

Jenuary 11, 2011

# MODELLING AND SIMULATION OF NUCLEATE BOILING

## A CONTRIBUTION TO THE STUDY OF THE BOILING CRISIS

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# OUTLINE

1 Context

2 Model

3 Numerical Approximation and Example

4 Conclusion

# OUTLINE

## 1 Context

## 2 Model

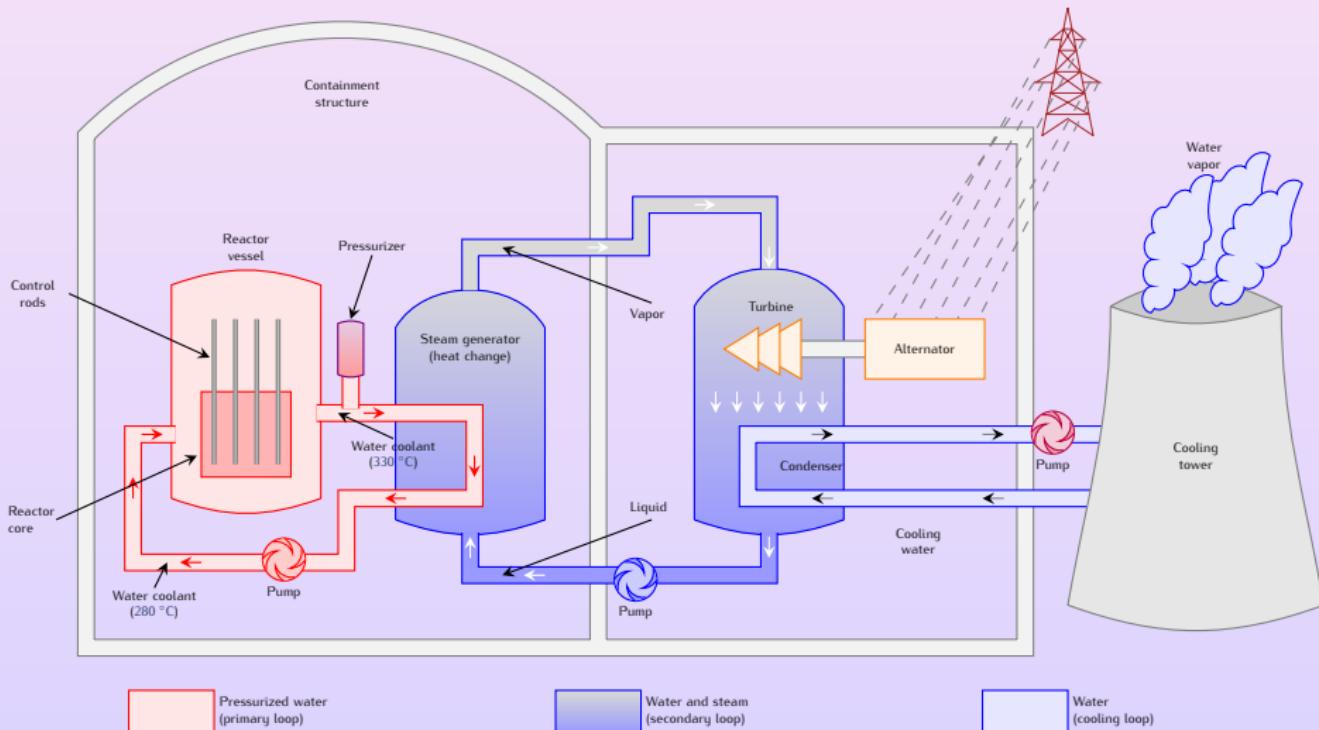
- Equation of State
- Conservation Laws

## 3 Numerical Approximation and Example

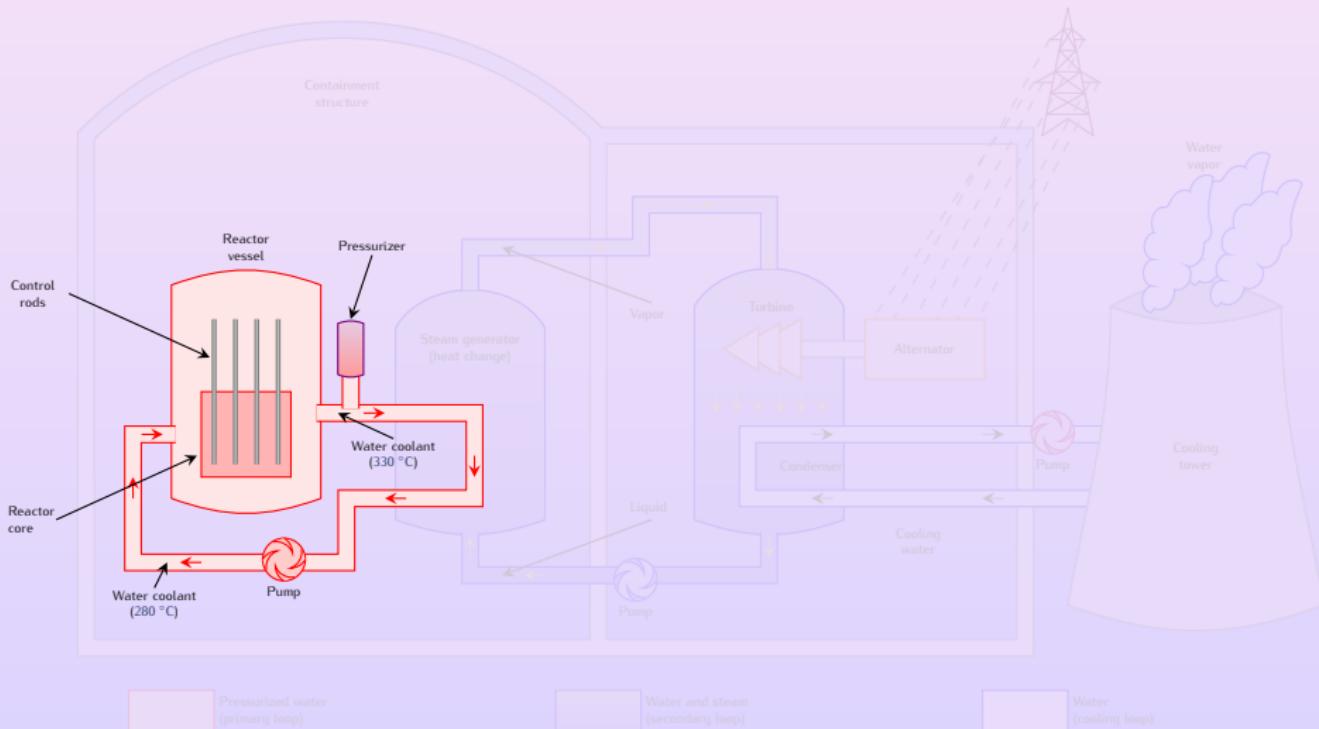
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- Numerical Scheme and Example

## 4 Conclusion

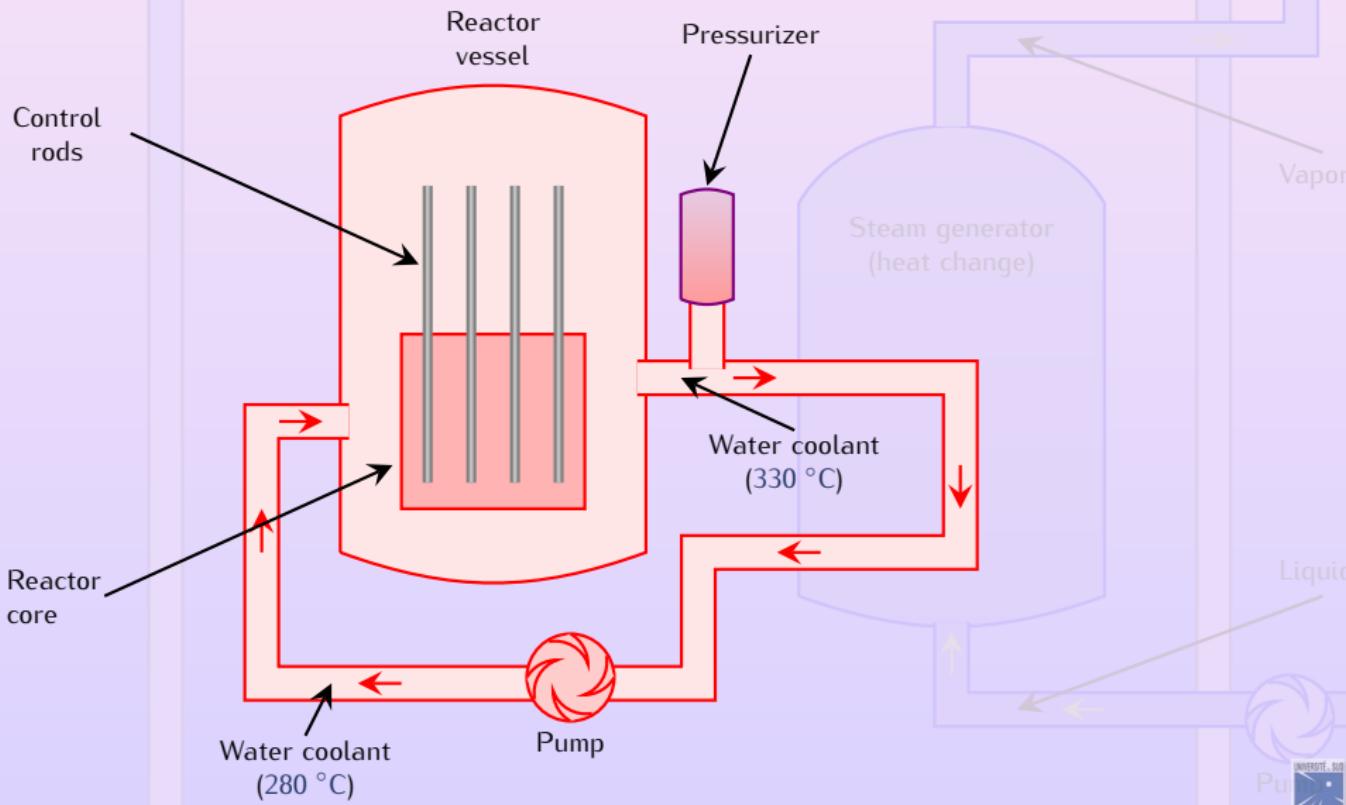
# PRESSURIZED WATER REACTOR



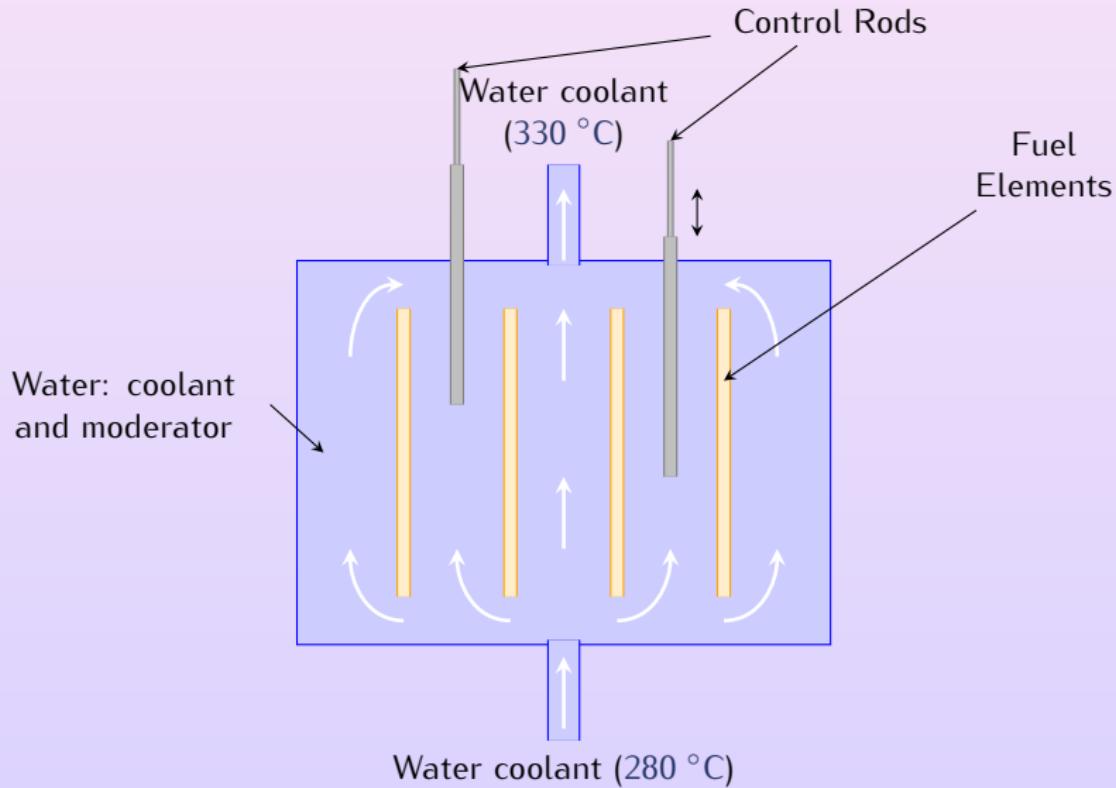
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# CORE OF A PRESSURIZED WATER REACTOR

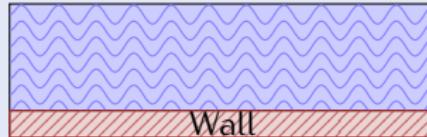


# BOILING CRISIS

## PHENOMENON

Liquid phase heated by a wall at a fixed temperature  $T^{\text{wall}}$ .

When  $T^{\text{wall}}$  increases, we switch from a **Nucleate Boiling** to a **Film Boiling**.

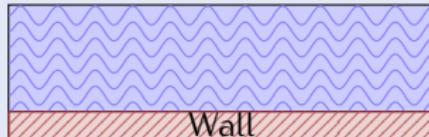


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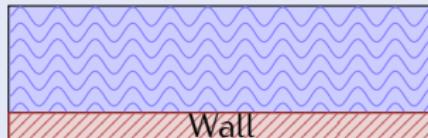
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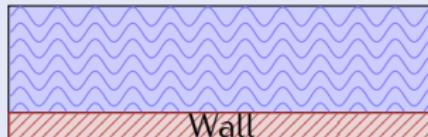
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# “INGREDIENTS” OF THE MODEL

✓ Simulating all bubbles (DNS),

- System of PDEs for the fluid flow (monophasic or diphasic),
- Phase transition (pressure and/or temperature variations),
- Heat Diffusion,
- Surface Tension,
- Gravity.



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# EULER SYSTEM

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0, \\ \partial_t (\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = \mathfrak{V}_{\text{vf}} - \mathfrak{S}_{\text{sf}}, \\ \partial_t \left( \varrho \left( \frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \right) + \operatorname{div} \left( \varrho \left( \frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \mathbf{u} + P \mathbf{u} \right) = (\mathfrak{V}_{\text{vf}} - \mathfrak{S}_{\text{sf}}) \cdot \mathbf{u} - \operatorname{div}(q). \end{cases}$$

- $(\mathbf{x}, t) \mapsto \varrho$  specific density,
- $(\mathbf{x}, t) \mapsto \varepsilon$  specific internal energy,
- $(\mathbf{x}, t) \mapsto \mathbf{u}$  velocity;
- $(\varrho, \varepsilon) \mapsto \mathfrak{V}_{\text{vf}}$  body forces,
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- $(\varrho, \varepsilon) \mapsto \operatorname{div}(q)$  heat transfer.

