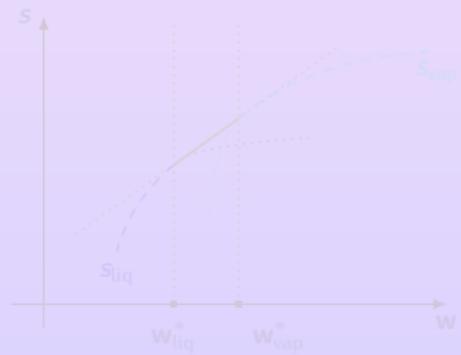
- if $y^* \in]0, 1[$ then $\tilde{\mathbf{w}}$ is an equilibrium mixture state

$$s^{\text{eq}}(\tilde{\mathbf{w}}) = y^* s_{\text{liq}}(\mathbf{w}_{\text{liq}}^*) + (1 - y^*) s_{\text{vap}}(\mathbf{w}_{\text{vap}}^*),$$

- if the system has no solution or $y^* \notin]0, 1[$ then $\tilde{\mathbf{w}}$ is a monophasic pure state

$$s^{\text{eq}}(\tilde{\mathbf{w}}) = \max\{s_{\text{liq}}(\tilde{\mathbf{w}}), s_{\text{vap}}(\tilde{\mathbf{w}})\},$$

$$P^{\text{eq}}(\mathbf{w}) = P_{\text{liq}}(\mathbf{w})$$



FROM $\mathbf{w} \mapsto s^{\text{eq}}$ TO $\mathbf{w} \mapsto P^{\text{eq}}$

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- ① if $y^* \in]0, 1[$ then $\tilde{\mathbf{w}}$ is an **equilibrium mixture state**

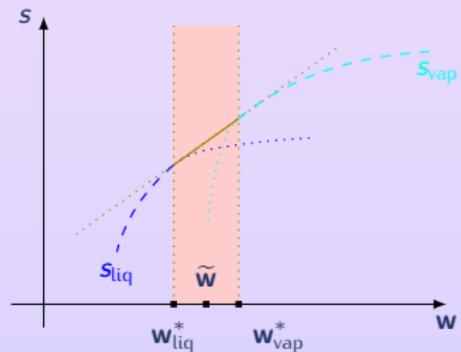
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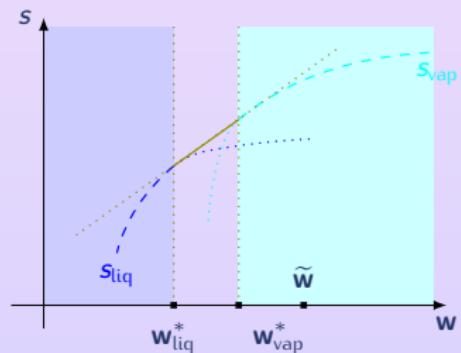
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FROM $\mathbf{w} \mapsto s^{\text{eq}}$ TO $\mathbf{w} \mapsto P^{\text{eq}}$

For all $\tilde{\mathbf{w}}$ fixed, we seek $(\mathbf{w}_{\text{liq}}^*, \mathbf{w}_{\text{vap}}^*, y^*)$ as the solution of the system

$$\begin{cases} P_{\text{liq}}(\mathbf{w}_{\text{liq}}) = P_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ T_{\text{liq}}(\mathbf{w}_{\text{liq}}) = T_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ g_{\text{liq}}(\mathbf{w}_{\text{liq}}) = g_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ \tilde{\mathbf{w}} = y\mathbf{w}_{\text{liq}} + (1 - y)\mathbf{w}_{\text{vap}} \end{cases}$$

- ① if $y^* \in]0, 1[$ then $\tilde{\mathbf{w}}$ is an **equilibrium mixture state**

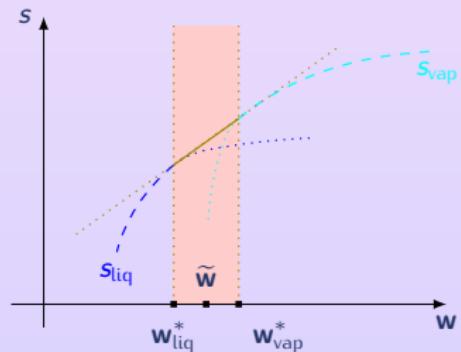
$$s^{\text{eq}}(\tilde{\mathbf{w}}) = y^* s_{\text{liq}}(\mathbf{w}_{\text{liq}}^*) + (1 - y^*) s_{\text{vap}}(\mathbf{w}_{\text{vap}}^*),$$

$$P^{\text{eq}}(\tilde{\mathbf{w}}) = P_{\text{liq}}(\mathbf{w}_{\text{liq}}^*) = P_{\text{vap}}(\mathbf{w}_{\text{vap}}^*);$$