$(\varrho, \varepsilon) \mapsto P$  pressure law.



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# EOS OF EACH PHASE $\alpha = \text{liq}, \text{vap}$

$$\left. \begin{array}{l} \tau_\alpha \text{ specific volume} \\ \varepsilon_\alpha \text{ specific internal energy} \end{array} \right\} \Rightarrow \mathbf{w}_\alpha \stackrel{\text{def}}{=} (\tau_\alpha, \varepsilon_\alpha);$$

$\mathbf{w}_\alpha \mapsto s_\alpha$  specific entropy (Hessian matrix neg. def.);



$$\left. \begin{array}{ll} T_\alpha & \stackrel{\text{def}}{=} \left( \frac{\partial s_\alpha}{\partial \varepsilon_\alpha} \Big|_{\tau_\alpha} \right)^{-1} > 0 & \text{temperature,} \\ P_\alpha & \stackrel{\text{def}}{=} T_\alpha \frac{\partial s_\alpha}{\partial \tau_\alpha} \Big|_{\varepsilon_\alpha} > 0 & \text{pressure,} \\ g_\alpha & \stackrel{\text{def}}{=} \varepsilon_\alpha + P_\alpha \tau_\alpha - T_\alpha s_\alpha & \text{free enthalpy (Gibbs potential).} \end{array} \right.$$

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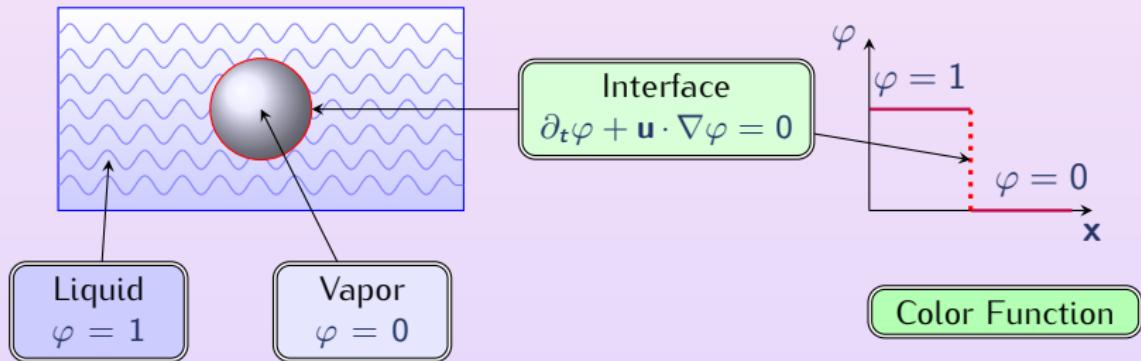
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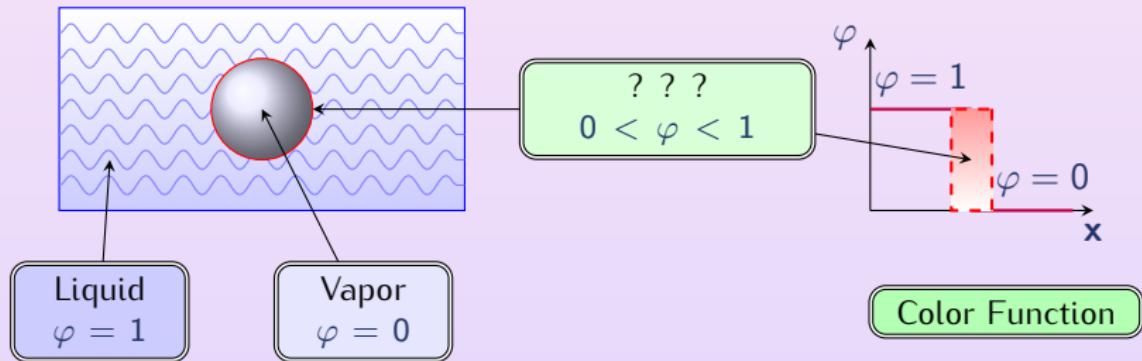


# LIQUID-VAPOR INTERFACE



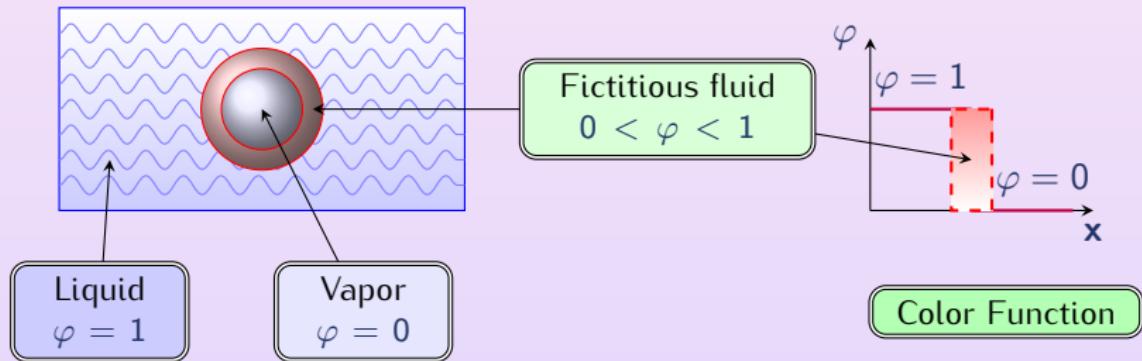
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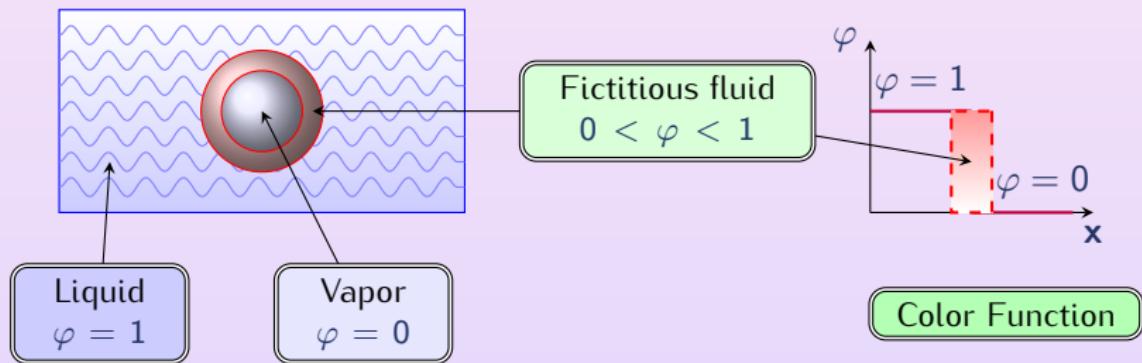
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# LIQUID-VAPOR INTERFACE



➡ Goal: define a global pressure law such that

- $(\varrho, \varepsilon, \mathbf{u}, P)$  are continuous (3 zones)
- the interface position and the phase change are implicit (i.e. ~~✓~~)
- coherence with classical thermodynamics [H. CALLEN]

# EOS OF A MIXTURE

- $\mathbf{w} \stackrel{\text{def}}{=} y\mathbf{w}_{\text{liq}} + (1 - y)\mathbf{w}_{\text{vap}}$ ;
- $y$  mass fraction;
- $z$  volume fraction s.t.  $y\tau_{\text{liq}} = z\tau$ ;
- $\psi$  energy fraction s.t.  $y\varepsilon_{\text{liq}} = \psi\varepsilon$ .



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## ENTROPY WITHOUT PHASE CHANGE

$$\sigma \stackrel{\text{def}}{=} y s_{\text{liq}}(\mathbf{w}_{\text{liq}}) + (1 - y)s_{\text{vap}}(\mathbf{w}_{\text{vap}}) = y s_{\text{liq}}\left(\frac{z}{y}\tau, \frac{\psi}{y}\varepsilon\right) + (1 - y)s_{\text{vap}}\left(\frac{1-z}{1-y}\tau, \frac{1-\psi}{1-y}\varepsilon\right)$$

$$P = \left( \frac{\partial \sigma}{\partial \varepsilon} \Bigg|_{\tau, y, z, \psi} \right)^{-1} \frac{\partial \sigma}{\partial \tau} \Bigg|_{\varepsilon; y, z, \psi}$$

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# EOS OF PHASE CHANGE

## ENTROPY AT EQUILIBRIUM

$$\mathbf{w} \mapsto s^{\text{eq}}(\mathbf{w}) = \sigma(\mathbf{w}, z^{\text{eq}}(\mathbf{w}), y^{\text{eq}}(\mathbf{w}), \psi^{\text{eq}}(\mathbf{w}))$$

DEFINITION [H. CALLEN, PH. HELLUY ...]

Optimization Problem:

$$s^{\text{eq}}(\mathbf{w}) \stackrel{\text{def}}{=} \max_{z, y, \psi \in [0,1]^3} \sigma(\mathbf{w}, z, y, \psi)$$

Optimality Condition:  $\begin{cases} T_1(z, y, \psi) = T_2(z, y, \psi) \\ P_1(z, y, \psi) = P_2(z, y, \psi) \\ g_1(z, y, \psi) = g_2(z, y, \psi) \end{cases}$       Solution:  $(z^*, y^*, \psi^*)$



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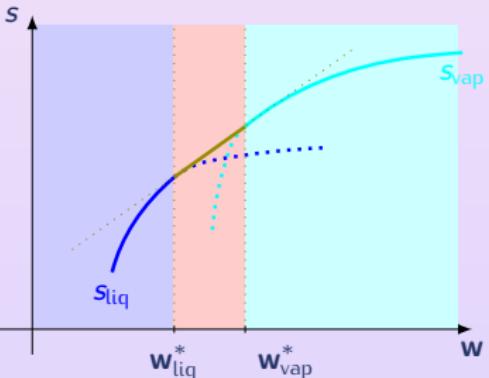
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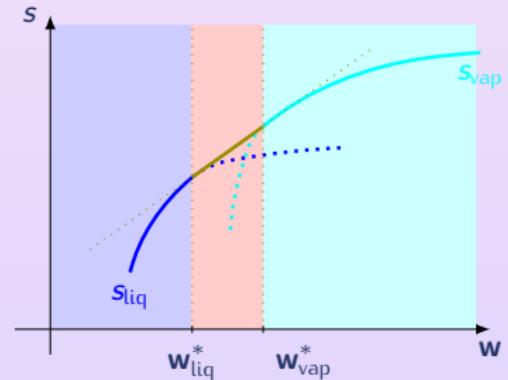
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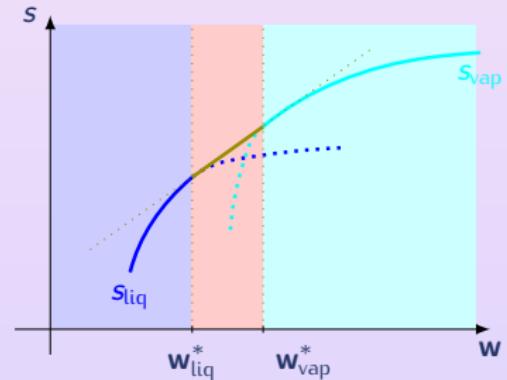
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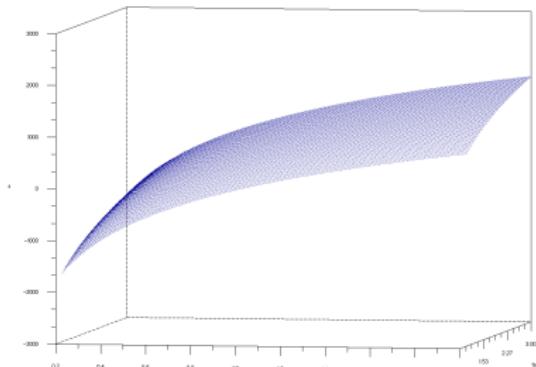


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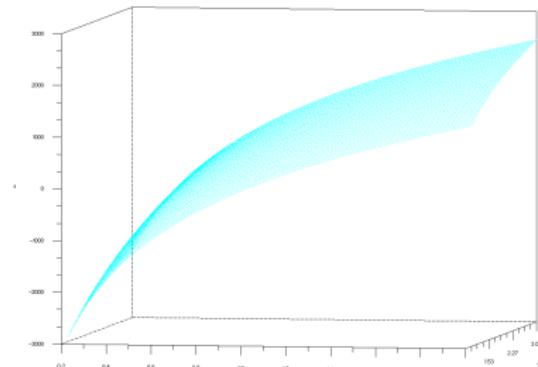
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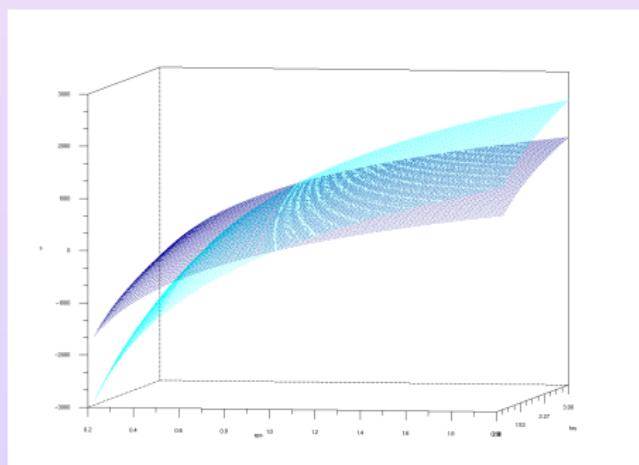


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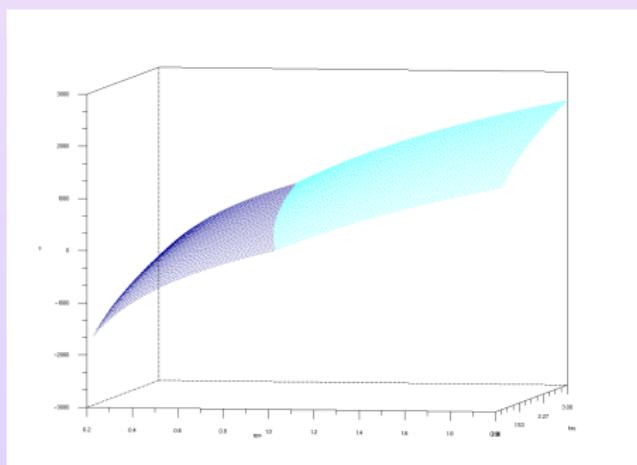
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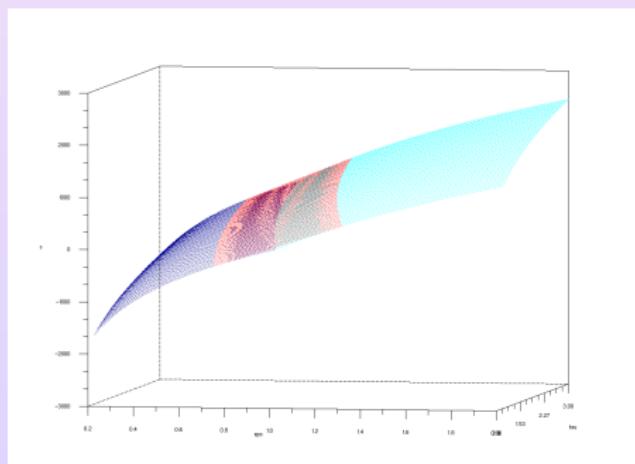
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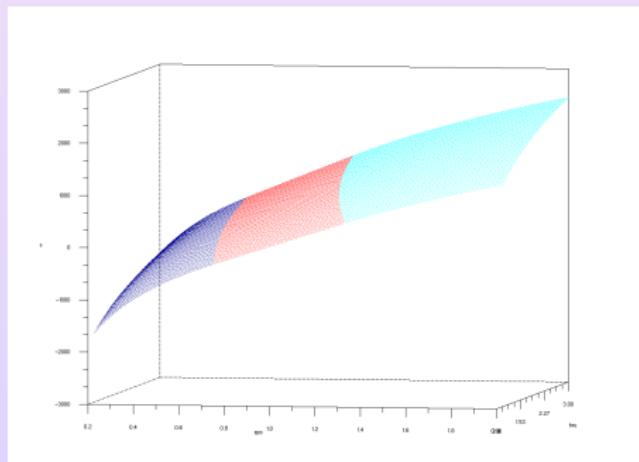
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# FROM $\mathbf{w} \mapsto s^{\text{eq}}$ TO $\mathbf{w} \mapsto P^{\text{eq}}$

For all  $\tilde{\mathbf{w}}$  fixed, we seek  $(\mathbf{w}_{\text{liq}}^*, \mathbf{w}_{\text{vap}}^*, y^*)$  as the solution of the system

$$\begin{cases} P_{\text{liq}}(\mathbf{w}_{\text{liq}}) = P_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ T_{\text{liq}}(\mathbf{w}_{\text{liq}}) = T_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ g_{\text{liq}}(\mathbf{w}_{\text{liq}}) = g_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ \tilde{\mathbf{w}} = y\mathbf{w}_{\text{liq}} + (1 - y)\mathbf{w}_{\text{vap}} \end{cases}$$

- if  $y^* \in ]0, 1[$  then  $\tilde{\mathbf{w}}$  is an equilibrium mixture state

$$s^{\text{eq}}(\tilde{\mathbf{w}}) = y^* s_{\text{liq}}(\mathbf{w}_{\text{liq}}^*) + (1 - y^*) s_{\text{vap}}(\mathbf{w}_{\text{vap}}^*),$$

- if the system has no solution or  $y^* \notin ]0, 1[$  then  $\tilde{\mathbf{w}}$  is a monophasic pure state

$$s^{\text{eq}}(\tilde{\mathbf{w}}) = \max\{s_{\text{liq}}(\tilde{\mathbf{w}}), s_{\text{vap}}(\tilde{\mathbf{w}})\},$$

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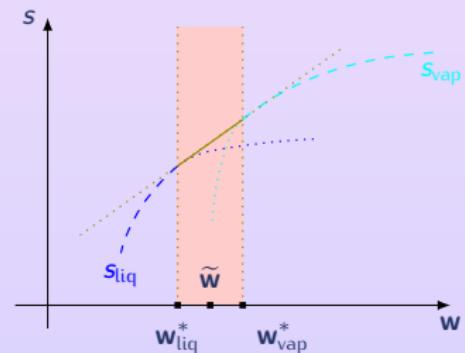
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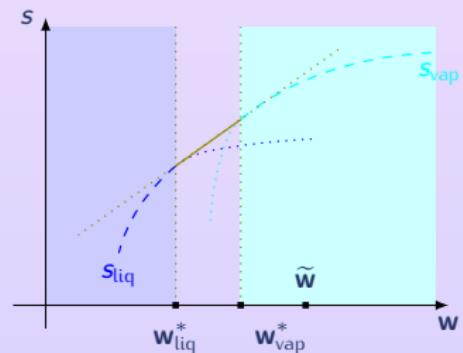
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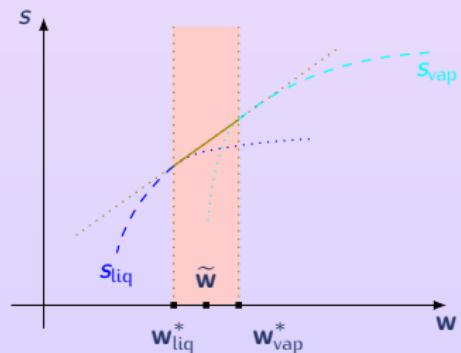
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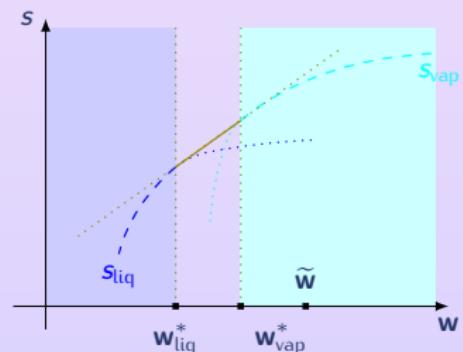
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# OUTLINE

## 1 Context

## 2 Model

- Equation of State
- Conservation Laws

## 3 Numerical Approximation and Example

- The Phase Change Equation
- Numerical Scheme and Example

## 4 Conclusion

# DYNAMIC LIQUID-VAPOR PHASE CHANGE

## EULER SYSTEM

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0, \\ \partial_t (\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t \left( \varrho \left( \frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \right) + \operatorname{div} \left( \varrho \left( \frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \mathbf{u} + P^{\text{eq}} \mathbf{u} \right) = 0 \end{cases} \quad \text{with } P^{\text{eq}} \stackrel{\text{def}}{=} \frac{s_{\tau}^{\text{eq}}}{s_{\varepsilon}^{\text{eq}}}.$$

## MATHEMATICAL PROPERTIES

If  $\tau_1^* \neq \tau_2^*$  and  $\varepsilon_1^* \neq \varepsilon_2^*$  (first order phase transition) then

- Euler system with hyperbolic (or parabolic)
- Riemann problem: millions of entropy (local) solutions in contact discontinuities at  $t=0$



# DYNAMIC LIQUID-VAPOR PHASE CHANGE

## EULER SYSTEM

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## MATHEMATICAL PROPERTIES

If  $\tau_1^* \neq \tau_2^*$  and  $\varepsilon_1^* \neq \varepsilon_2^*$  (first order phase transition) then

$$\textcircled{1} \ c(\mathbf{w}) > 0, \quad \textcircled{2} \ s_{\tau^*}^{\text{eq}}(\mathbf{w}) > 0$$

**① Euler system:** strict hyperbolicity ( $\neq p$ -system).

**② Riemann problem:** multitude of entropy (Lax) solutions [R. MENIKOFF, B. J. PLOHR], uniqueness of Liu solution.



# DYNAMIC LIQUID-VAPOR PHASE CHANGE

## EULER SYSTEM

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# SUMMARY OF THE MODEL

Euler System

$$\mathbf{w} \mapsto P^{\text{eq}}$$

$$\mathbf{w} \mapsto S^{\text{eq}}$$

$$\begin{cases} g_1(w_1) = g_2(w_2) \\ P_1(w_1) = P_2(w_2) \\ T_1(w_1) = T_2(w_2) \\ w = yw_1 + (1-y)w_2 \end{cases}$$

Phase Change Equation

$$\frac{\tau - \tau_{\text{vap}}^{\text{sat}}}{\tau_{\text{liq}}^{\text{sat}} - \tau_{\text{vap}}^{\text{sat}}} = \frac{\varepsilon - \varepsilon_{\text{vap}}^{\text{sat}}}{\varepsilon_{\text{liq}}^{\text{sat}} - \varepsilon_{\text{vap}}^{\text{sat}}}$$



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Euler System

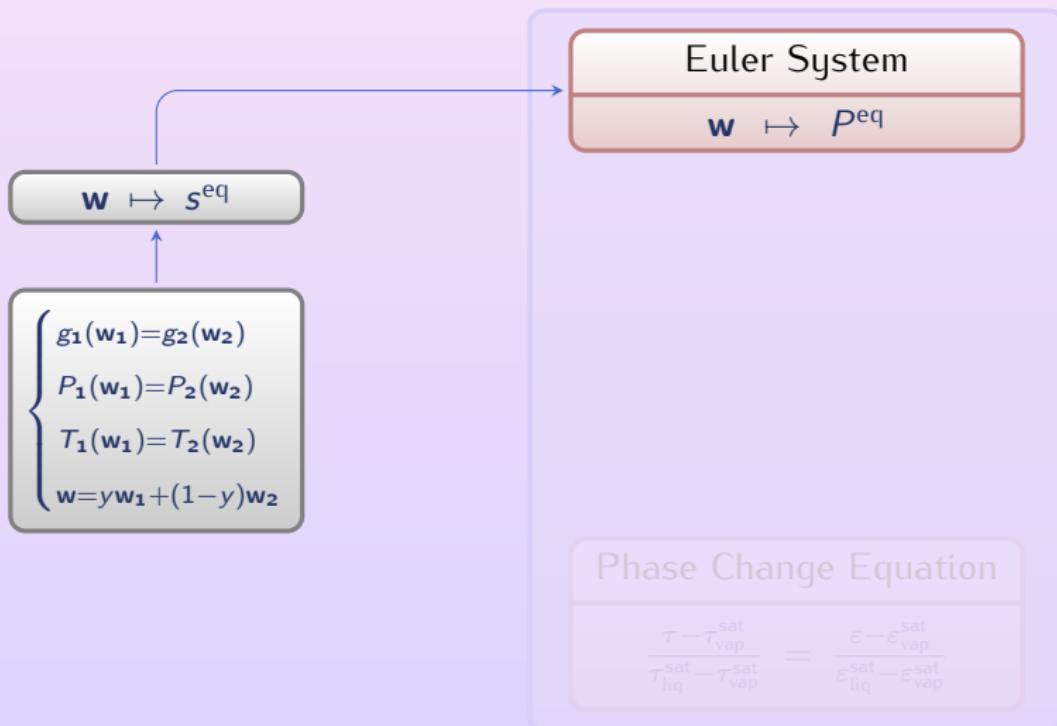
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Phase Change Equation

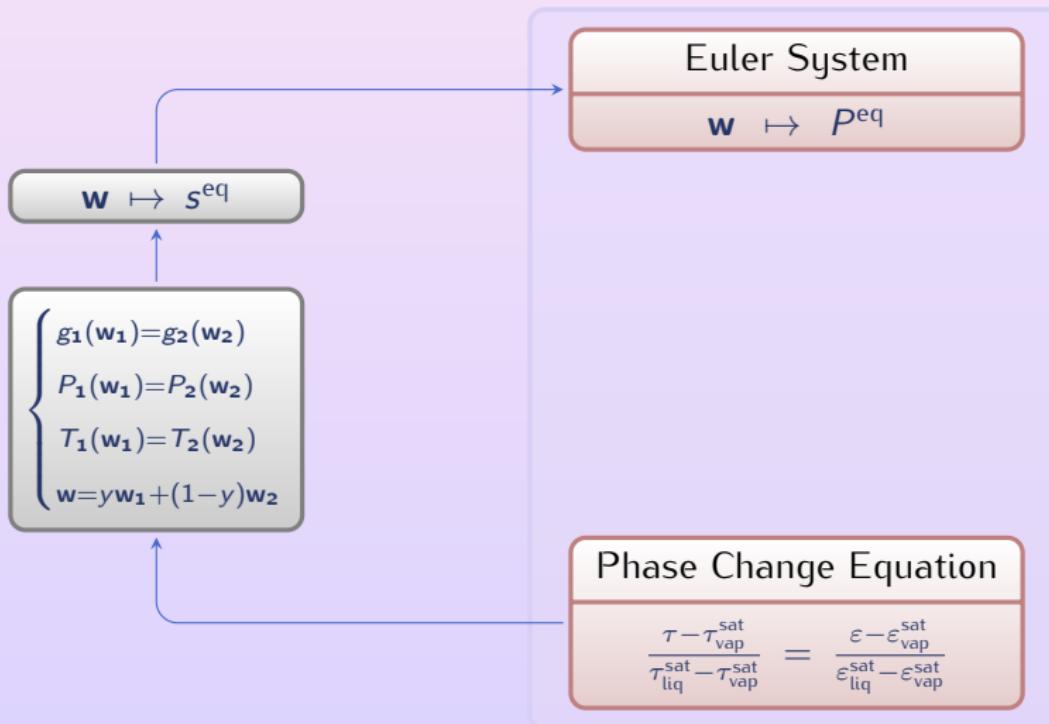
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# ANALYTICAL EOS

$(\tau, \varepsilon)$  fixed

$(\tau_1, \varepsilon_1, \tau_2, \varepsilon_2, y)$  SOLUTION OF

$$\begin{cases} g_1(\tau_1, \varepsilon_1) = g_2(\tau_2, \varepsilon_2) \\ P_1(\tau_1, \varepsilon_1) = P_2(\tau_2, \varepsilon_2) \\ T_1(\tau_1, \varepsilon_1) = T_2(\tau_2, \varepsilon_2) \\ \tau = y\tau_1 + (1-y)\tau_2 \\ \varepsilon = y\varepsilon_1 + (1-y)\varepsilon_2 \end{cases}$$

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$T \mapsto P = \hat{P}^{\text{sat}}(T) \approx P^{\text{sat}}(T)$

least square approximation

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# TABULATED EOS

$T$ (K)	$P^{\text{sat}}$ (MPa)	Volume (m <sup>3</sup> /kg)		Internal Energy (kJ/kg)	
		$\tau_{\text{liq}}^{\text{sat}}$	$\tau_{\text{vap}}^{\text{sat}}$	$\varepsilon_{\text{liq}}^{\text{sat}}$	$\varepsilon_{\text{vap}}^{\text{sat}}$
275	0,00069845	0,0010001	181,60	7,7590	2377,5
278	0,00086349	0,0010001	148,48	20,388	2381,6
281	0,0010621	0,0010002	122,01	32,996	2385,7
284	0,0012999	0,0010004	100,74	45,586	2389,8
287	0,0015835	0,0010008	83,560	58,162	2393,9
290	0,0019200	0,0010012	69,625	70,727	2398,0
293	0,0023177	0,0010018	58,267	83,284	2402,1
296	0,0027856	0,0010025	48,966	95,835	2406,2
299	0,0033342	0,0010032	41,318	108,38	2410,3
302	0,0039745	0,0010041	35,002	120,92	2414,4
305	0,0047193	0,0010050	29,764	133,46	2418,4
308	0,0055825	0,0010060	25,403	146	2422,5
...	...	...	...	...	...