- ② if the system has no solution or $y^* \notin]0, 1[$ then $\tilde{\mathbf{w}}$ is a **monophasic pure state**

$$s^{\text{eq}}(\tilde{\mathbf{w}}) = \max\{s_{\text{liq}}(\tilde{\mathbf{w}}), s_{\text{vap}}(\tilde{\mathbf{w}})\},$$

$$P^{\text{eq}}(\tilde{\mathbf{w}}) = P_\alpha(\tilde{\mathbf{w}}).$$



FROM $\mathbf{w} \mapsto s^{\text{eq}}$ TO $\mathbf{w} \mapsto P^{\text{eq}}$

For all $\tilde{\mathbf{w}}$ fixed, we seek $(\mathbf{w}_{\text{liq}}^*, \mathbf{w}_{\text{vap}}^*, y^*)$ as the solution of the system

$$\begin{cases} P_{\text{liq}}(\mathbf{w}_{\text{liq}}) = P_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ T_{\text{liq}}(\mathbf{w}_{\text{liq}}) = T_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ g_{\text{liq}}(\mathbf{w}_{\text{liq}}) = g_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ \tilde{\mathbf{w}} = y\mathbf{w}_{\text{liq}} + (1 - y)\mathbf{w}_{\text{vap}} \end{cases}$$

- ① if $y^* \in]0, 1[$ then $\tilde{\mathbf{w}}$ is an **equilibrium mixture state**

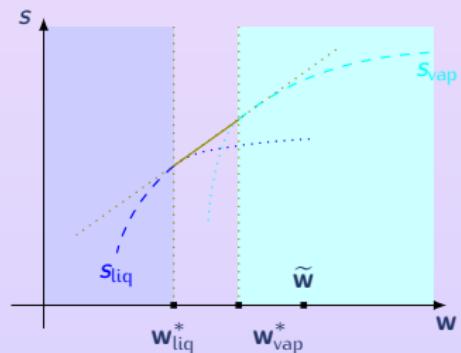
$$s^{\text{eq}}(\tilde{\mathbf{w}}) = y^* s_{\text{liq}}(\mathbf{w}_{\text{liq}}^*) + (1 - y^*) s_{\text{vap}}(\mathbf{w}_{\text{vap}}^*),$$

$$P^{\text{eq}}(\tilde{\mathbf{w}}) = P_{\text{liq}}(\mathbf{w}_{\text{liq}}^*) = P_{\text{vap}}(\mathbf{w}_{\text{vap}}^*);$$

- ② if the system has no solution or $y^* \notin]0, 1[$ then $\tilde{\mathbf{w}}$ is a **monophasic pure state**

$$s^{\text{eq}}(\tilde{\mathbf{w}}) = \max\{s_{\text{liq}}(\tilde{\mathbf{w}}), s_{\text{vap}}(\tilde{\mathbf{w}})\},$$

$$P^{\text{eq}}(\tilde{\mathbf{w}}) = P_\alpha(\tilde{\mathbf{w}}).$$



PROJECTION STEP: ANALYTICAL EOS

(τ, ε) fixed

$(\tau_{\text{liq}}, \varepsilon_{\text{liq}}, \tau_{\text{vap}}, \varepsilon_{\text{vap}}, y)$ SOLUTION OF

$$\begin{cases} P_{\text{liq}}(\tau_{\text{liq}}, \varepsilon_{\text{liq}}) = P_{\text{vap}}(\tau_{\text{vap}}, \varepsilon_{\text{vap}}) \\ T_{\text{liq}}(\tau_{\text{liq}}, \varepsilon_{\text{liq}}) = T_{\text{vap}}(\tau_{\text{vap}}, \varepsilon_{\text{vap}}) \\ g_{\text{liq}}(\tau_{\text{liq}}, \varepsilon_{\text{liq}}) = g_{\text{vap}}(\tau_{\text{vap}}, \varepsilon_{\text{vap}}) \\ \tau = y\tau_{\text{liq}} + (1-y)\tau_{\text{vap}} \\ \varepsilon = y\varepsilon_{\text{liq}} + (1-y)\varepsilon_{\text{vap}} \end{cases}$$

(P, T) SOLUTION OF

$$\begin{cases} \tau_\alpha = \tau_\alpha(P, T) \\ \varepsilon_\alpha = \varepsilon_\alpha(P, T) \\ g_{\text{liq}}(P, T) = g_{\text{vap}}(P, T) \\ y = \frac{\tau - \tau_{\text{vap}}(P, T)}{\tau_{\text{liq}}(P, T) - \tau_{\text{vap}}(P, T)} = \frac{\varepsilon - \varepsilon_{\text{vap}}(P, T)}{\varepsilon_{\text{liq}}(P, T) - \varepsilon_{\text{vap}}(P, T)} \end{cases}$$

$T \mapsto P = P^{\text{sat}}(T) \approx P^{\text{sat}}(T)$

T SOLUTION OF

$$\frac{\tau - \tau_{\text{vap}}^{\text{sat}}(T)}{\tau_{\text{liq}}^{\text{sat}}(T) - \tau_{\text{vap}}^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_{\text{vap}}^{\text{sat}}(T)}{\varepsilon_{\text{liq}}^{\text{sat}}(T) - \varepsilon_{\text{vap}}^{\text{sat}}(T)} \quad \text{where } \left(\frac{\tau}{\varepsilon}\right)_\alpha^{\text{sat}}(T) \stackrel{\text{def}}{=} \left(\frac{\tau}{\varepsilon}\right)_\alpha(P^{\text{sat}}(T), T)$$

PROJECTION STEP: ANALYTICAL EOS

(τ, ε) fixed

$(\tau_{\text{liq}}, \varepsilon_{\text{liq}}, \tau_{\text{vap}}, \varepsilon_{\text{vap}}, y)$ SOLUTION OF

$$\begin{cases} P_{\text{liq}}(\tau_{\text{liq}}, \varepsilon_{\text{liq}}) = P_{\text{vap}}(\tau_{\text{vap}}, \varepsilon_{\text{vap}}) \\ T_{\text{liq}}(\tau_{\text{liq}}, \varepsilon_{\text{liq}}) = T_{\text{vap}}(\tau_{\text{vap}}, \varepsilon_{\text{vap}}) \\ g_{\text{liq}}(\tau_{\text{liq}}, \varepsilon_{\text{liq}}) = g_{\text{vap}}(\tau_{\text{vap}}, \varepsilon_{\text{vap}}) \\ \tau = y\tau_{\text{liq}} + (1-y)\tau_{\text{vap}} \\ \varepsilon = y\varepsilon_{\text{liq}} + (1-y)\varepsilon_{\text{vap}} \end{cases}$$

(P, T) SOLUTION OF

$$\begin{cases} \tau_\alpha = \tau_\alpha(P, T) \\ \varepsilon_\alpha = \varepsilon_\alpha(P, T) \\ g_{\text{liq}}(P, T) = g_{\text{vap}}(P, T) \\ y = \frac{\tau - \tau_{\text{vap}}(P, T)}{\tau_{\text{liq}}(P, T) - \tau_{\text{vap}}(P, T)} = \frac{\varepsilon - \varepsilon_{\text{vap}}(P, T)}{\varepsilon_{\text{liq}}(P, T) - \varepsilon_{\text{vap}}(P, T)} \end{cases}$$

$T \mapsto P = \hat{P}^{\text{sat}}(T) \approx P^{\text{sat}}(T)$

T SOLUTION OF

$$\frac{\tau - \tau_{\text{vap}}^{\text{sat}}(T)}{\tau_{\text{liq}}^{\text{sat}}(T) - \tau_{\text{vap}}^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_{\text{vap}}^{\text{sat}}(T)}{\varepsilon_{\text{liq}}^{\text{sat}}(T) - \varepsilon_{\text{vap}}^{\text{sat}}(T)} \quad \text{where } \left(\frac{\tau}{\varepsilon}\right)_\alpha^{\text{sat}}(T) \stackrel{\text{def}}{=} \left(\frac{\tau}{\varepsilon}\right)_\alpha(\hat{P}^{\text{sat}}(T), T)$$

PROJECTION STEP: TABULATED EOS

T (K)	P^{sat} (MPa)	Volume $(\text{m}^3 \text{kg}^{-1})$		Internal Energy (kJ kg^{-1})	
		$\tau_{\text{liq}}^{\text{sat}}$	$\tau_{\text{vap}}^{\text{sat}}$	$\varepsilon_{\text{liq}}^{\text{sat}}$	$\varepsilon_{\text{vap}}^{\text{sat}}$
275	0,00069845	0,0010001	181,60	7,7590	2377,5
278	0,00086349	0,0010001	148,48	20,388	2381,6
281	0,0010621	0,0010002	122,01	32,996	2385,7
284	0,0012999	0,0010004	100,74	45,586	2389,8
287	0,0015835	0,0010008	83,560	58,162	2393,9
290	0,0019200	0,0010012	69,625	70,727	2398,0
293	0,0023177	0,0010018	58,267	83,284	2402,1
296	0,0027856	0,0010025	48,966	95,835	2406,2
299	0,0033342	0,0010032	41,318	108,38	2410,3
302	0,0039745	0,0010041	35,002	120,92	2414,4
305	0,0047193	0,0010050	29,764	133,46	2418,4
308	0,0055825	0,0010060	25,403	146	2422,5
...

Source: <http://webbook.nist.gov/chemistry/fluid/>

PROJECTION STEP: TABULATED EOS

(τ, ε) fixed

T SOLUTION OF

$$\frac{\tau - \tau_{\text{vap}}^{\text{sat}}(T)}{\tau_{\text{liq}}^{\text{sat}}(T) - \tau_{\text{vap}}^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_{\text{vap}}^{\text{sat}}(T)}{\varepsilon_{\text{liq}}^{\text{sat}}(T) - \varepsilon_{\text{vap}}^{\text{sat}}(T)} \quad \text{with} \quad \left(\begin{matrix} \tau \\ \varepsilon \end{matrix}\right)_{\alpha}^{\text{sat}}(T) \quad \text{tabulated}$$

2

$$\frac{\tau - \hat{\tau}_{\text{vap}}^{\text{sat}}(T)}{\hat{\tau}_{\text{liq}}^{\text{sat}}(T) - \hat{\tau}_{\text{vap}}^{\text{sat}}(T)} = \frac{\varepsilon - \hat{\varepsilon}_{\text{vap}}^{\text{sat}}(T)}{\hat{\varepsilon}_{\text{liq}}^{\text{sat}}(T) - \hat{\varepsilon}_{\text{vap}}^{\text{sat}}(T)} \quad \text{with} \quad \left(\begin{matrix} \hat{\tau} \\ \hat{\varepsilon} \end{matrix}\right)_{\alpha}^{\text{sat}}(T)$$