Source: <http://webbook.nist.gov/chemistry/fluid/>



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$(\tau, \varepsilon)$  fixed

## $T$ SOLUTION OF

$$\frac{\tau - \tau_2^{\text{sat}}(T)}{\tau_1^{\text{sat}}(T) - \tau_2^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_2^{\text{sat}}(T)}{\varepsilon_1^{\text{sat}}(T) - \varepsilon_2^{\text{sat}}(T)} \quad \text{with} \quad \left(\frac{\tau}{\varepsilon}\right)_\alpha^{\text{sat}}(T) \quad \text{tabulated}$$

Q

$$\frac{\tau - \hat{\tau}_2^{\text{sat}}(T)}{\hat{\tau}_1^{\text{sat}}(T) - \hat{\tau}_2^{\text{sat}}(T)} = \frac{\varepsilon - \hat{\varepsilon}_2^{\text{sat}}(T)}{\hat{\varepsilon}_1^{\text{sat}}(T) - \hat{\varepsilon}_2^{\text{sat}}(T)} \quad \text{with} \quad \left(\frac{\hat{\tau}}{\hat{\varepsilon}}\right)_\alpha^{\text{sat}}(T)$$



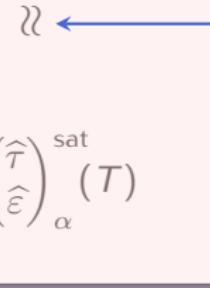
# TABULATED EOS

$(\tau, \varepsilon)$  fixed

## $T$ SOLUTION OF

$$\frac{\tau - \tau_2^{\text{sat}}(T)}{\tau_1^{\text{sat}}(T) - \tau_2^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_2^{\text{sat}}(T)}{\varepsilon_1^{\text{sat}}(T) - \varepsilon_2^{\text{sat}}(T)} \quad \text{with} \quad \left(\begin{matrix} \tau \\ \varepsilon \end{matrix}\right)_\alpha^{\text{sat}}(T) \quad \text{tabulated}$$

$$\frac{\tau - \hat{\tau}_2^{\text{sat}}(T)}{\hat{\tau}_1^{\text{sat}}(T) - \hat{\tau}_2^{\text{sat}}(T)} = \frac{\varepsilon - \hat{\varepsilon}_2^{\text{sat}}(T)}{\hat{\varepsilon}_1^{\text{sat}}(T) - \hat{\varepsilon}_2^{\text{sat}}(T)} \quad \text{with} \quad \left(\begin{matrix} \hat{\tau} \\ \hat{\varepsilon} \end{matrix}\right)_\alpha^{\text{sat}}(T)$$



least square  
approximations

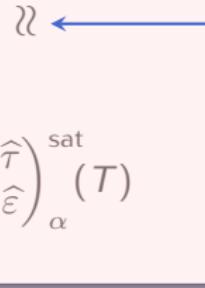
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least square  
approximations

# OUTLINE

## 1 Context

## 2 Model

- Equation of State
- Conservation Laws

## 3 Numerical Approximation and Example

- The Phase Change Equation
- Numerical Scheme and Example

## 4 Conclusion

# NUMERICAL SCHEME BASED ON RELAXATION APPROACH

$$\sigma(y, z, \psi, \tau, \varepsilon)$$

Optimization

$$s^{\text{eq}}(\tau, \varepsilon)$$

Off Equilibrium

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0 \\ \partial_t(\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = 0 \\ \partial_t(\varrho e) + \operatorname{div}((\varrho e + P)\mathbf{u}) = 0 \\ \partial_t z + \nabla \cdot (\varrho \mathbf{u} \otimes \mathbf{z}) = 0 \\ \partial_t y + \nabla \cdot (\varrho \mathbf{u} \otimes \mathbf{y}) = 0 \\ \partial_t \psi + \nabla \cdot (\varrho \mathbf{u} \otimes \psi) = 0 \end{cases}$$

$$\mu_j \rightarrow \infty$$

Equilibrium

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0 \\ \partial_t(\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t(\varrho e) + \operatorname{div}((\varrho e + P^{\text{eq}})\mathbf{u}) = 0 \\ P^{\text{eq}}(\varrho, \varepsilon) = \frac{s_{\tau}^{\text{eq}}}{s_{\varepsilon}^{\text{eq}}} \end{cases}$$

Two Steps:

- ① Hydrodynamic (+ gravity, surface tension, heat diffusion, ...)
- ② Projection by solving the Phase-Change Equation

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$$P(\varrho, z, y, \psi) = \frac{\sigma_z}{\sigma_z}$$

$$\mu_j \rightarrow \infty$$

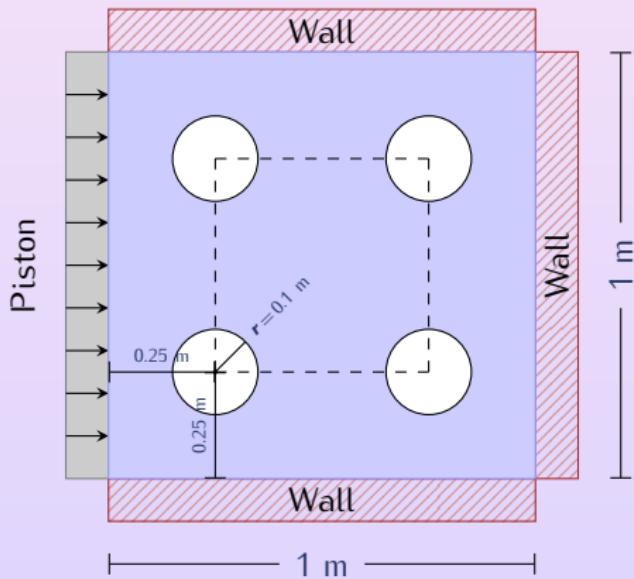
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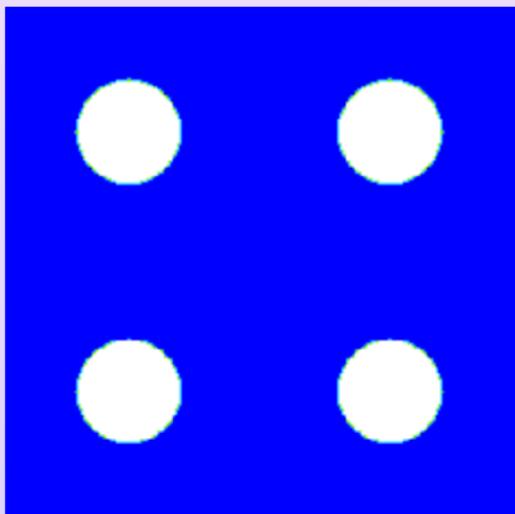
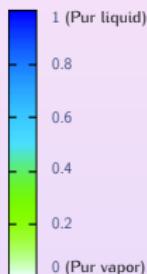
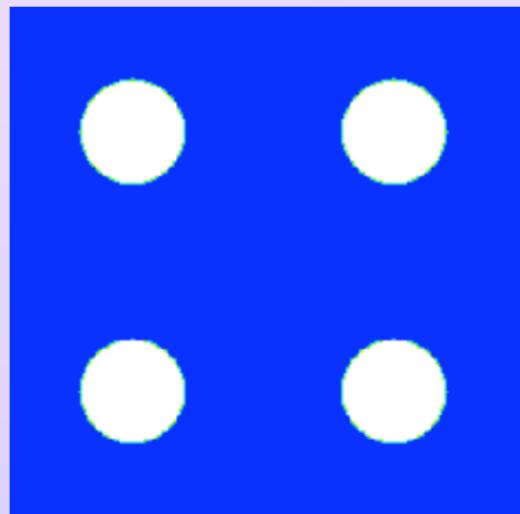
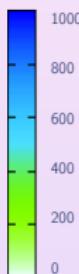
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# COMPRESSION OF VAPOR BUBBLES



# COMPRESSION OF VAPOR BUBBLES

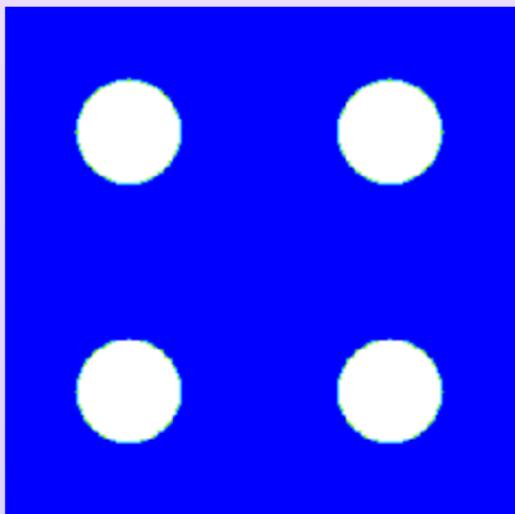
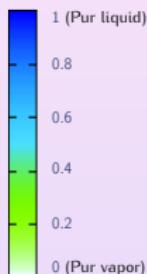
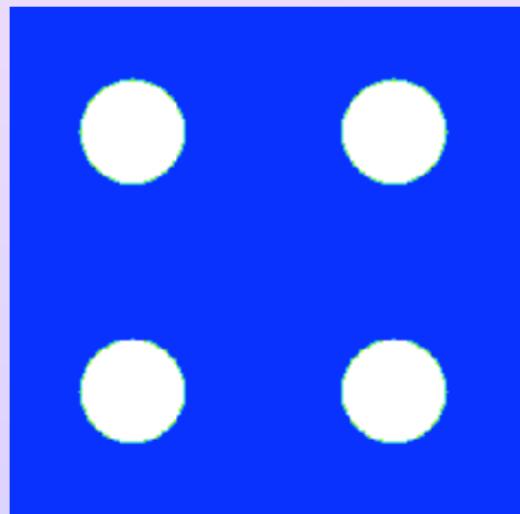
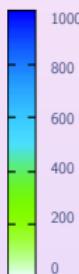
Massee fraction  $y$ Density  $\varrho$ 

◀ Geometry

▶ Play

▶ Skip

# COMPRESSION OF VAPOR BUBBLES

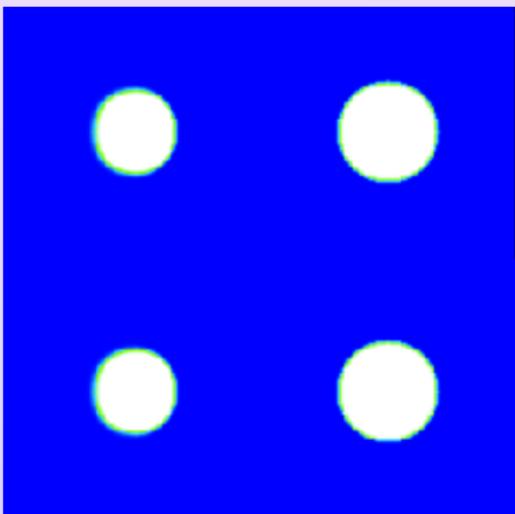
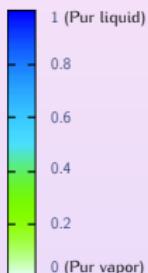
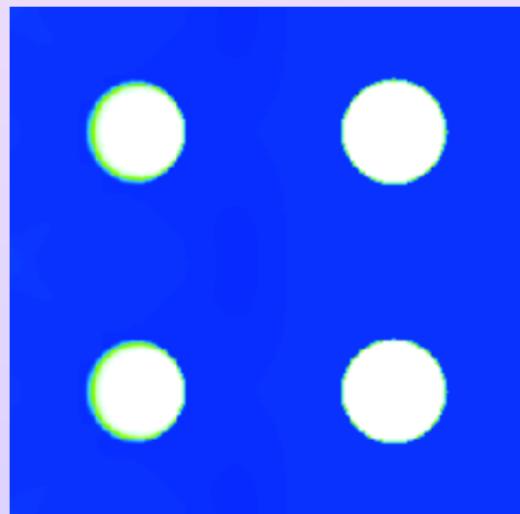
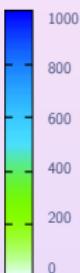
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◀ Geometry

▶ Play

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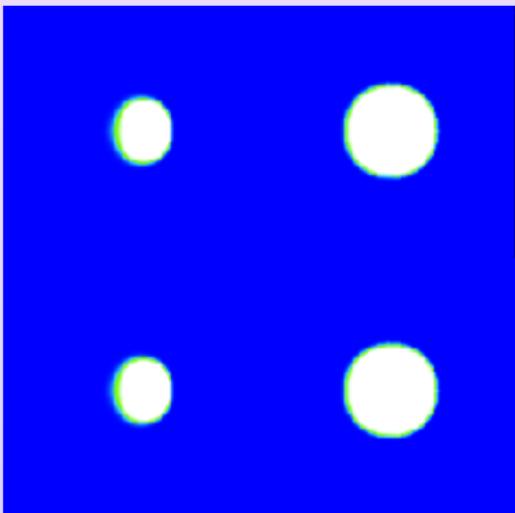
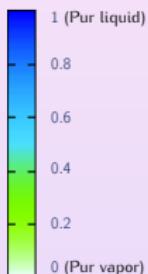
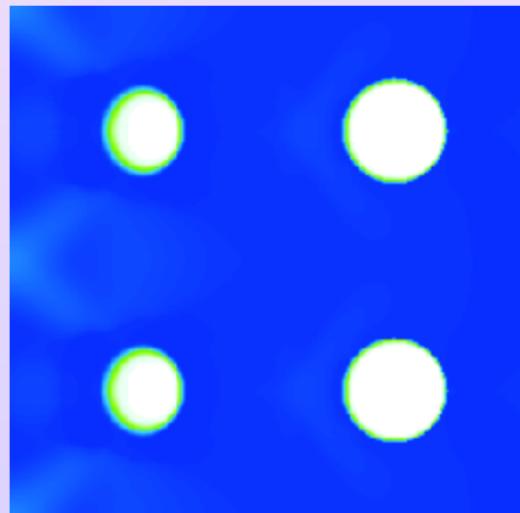
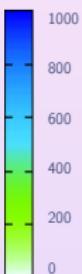
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◀ Geometry

▶ Play

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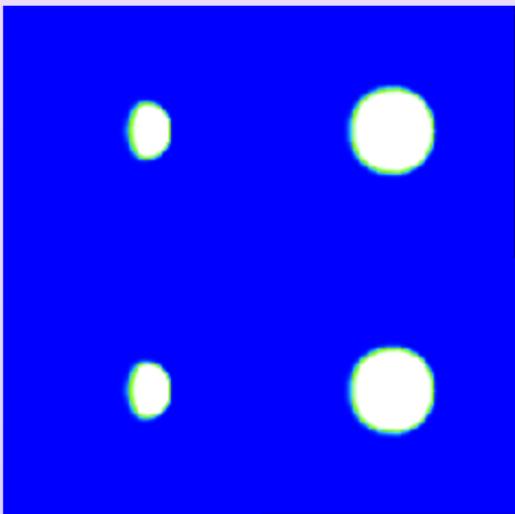
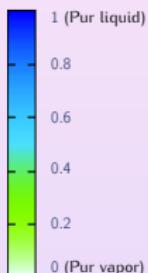
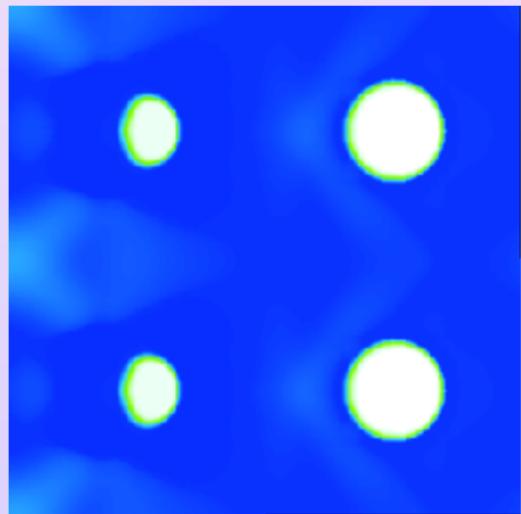
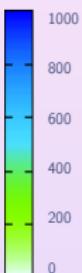
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◀ Geometry