PROJECTION STEP: TABULATED EOS

(τ, ε) fixed

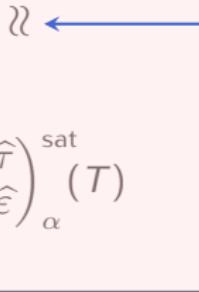
T SOLUTION OF

$$\frac{\tau - \tau_{\text{vap}}^{\text{sat}}(T)}{\tau_{\text{liq}}^{\text{sat}}(T) - \tau_{\text{vap}}^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_{\text{vap}}^{\text{sat}}(T)}{\varepsilon_{\text{liq}}^{\text{sat}}(T) - \varepsilon_{\text{vap}}^{\text{sat}}(T)}$$

with $\begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(T)$ tabulated

$$\frac{\tau - \hat{\tau}_{\text{vap}}^{\text{sat}}(T)}{\hat{\tau}_{\text{liq}}^{\text{sat}}(T) - \hat{\tau}_{\text{vap}}^{\text{sat}}(T)} = \frac{\varepsilon - \hat{\varepsilon}_{\text{vap}}^{\text{sat}}(T)}{\hat{\varepsilon}_{\text{liq}}^{\text{sat}}(T) - \hat{\varepsilon}_{\text{vap}}^{\text{sat}}(T)}$$

with $\begin{pmatrix} \hat{\tau} \\ \hat{\varepsilon} \end{pmatrix}_{\alpha}^{\text{sat}}(T)$



least square
approximations

PROJECTION STEP: TABULATED EOS

(τ, ε) fixed

T SOLUTION OF

$$\frac{\tau - \tau_{\text{vap}}^{\text{sat}}(T)}{\tau_{\text{liq}}^{\text{sat}}(T) - \tau_{\text{vap}}^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_{\text{vap}}^{\text{sat}}(T)}{\varepsilon_{\text{liq}}^{\text{sat}}(T) - \varepsilon_{\text{vap}}^{\text{sat}}(T)} \quad \text{with} \quad \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(T) \quad \text{tabulated}$$

$$\frac{\tau - \hat{\tau}_{\text{vap}}^{\text{sat}}(T)}{\hat{\tau}_{\text{liq}}^{\text{sat}}(T) - \hat{\tau}_{\text{vap}}^{\text{sat}}(T)} = \frac{\varepsilon - \hat{\varepsilon}_{\text{vap}}^{\text{sat}}(T)}{\hat{\varepsilon}_{\text{liq}}^{\text{sat}}(T) - \hat{\varepsilon}_{\text{vap}}^{\text{sat}}(T)} \quad \text{with} \quad \begin{pmatrix} \hat{\tau} \\ \hat{\varepsilon} \end{pmatrix}_{\alpha}^{\text{sat}}(T)$$

least square
approximations

STIFFENED GAS FOR WATER

Phase	c_v [J kg $^{-1}$ K $^{-1}$]	γ	π [Pa]	q [J kg $^{-1}$]	m [J kg $^{-1}$ K $^{-1}$]
Water	1816.2	2.35	10^9	-1167.056×10^3	-32765.55596
Steam	1040.14	1.43	0	2030.255×10^3	-33265.65947

Table: Parameters proposed by [O. LE METAYER] for water.

$$(\tau_\alpha, \varepsilon_\alpha) \mapsto s_\alpha = c_{v_\alpha} \ln(\varepsilon_\alpha - q_\alpha - \pi_\alpha \tau_\alpha) + c_{v_\alpha} (\gamma_\alpha - 1) \ln \tau_\alpha + m_\alpha$$

$$(P, T) \mapsto \varepsilon_\alpha = c_{v_\alpha} T \frac{P + \pi_\alpha \gamma_\alpha}{P + \pi_\alpha} + q_\alpha, \quad (P, T) \mapsto \tau_\alpha = c_{v_\alpha} (\gamma_\alpha - 1) \frac{T}{P + \pi_\alpha}.$$

$$\left. \begin{array}{l} T^i = 278 \text{ K} \dots 610 \text{ K}, \\ g_{\text{liq}}(P, T^i) = g_{\text{vap}}(P, T^i) \Rightarrow P^{\text{sat}}(T^i) \end{array} \right\} \Rightarrow \mathfrak{A} = \{(T^i, P^{\text{sat}}(T^i))\}_{i=0}^{83}$$

\hat{P}^{sat} defined by using a least square approximation of \mathfrak{A} :

$$T \mapsto P^{\text{sat}}(T) \approx \hat{P}^{\text{sat}}(T) \stackrel{\text{def}}{=} \exp \left(\sum_{k=-8}^{k=8} a_k T^k \right)$$

STIFFENED GAS FOR WATER

Phase	c_v [J kg $^{-1}$ K $^{-1}$]	γ	π [Pa]	q [J kg $^{-1}$]	m [J kg $^{-1}$ K $^{-1}$]
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STIFFENED GAS FOR WATER