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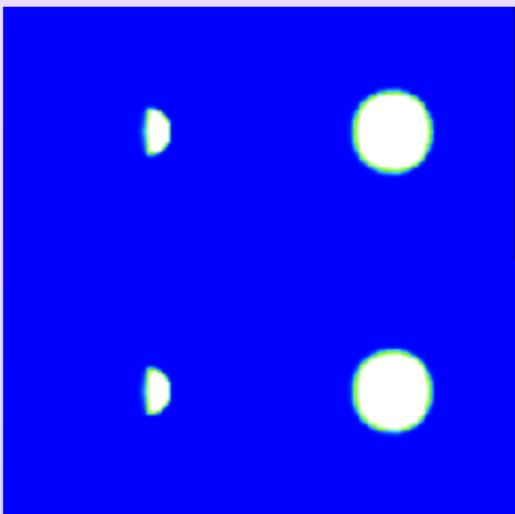
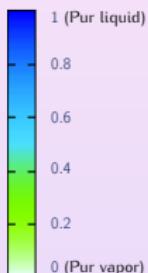
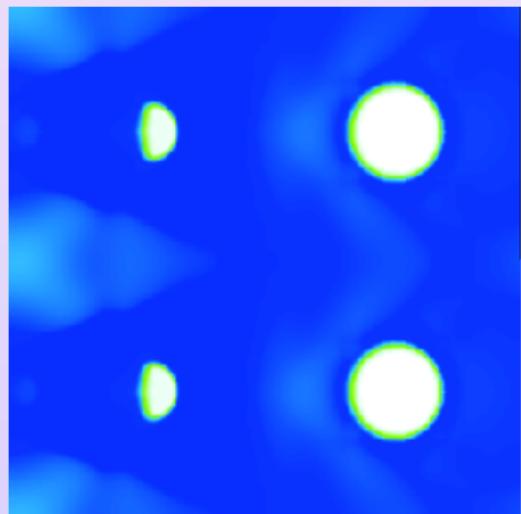
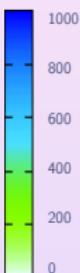
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◀ Geometry

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▶ Skip

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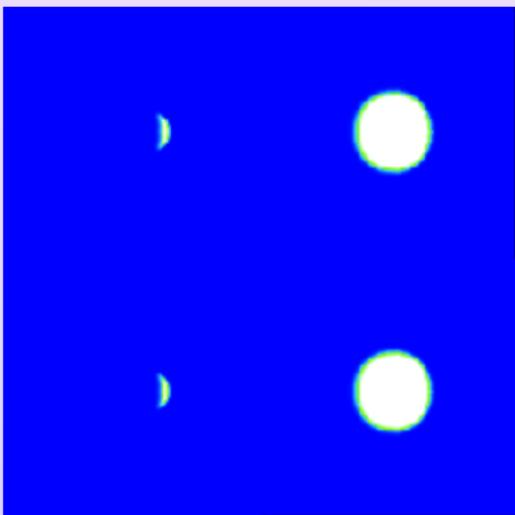
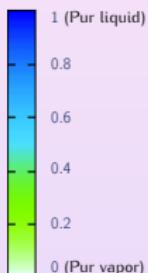
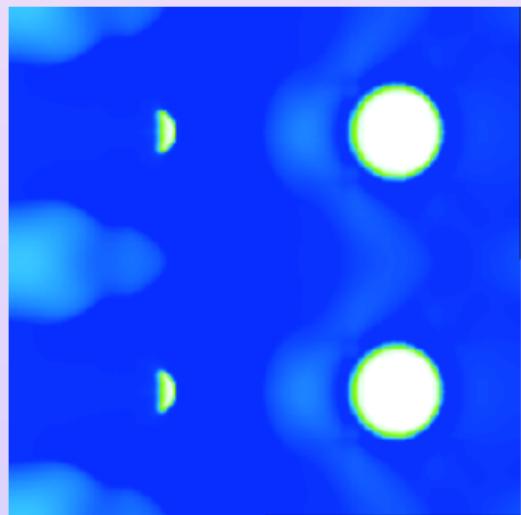
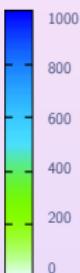
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◀ Geometry

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▶ Skip

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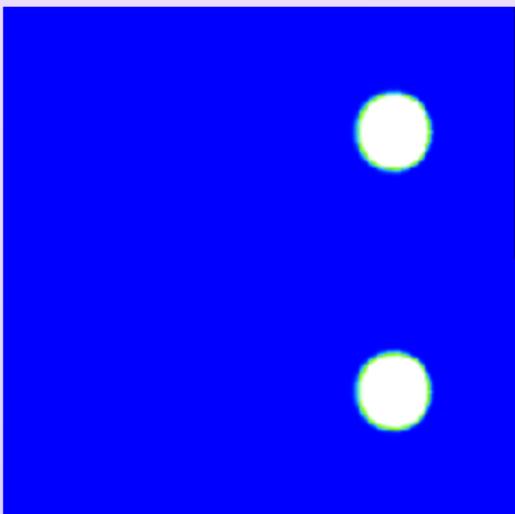
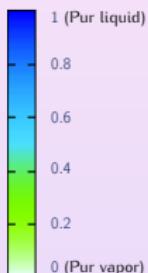
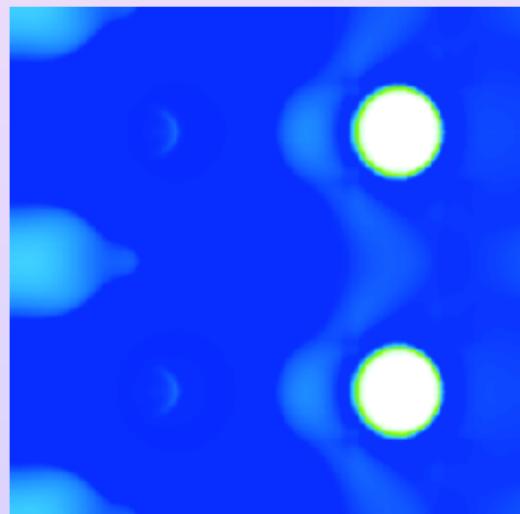
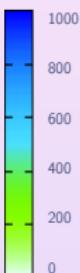
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◀ Geometry

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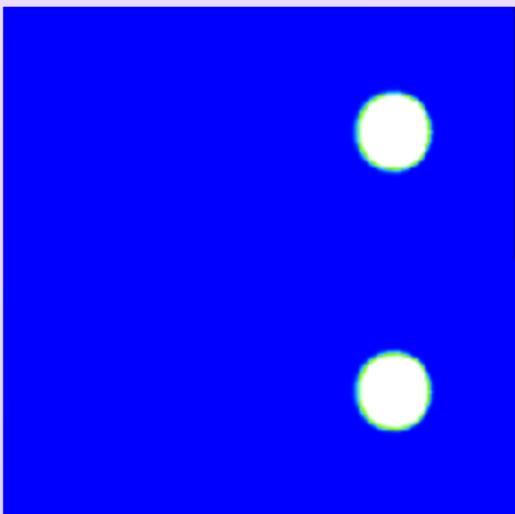
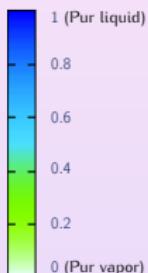
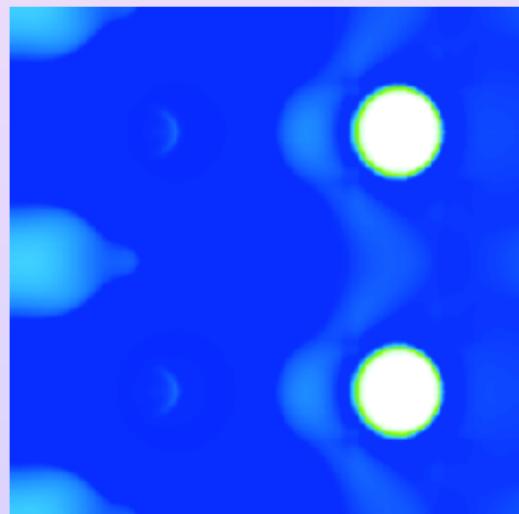
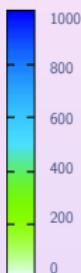
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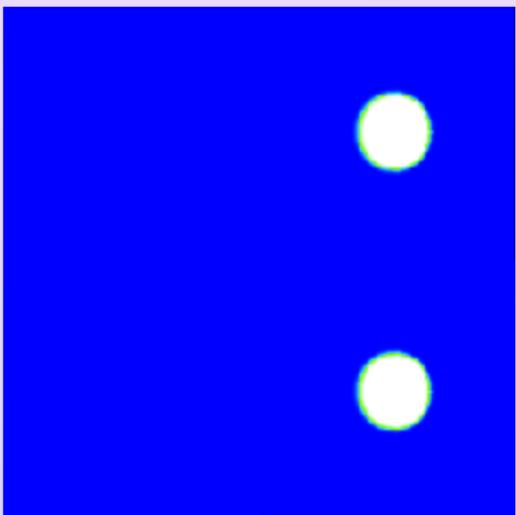
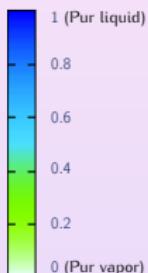
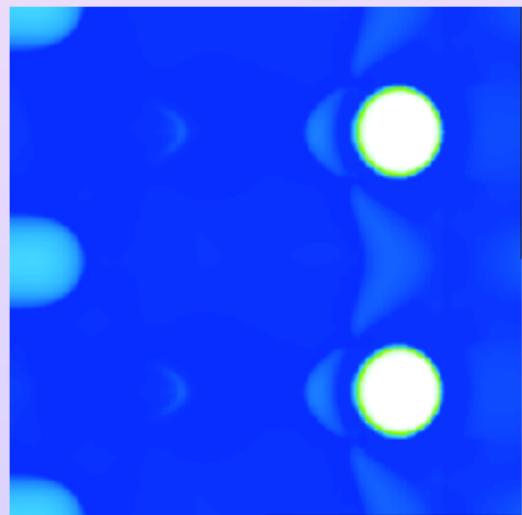
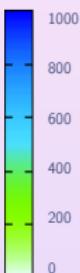
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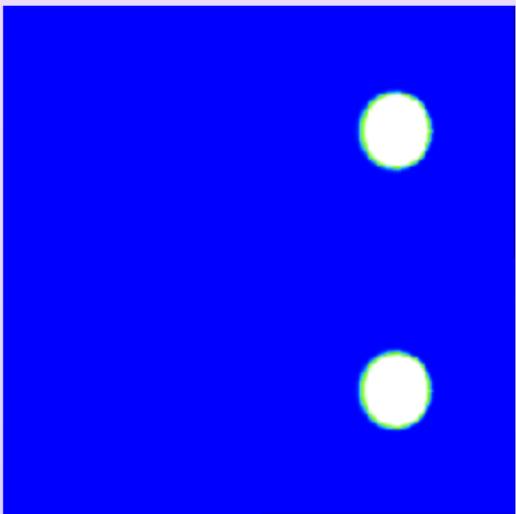
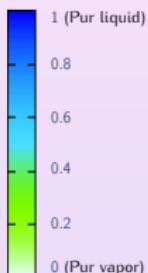
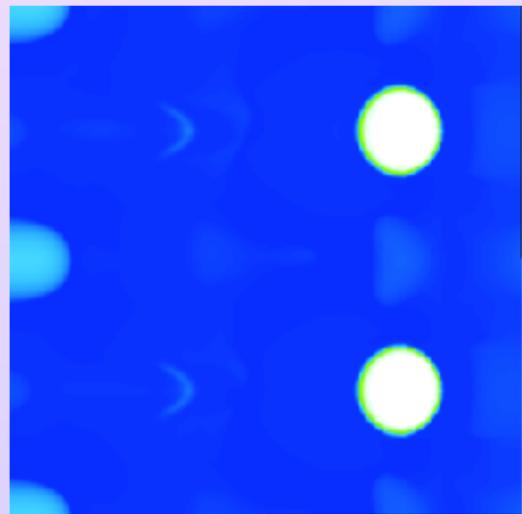
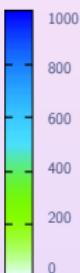
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◀ Geometry

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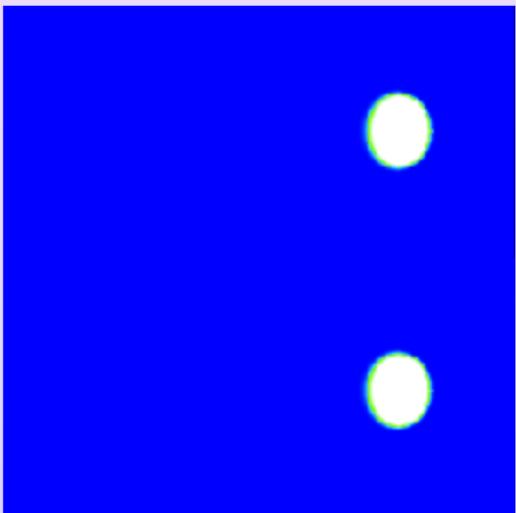
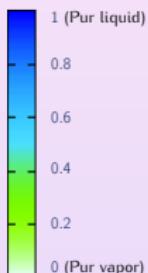
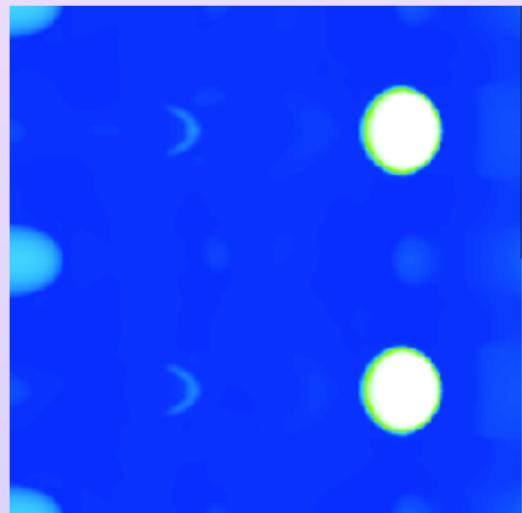
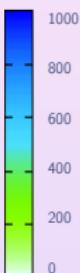
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◀ Geometry

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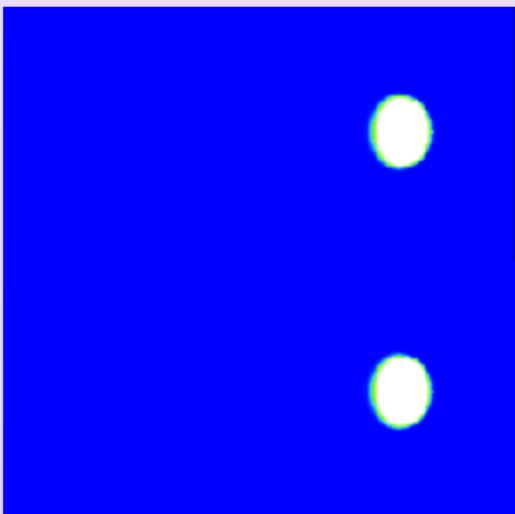
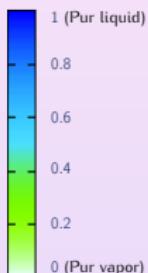
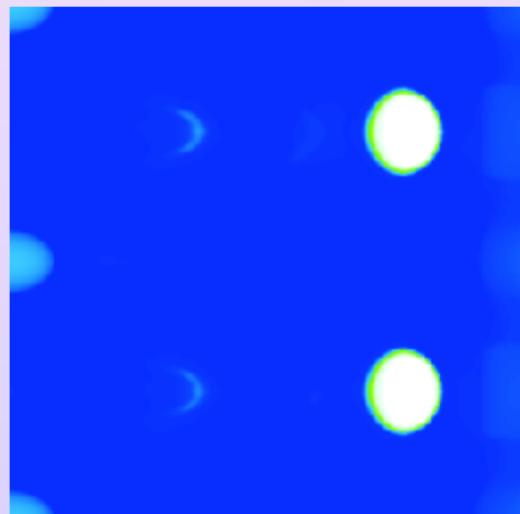
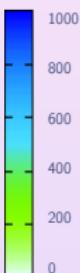
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▶ Skip