Phase	c_v [J kg ⁻¹ K ⁻¹]	γ	π [Pa]	q [J kg ⁻¹]	m [J kg ⁻¹ K ⁻¹]
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\hat{P}^{sat} defined by using a least square approximation of \mathfrak{A} :

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STIFFENED GAS FOR WATER

Phase	c_v [J kg ⁻¹ K ⁻¹]	γ	π [Pa]	q [J kg ⁻¹]	m [J kg ⁻¹ K ⁻¹]
Water	1816.2	2.35	10^9	-1167.056×10^3	-32765.55596
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\hat{P}^{sat} defined by using a least square approximation of \mathfrak{A} :

$$T \mapsto P^{\text{sat}}(T) \approx \hat{P}^{\text{sat}}(T) \stackrel{\text{def}}{=} \exp \left(\sum_{k=-8}^{k=8} a_k T^k \right)$$

WATER TABULATED EOS

$$T^i = 278 \text{ K} \dots 610 \text{ K}, \quad \varepsilon_\alpha^{\text{sat}}(T^i), \tau_\alpha^{\text{sat}}(T^i) \text{ found in the tables} \quad \left\{ \begin{array}{l} \mathfrak{A} = \left\{ \left(T_i, \frac{1}{\varepsilon_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{B} = \left\{ \left(T_i, \frac{\varepsilon_{\text{liq}}^{\text{sat}}(T_i)}{\varepsilon_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{C} = \left\{ \left(T_i, \frac{1}{\tau_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{D} = \left\{ \left(T_i, \frac{\tau_{\text{liq}}^{\text{sat}}(T_i)}{\tau_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \end{array} \right.$$

$\hat{\varepsilon}_\alpha^{\text{sat}}$ and $\hat{\tau}_\alpha^{\text{sat}}$ defined by using a least square approximation of \mathfrak{A} , \mathfrak{B} , \mathfrak{C} and \mathfrak{D} :

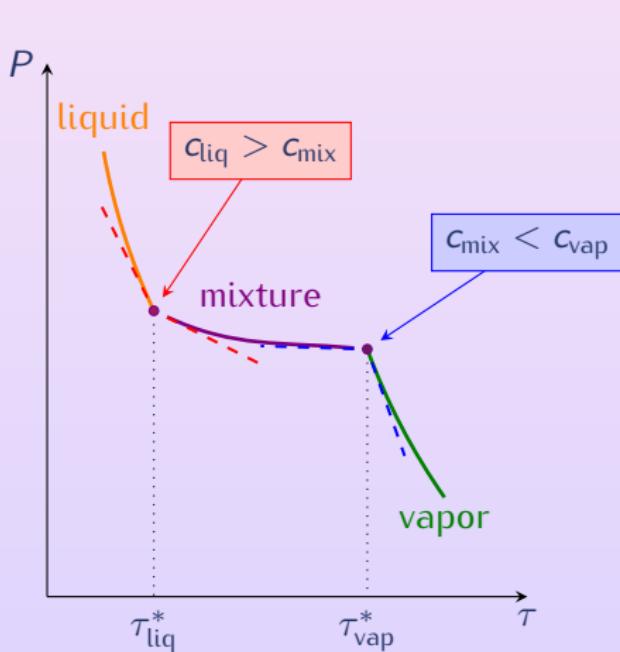
$$T \mapsto \varepsilon_{\text{vap}}^{\text{sat}} \approx \hat{\varepsilon}_{\text{vap}}^{\text{sat}} \stackrel{\text{def}}{=} \frac{1}{\sum_{k=0}^6 a_k T^k}$$

$$T \mapsto \tau_{\text{vap}}^{\text{sat}} \approx \hat{\tau}_{\text{vap}}^{\text{sat}} \stackrel{\text{def}}{=} \frac{1}{\sum_{k=0}^8 c_k T^k}$$

$$T \mapsto \varepsilon_{\text{liq}}^{\text{sat}} \approx \hat{\varepsilon}_{\text{liq}}^{\text{sat}} \stackrel{\text{def}}{=} \hat{\varepsilon}_{\text{vap}}^{\text{sat}}(T) \sum_{k=0}^6 b_k T^k$$

$$T \mapsto \tau_{\text{liq}}^{\text{sat}} \approx \hat{\tau}_{\text{liq}}^{\text{sat}} \stackrel{\text{def}}{=} \hat{\tau}_{\text{vap}}^{\text{sat}}(T) \sum_{k=0}^9 d_k T^k$$

ISENTROPIC CURVES



$$\gamma \stackrel{\text{def}}{=} -\frac{\tau}{P} \left. \frac{\partial P}{\partial \tau} \right|_s$$

$$\Gamma \stackrel{\text{def}}{=} \tau \left. \frac{\partial P}{\partial \varepsilon} \right|_\tau$$

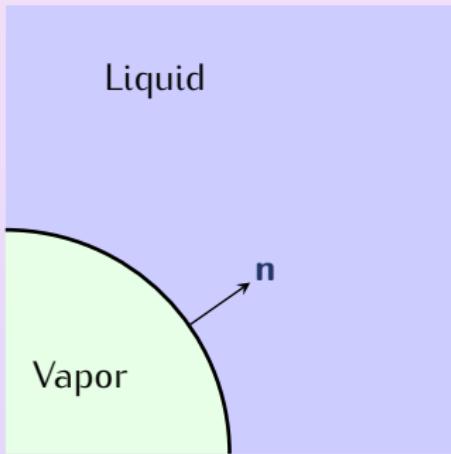
$$\mathfrak{G} \stackrel{\text{def}}{=} \frac{\tau^2}{2\gamma P} \left. \frac{\partial^2 P}{\partial \tau^2} \right|_s$$

- Regularity: [J. CORREIA, P.G. LEFLOCH, M.D. THANH]
- Loss of convexity: [A. Voss]

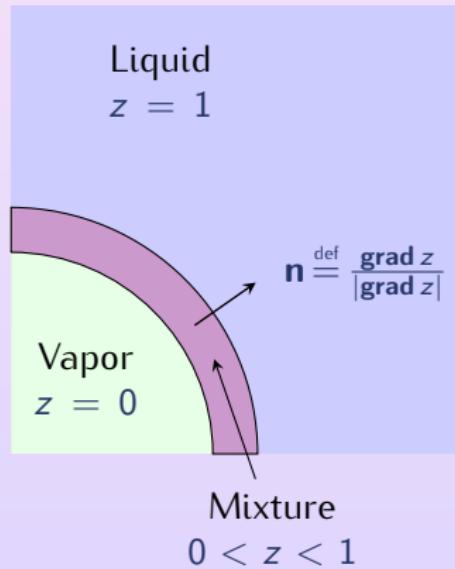
- Pure Phases
 - (H) $\gamma > 0$
 - (H) $\Gamma > 0$
 - (H) $\mathfrak{G} > 0$
- Mixture
 - (P) $\gamma > 0$
 - (P) $\Gamma > 0$
 - (H) $\mathfrak{G} > 0$

CONTINUUM SURFACE FORCE (CSF) APPROACH

Physical Interface



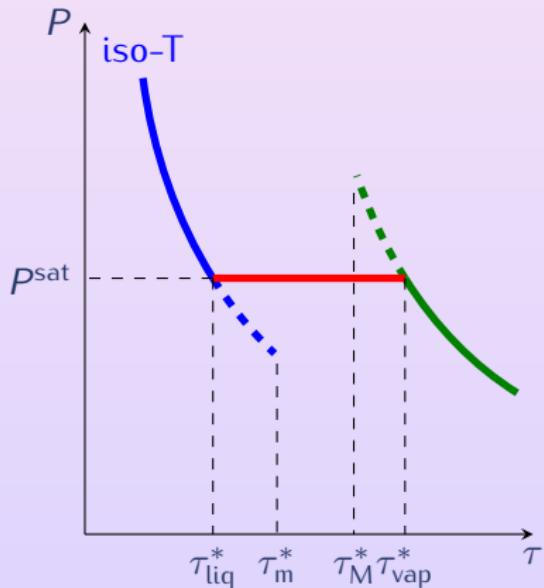
Diffuse Interface



$$\Pi_{\text{tension}} = -\sigma \operatorname{div}(\mathbf{n})\mathbf{n}$$

[J.U. BRACKBILL, D.B. KOTHE, C. ZEMACH]

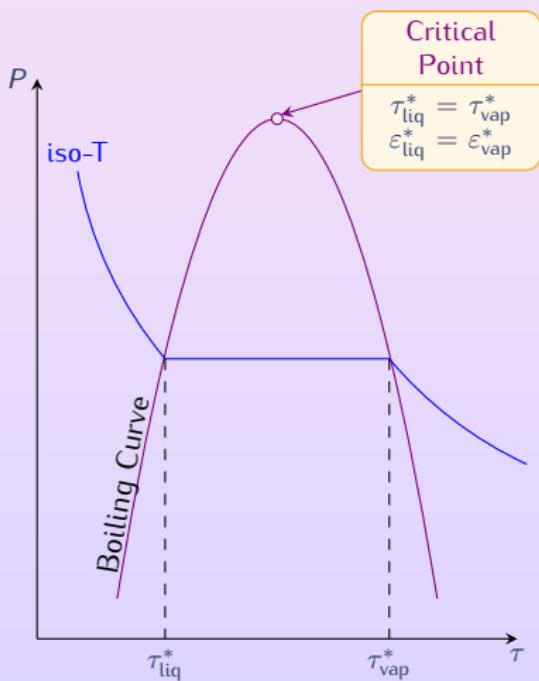
METASTABILITY



$$P^{\text{eq}} = \begin{cases} P_{\text{liq}}, & \text{if } \tau < \tau_{\text{liq}}^*, \\ P^{\text{sat}}, & \text{if } \tau_{\text{liq}}^* < \tau < \tau_{\text{vap}}^*, \\ P_{\text{vap}}, & \text{if } \tau_{\text{vap}}^* < \tau. \end{cases}$$

$$P^{\text{met}} = \begin{cases} P_{\text{liq}}, & \text{if } \tau < \tau_{\text{liq}}^*, \\ [P^{\text{sat}} \text{ or } P_{\text{liq}}], & \text{if } \tau_{\text{liq}}^* < \tau < \tau_m^*, \\ P^{\text{sat}}, & \text{if } \tau_m^* < \tau < \tau_M^*, \\ [P^{\text{sat}} \text{ or } P_{\text{vap}}], & \text{if } \tau_M^* < \tau < \tau_{\text{vap}}^*, \\ P_{\text{vap}}, & \text{if } \tau_{\text{vap}}^* < \tau, \end{cases}$$