# COMPRESSION OF VAPOR BUBBLES

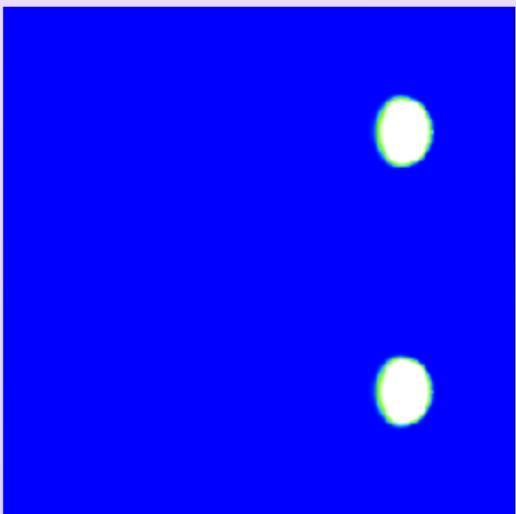
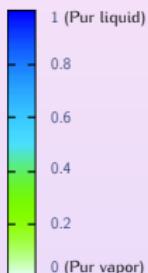
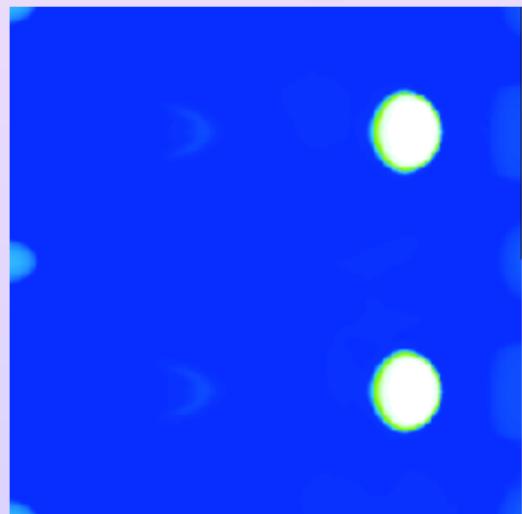
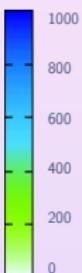
Massee fraction  $y$ Density  $\varrho$ 

◀ Geometry

▶ Play

▶ Skip

# COMPRESSION OF VAPOR BUBBLES

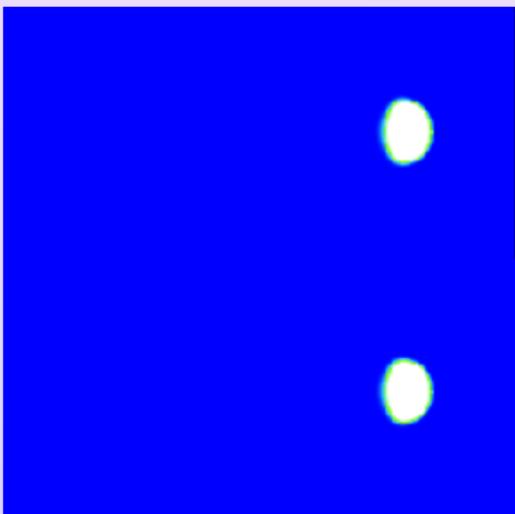
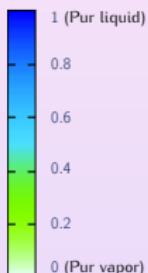
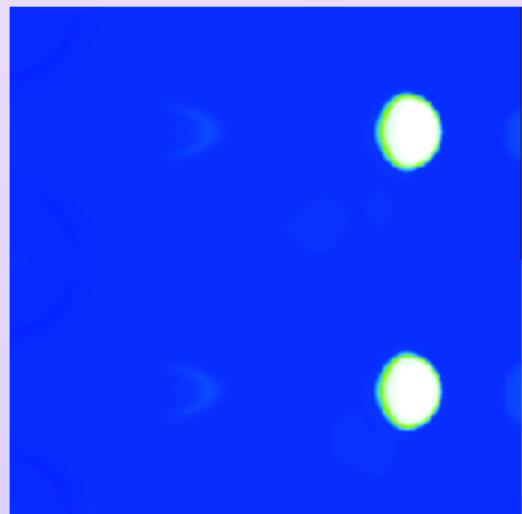
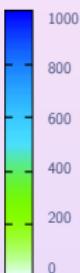
Massee fraction  $y$ Density  $\varrho$ 

◀ Geometry

▶ Play

▶ Skip

# COMPRESSION OF VAPOR BUBBLES

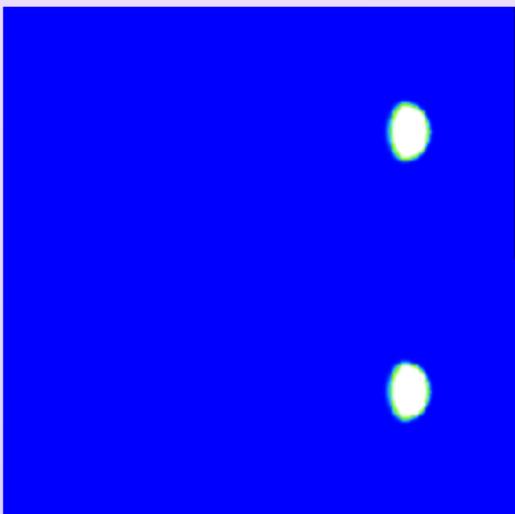
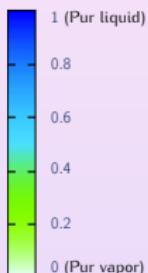
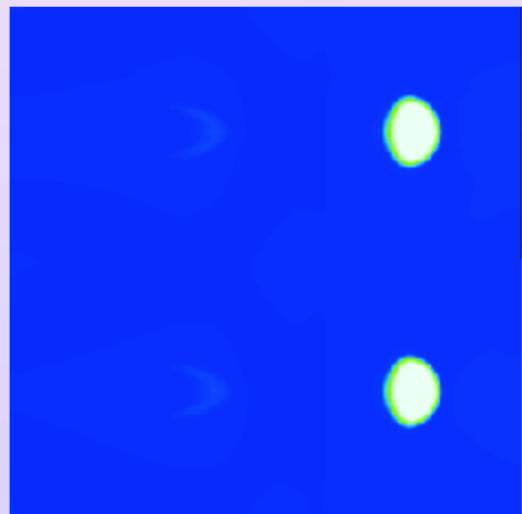
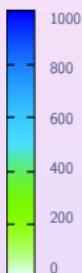
Massee fraction  $y$ Density  $\varrho$ 

◀ Geometry

▶ Play

▶ Skip

# COMPRESSION OF VAPOR BUBBLES

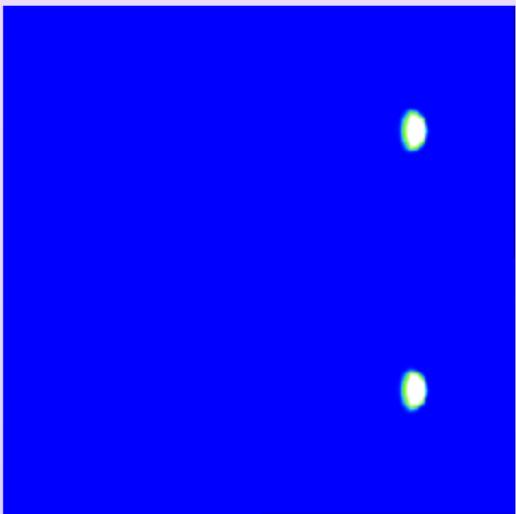
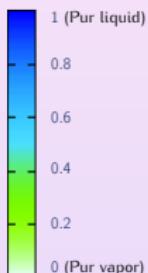
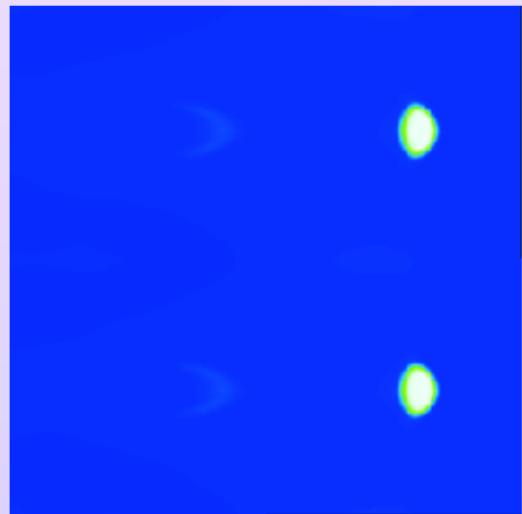
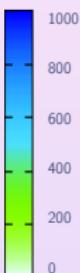
Massee fraction  $y$ Density  $\varrho$ 

◀ Geometry

▶ Play

▶ Skip

# COMPRESSION OF VAPOR BUBBLES

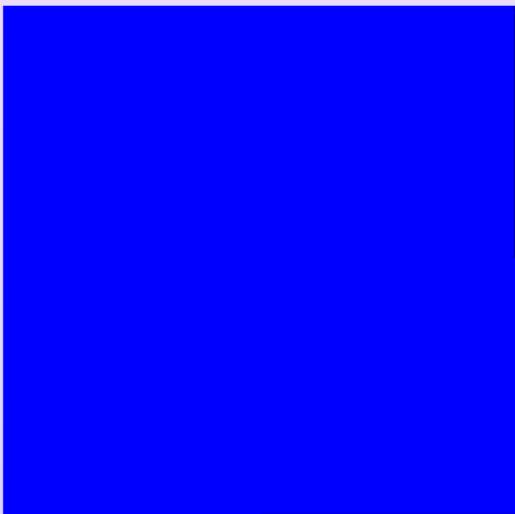
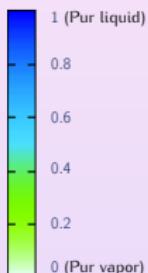
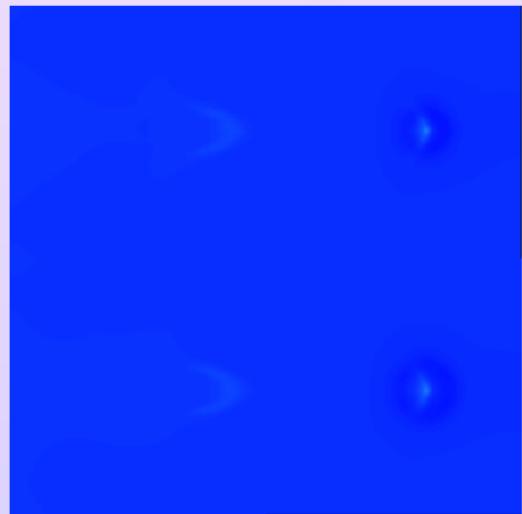
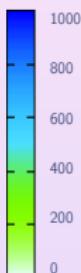
Massee fraction  $y$ Density  $\varrho$ 

◀ Geometry

▶ Play

▶ Skip

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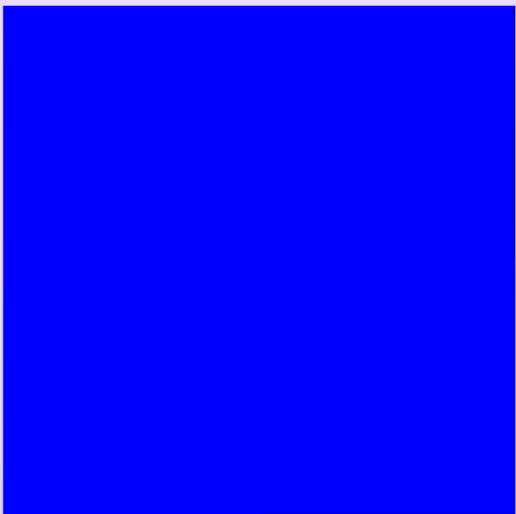
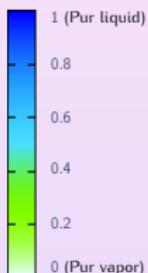
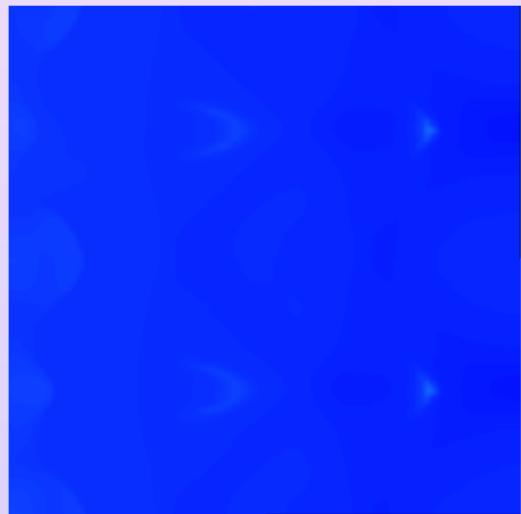
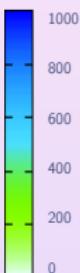
Massee fraction  $y$ Density  $\varrho$ 

◀ Geometry

▶ Play

▶ Skip

# COMPRESSION OF VAPOR BUBBLES

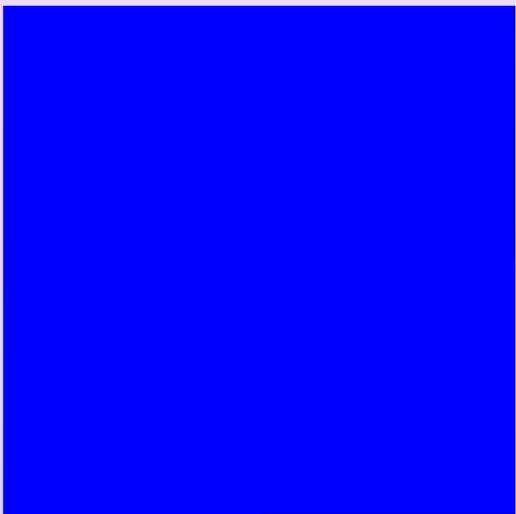
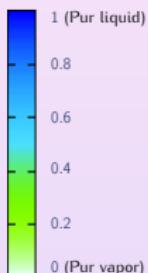
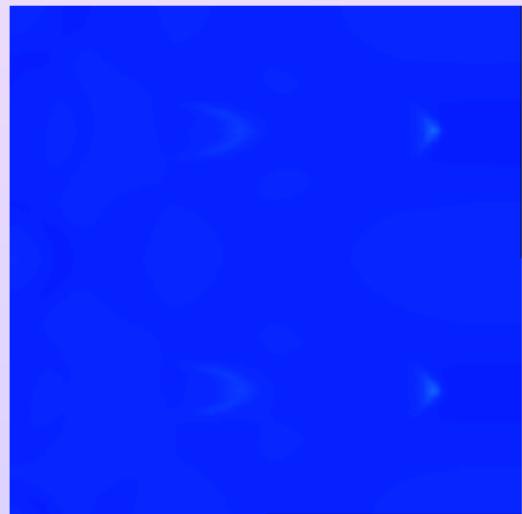
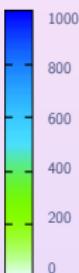
Massee fraction  $y$ Density  $\varrho$ 

◀ Geometry

▶ Play

▶ Skip

# COMPRESSION OF VAPOR BUBBLES

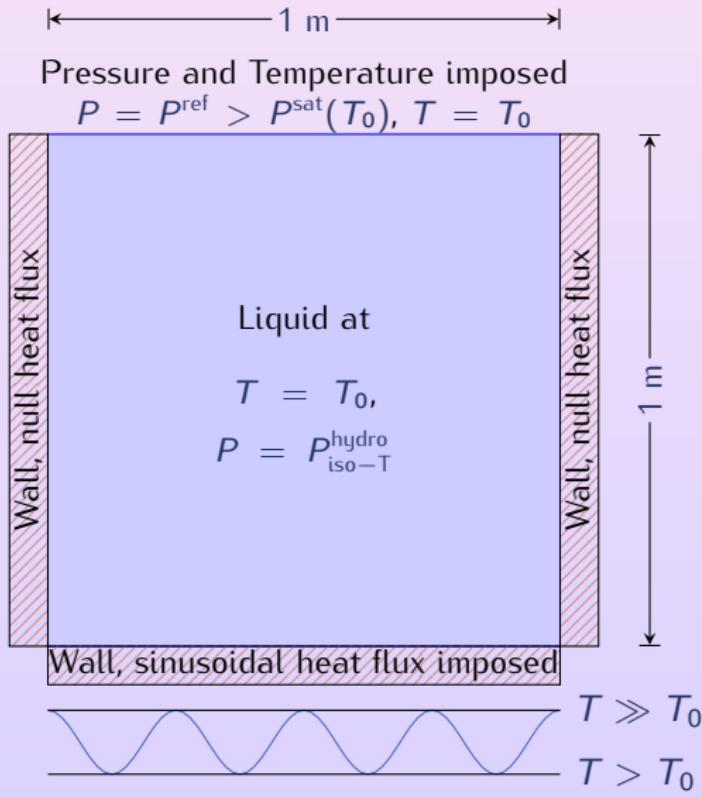
Massee fraction  $y$ Density  $\varrho$ 

◀ Geometry

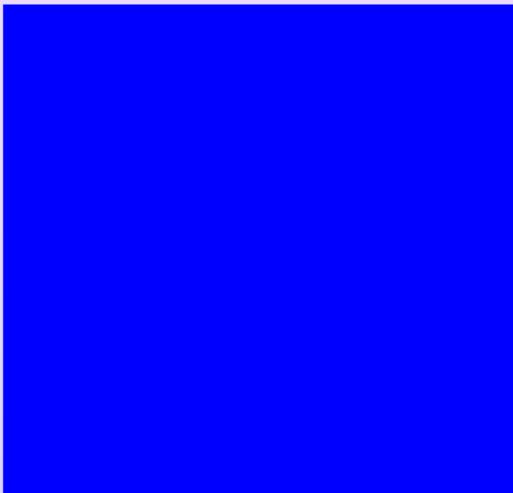
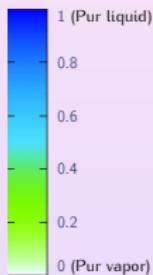
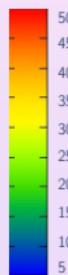
▶ Play

▶ Skip

# TRANSITION TO A FILM BOILING



# TRANSITION TO A FILM BOILING

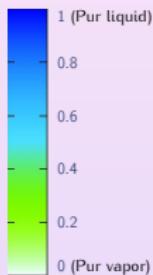
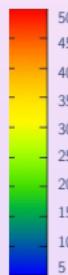
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

# TRANSITION TO A FILM BOILING

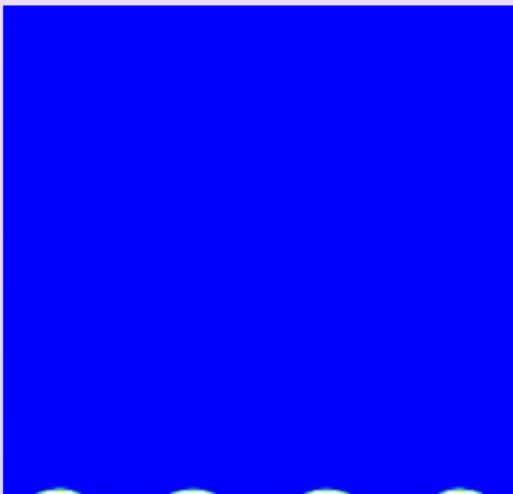
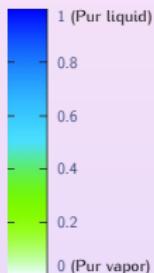
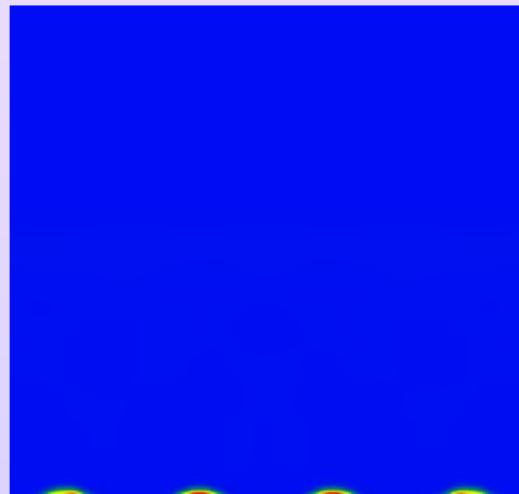
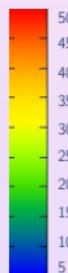
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

# TRANSITION TO A FILM BOILING

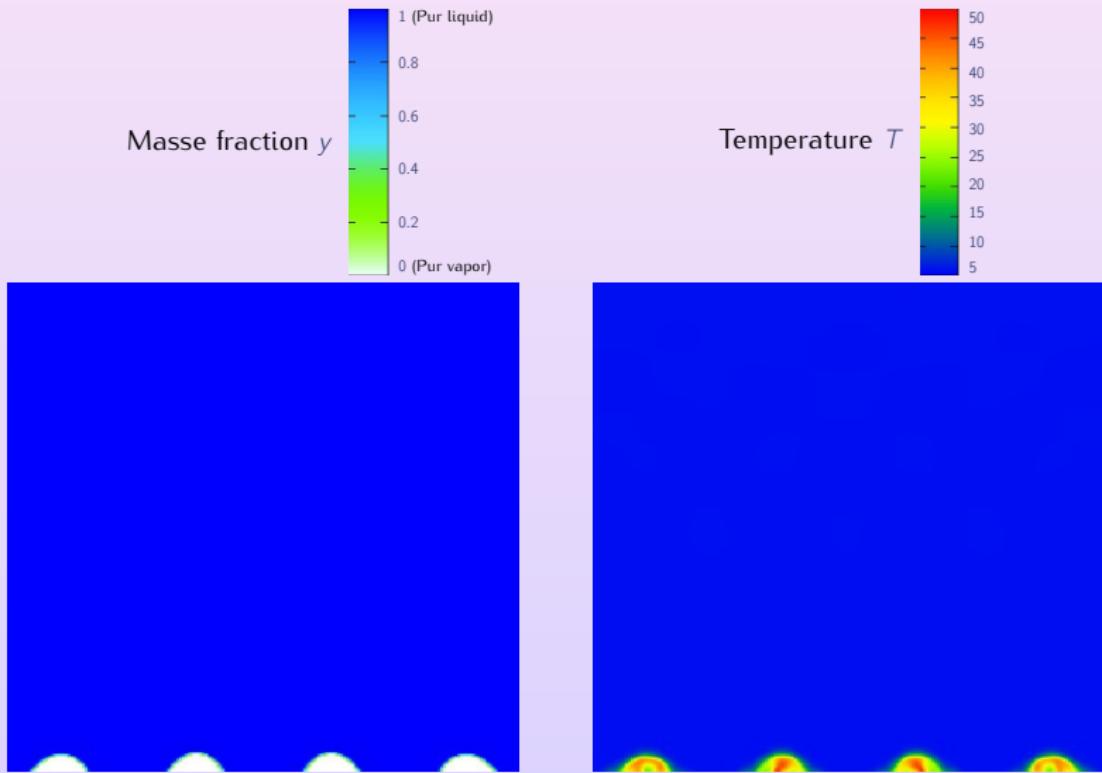
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

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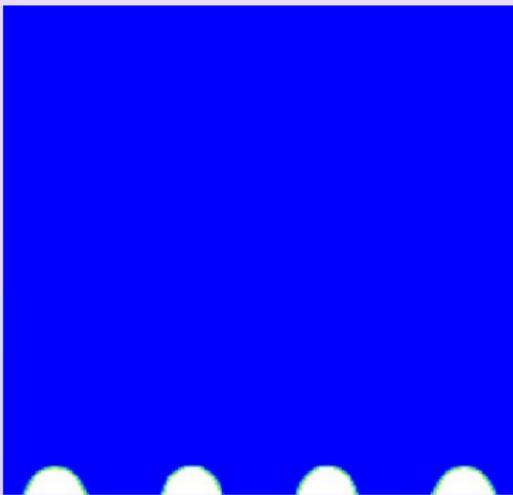
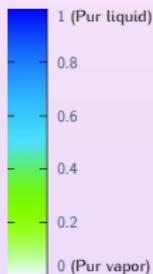
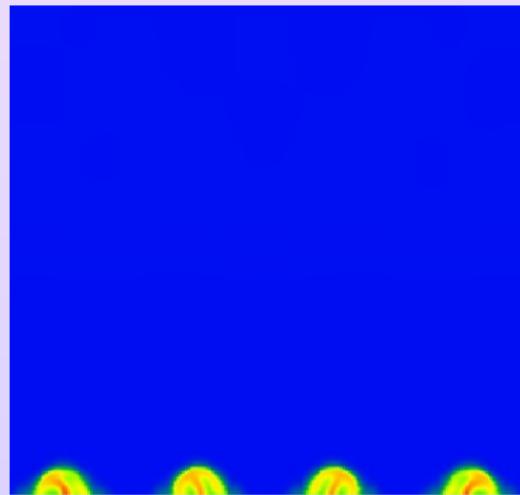
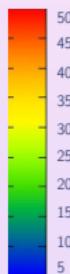


◀ Geometry

▶ Play

▶ Skip

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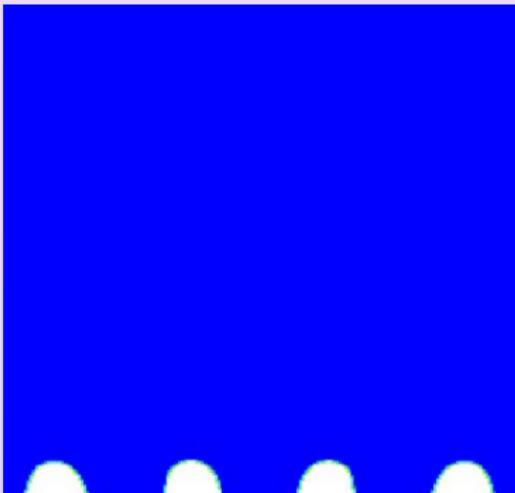
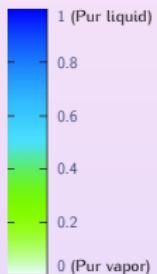
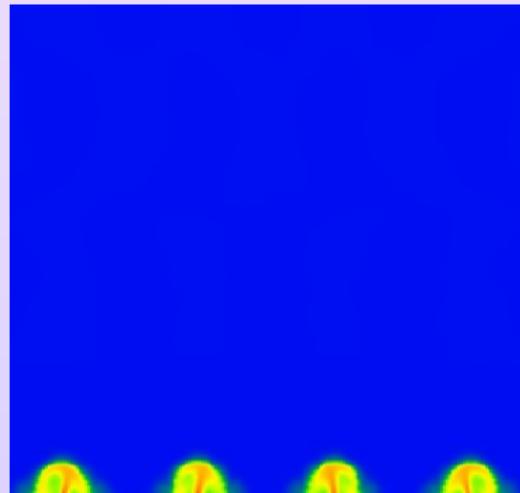
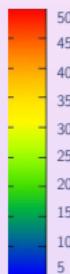
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

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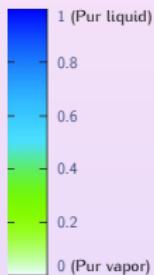
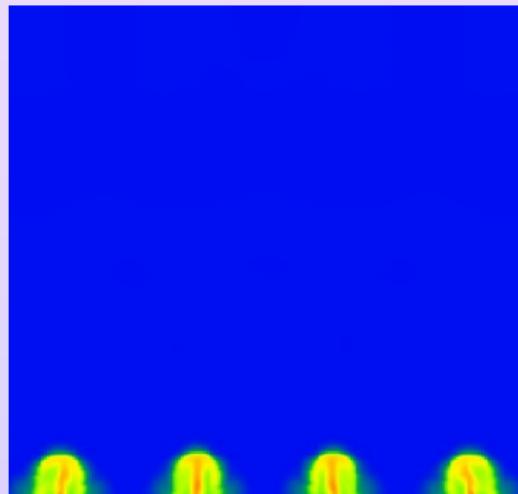
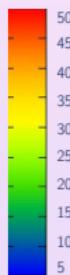
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

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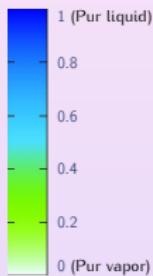
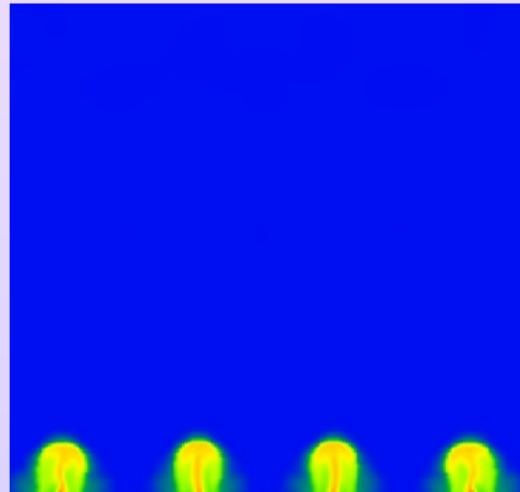
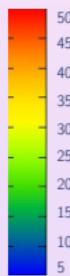
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