CRITICAL POINT



Physic

- 2 Pure Phases EOS $(\tau, \varepsilon) \mapsto P_\alpha$
- 1 Saturation EOS $\tau \mapsto P^{\text{sat}}$

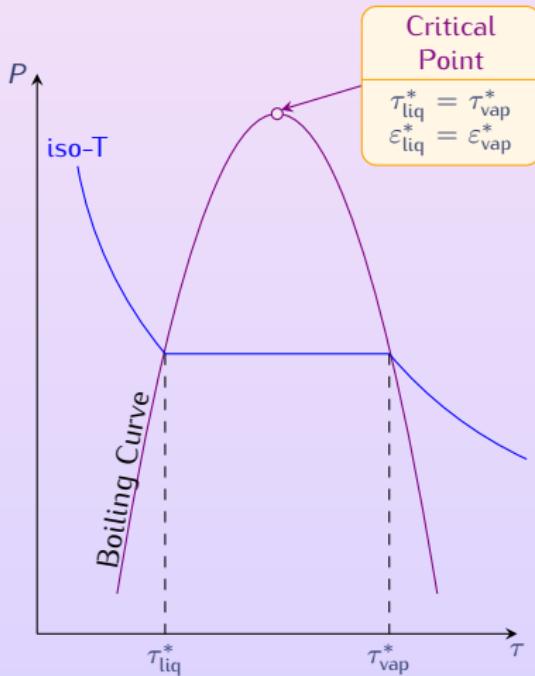
EOS

PG $\varepsilon_{\text{liq}}^* = \varepsilon_{\text{vap}}^* \Leftrightarrow c_{V_{\text{liq}}} = c_{V_{\text{vap}}} \text{ (indip. of } T\text{)}$

SG $\left\{ \tau_i, P_i^{\text{sat},e} \right\}_i \rightsquigarrow (\tau, \varepsilon) \mapsto P_\alpha \rightsquigarrow \tau \mapsto P^{\text{sat}}$

$\tau_{\text{liq}}^* = \tau_{\text{vap}}^* \text{ but } \varepsilon_{\text{liq}}^* \neq \varepsilon_{\text{vap}}^*$

CRITICAL POINT



PHYSIC

- 2 Pure Phases EOS $(\tau, \varepsilon) \mapsto P_\alpha$
- 1 Saturation EOS $\tau \mapsto P^{\text{sat}}$

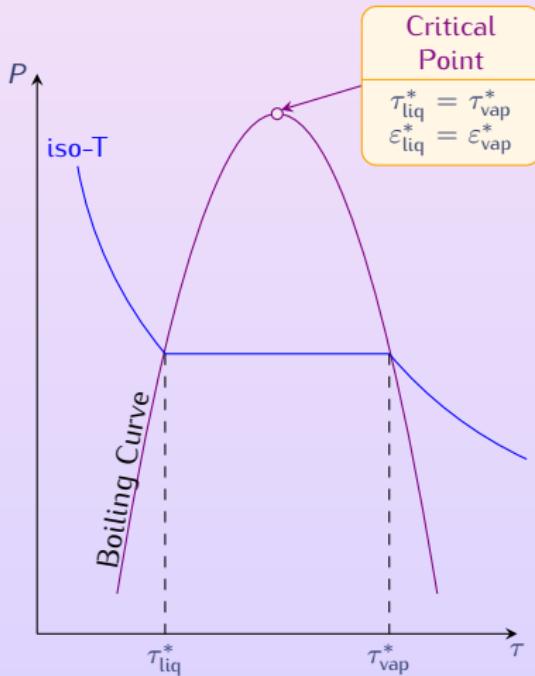
EOS

PG $\varepsilon_{liq}^* = \varepsilon_{vap}^* \Leftrightarrow c_{V_{liq}} = c_{V_{vap}}$ (indip. of T)

SG $\left\{ \tau_i, P_i^{\text{sat},e} \right\}_i \rightsquigarrow (\tau, \varepsilon) \mapsto P_\alpha \rightsquigarrow \tau \mapsto P^{\text{sat}}$

$\tau_{liq}^* = \tau_{vap}^*$ but $\varepsilon_{liq}^* \neq \varepsilon_{vap}^*$

CRITICAL POINT



PHYSIC

- 2 Pure Phases EOS $(\tau, \epsilon) \mapsto P_\alpha$
- 1 Saturation EOS $\tau \mapsto P^{\text{sat}}$

EOS

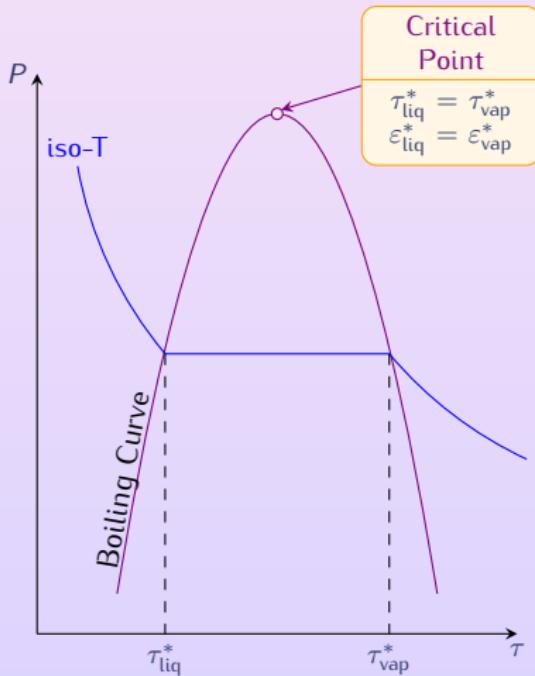
PG $\epsilon_{\text{liq}}^* = \epsilon_{\text{vap}}^* \Leftrightarrow c_{V_{\text{liq}}} = c_{V_{\text{vap}}} \text{ (indip. of } T\text{)}$

SG $\left\{ \tau_i, P_i^{\text{sat},e} \right\}_i \rightsquigarrow (\tau, \epsilon) \mapsto P_\alpha \rightsquigarrow \tau \mapsto P^{\text{sat}}$

$\tau_{\text{liq}}^* = \tau_{\text{vap}}^* \text{ but } \epsilon_{\text{liq}}^* \neq \epsilon_{\text{vap}}^*$

TAB $\left\{ \tau_i, P_i^{\text{sat},e} \right\}_i \rightsquigarrow \tau \mapsto P^{\text{sat}}$
 $\{(\tau_i, \epsilon_i), (P_\alpha^e)_i\}_i \rightsquigarrow (\tau, \epsilon) \mapsto P_\alpha$

CRITICAL POINT



PHYSIC

- 2 Pure Phases EOS $(\tau, \epsilon) \mapsto P_\alpha$
- 1 Saturation EOS $\tau \mapsto P^{\text{sat}}$

EOS

PG $\epsilon_{\text{liq}}^* = \epsilon_{\text{vap}}^* \Leftrightarrow c_{V_{\text{liq}}} = c_{V_{\text{vap}}} \text{ (indip. of } T\text{)}$

SG $\left\{ \tau_i, P_i^{\text{sat,e}} \right\}_i \rightsquigarrow (\tau, \epsilon) \mapsto P_\alpha \rightsquigarrow \tau \mapsto P^{\text{sat}}$

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SUMMARY

PHASE CHANGE EQUATION

$$\frac{\tau - \tau_{\text{vap}}^{\text{sat}}}{\tau_{\text{liq}}^{\text{sat}} - \tau_{\text{vap}}^{\text{sat}}} = \frac{\varepsilon - \varepsilon_{\text{vap}}^{\text{sat}}}{\varepsilon_{\text{liq}}^{\text{sat}} - \varepsilon_{\text{vap}}^{\text{sat}}}$$

with

$$T \mapsto \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(T) = \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}(T, P^{\text{sat}}(T))$$

or

$$P \mapsto \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(P) = \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}(T^{\text{sat}}(P), P)$$

SUMMARY

How to compute saturation functions τ_α^{sat} and $\varepsilon_\alpha^{\text{sat}}$

- **Analytical EOS:** we compute the saturation functions τ_α^{sat} and $\varepsilon_\alpha^{\text{sat}}$ by the **Coexistence Curve**:

- Exact: $T \mapsto P^{\text{sat}}(T)$ or $P \mapsto T^{\text{sat}}(P)$

$$\begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha^{\text{sat}}(P) = \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha(T^{\text{sat}}(P), P) \quad \text{e.g. Simplified Stiffened Gases}$$

- Approximated: $T \mapsto \hat{P}^{\text{sat}}(T) \approx P^{\text{sat}}(T)$

$$\begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha^{\text{sat}}(T) \approx \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha(T, \hat{P}^{\text{sat}}(T)) \quad \text{e.g. General Stiffened Gases}$$

- **Tabulated EOS:** the saturation functions τ_α^{sat} and $\varepsilon_\alpha^{\text{sat}}$ are given by experiments and we set

$$\begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha^{\text{sat}}(T \text{ or } P) \approx \begin{pmatrix} \hat{\tau} \\ \hat{\varepsilon} \end{pmatrix}_\alpha^{\text{sat}}(T \text{ or } P)$$

To Do

	EOS	Pure Phases	Equilibrium	Cavitation	Boiling	Simulation
	✓	✓	✓	✓	✓	①
Virtual Fluid (SG)	✓	✓	✓	✓	✓	②
Real Fluid (SG)	✓	✓	✓	✓	✓	③
Tabulated	④	✓	⑤	⑥	⑦	