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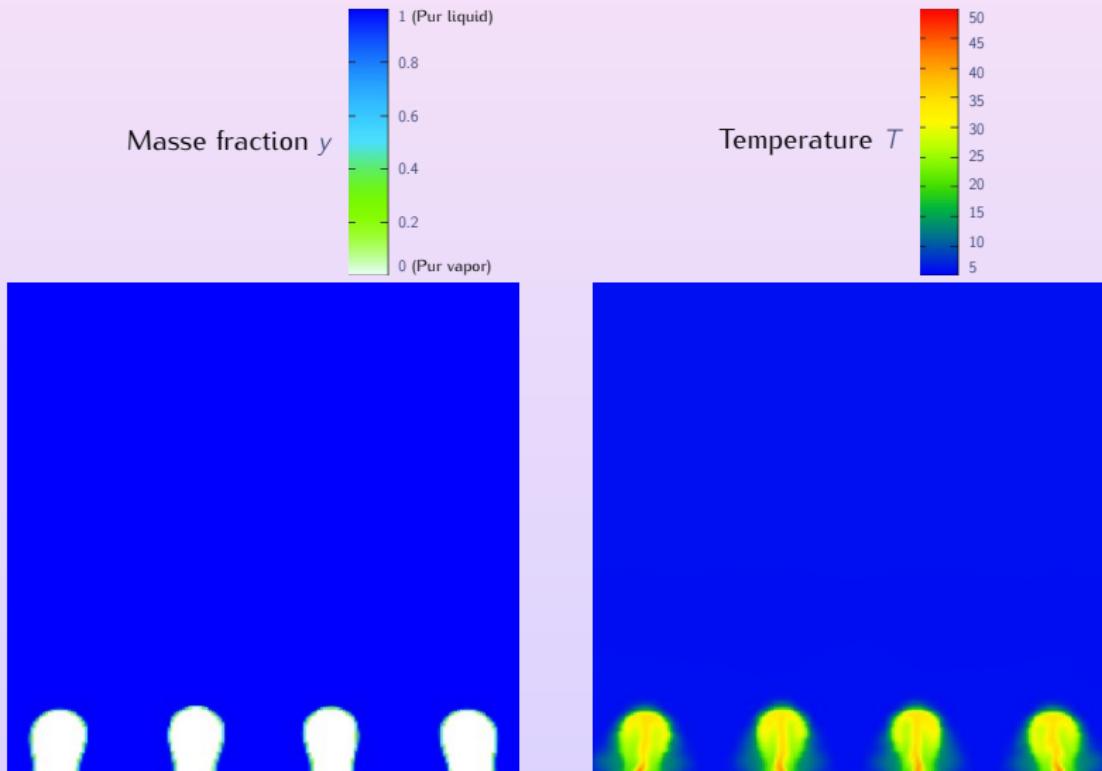
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

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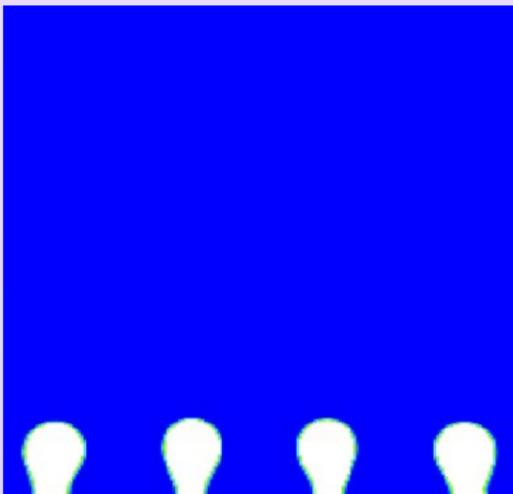
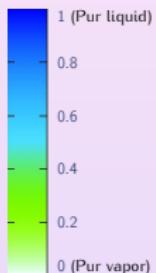
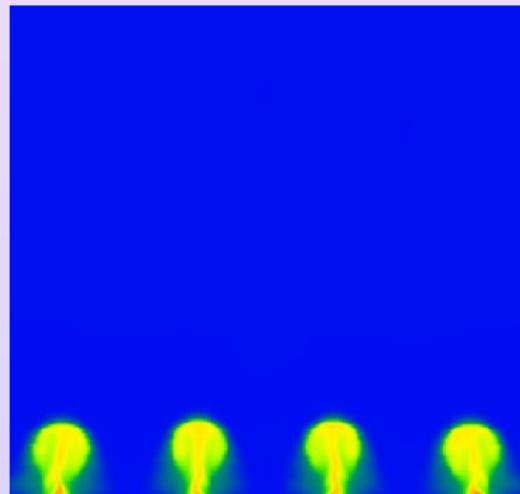
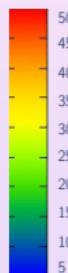


◀ Geometry

▶ Play

▶ Skip

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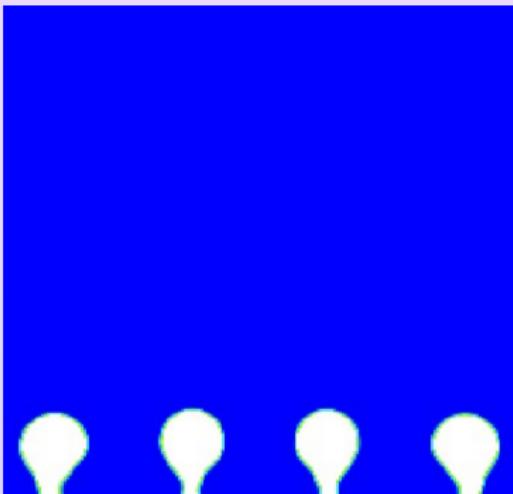
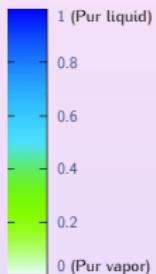
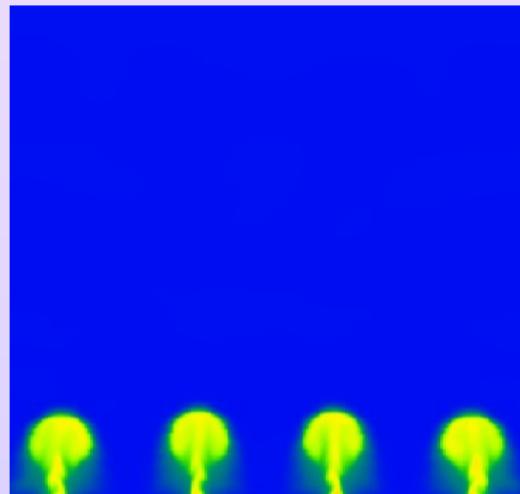
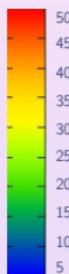
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

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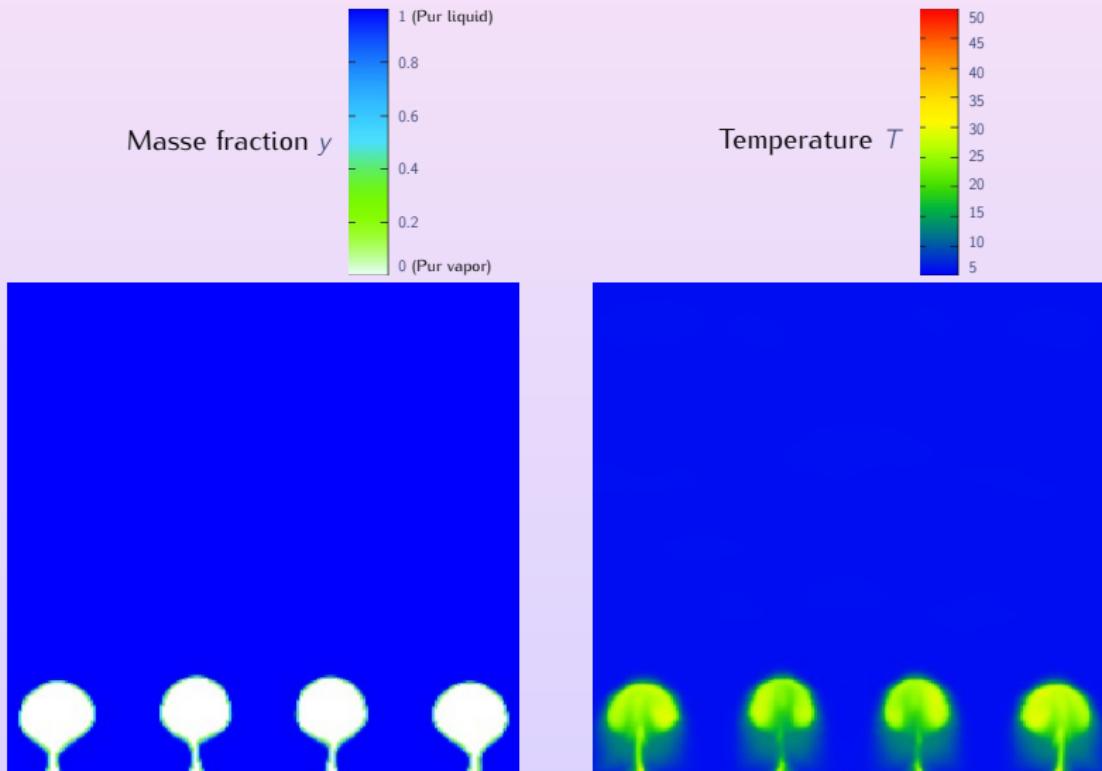
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

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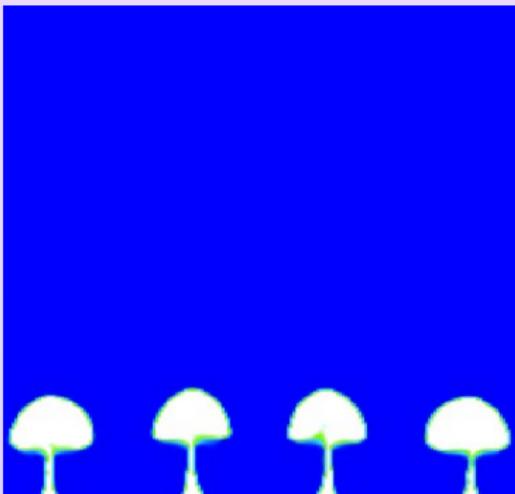
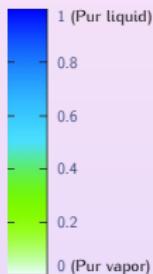
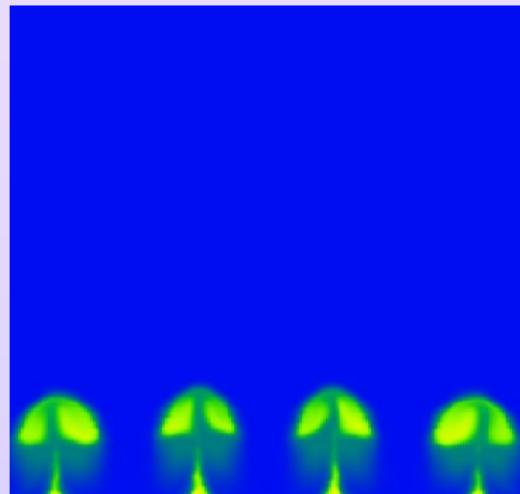
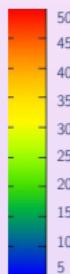


◀ Geometry

▶ Play

▶ Skip

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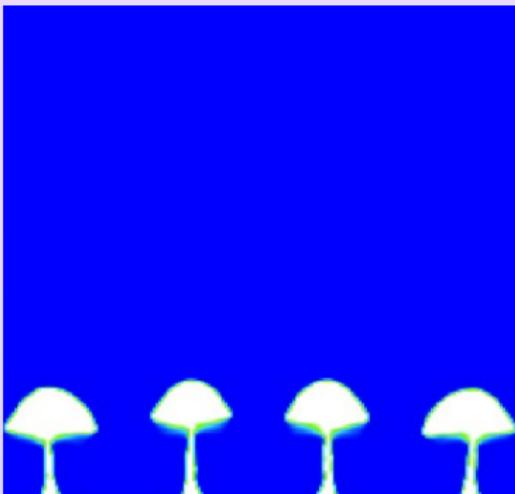
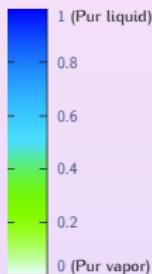
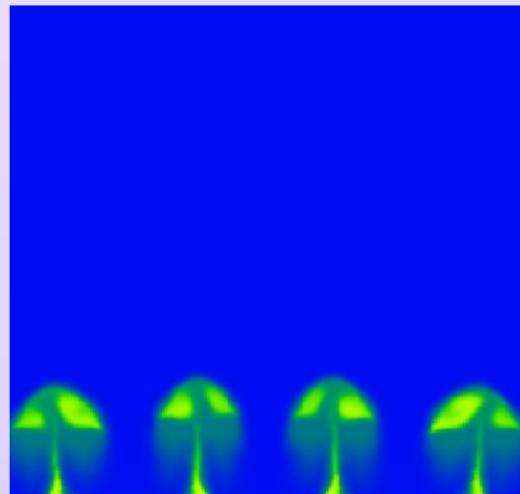
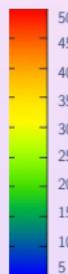
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

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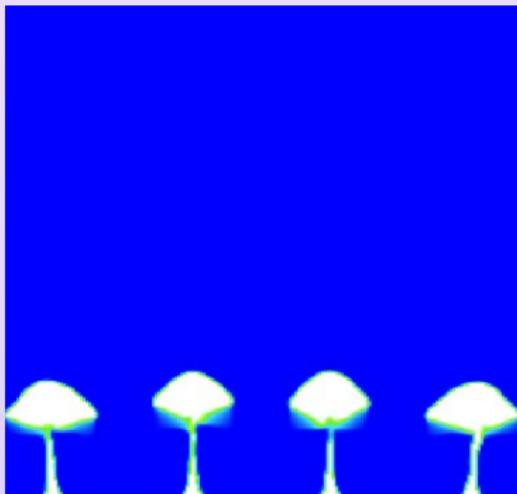
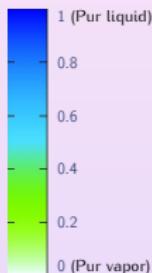
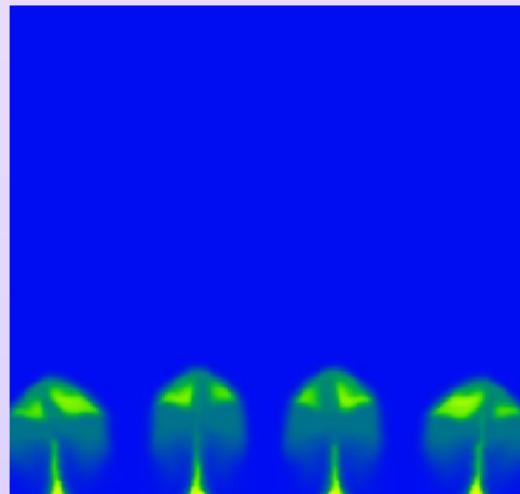
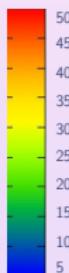
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

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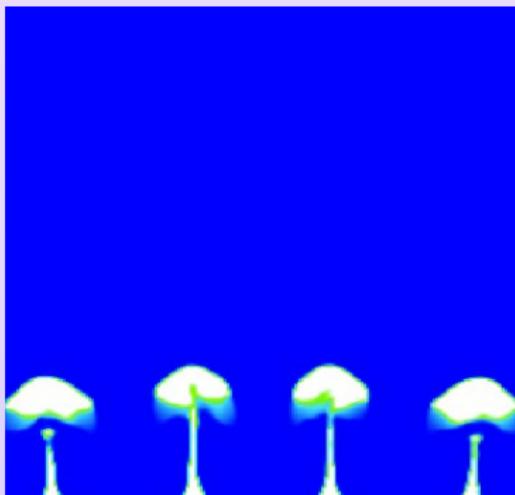
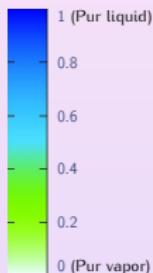
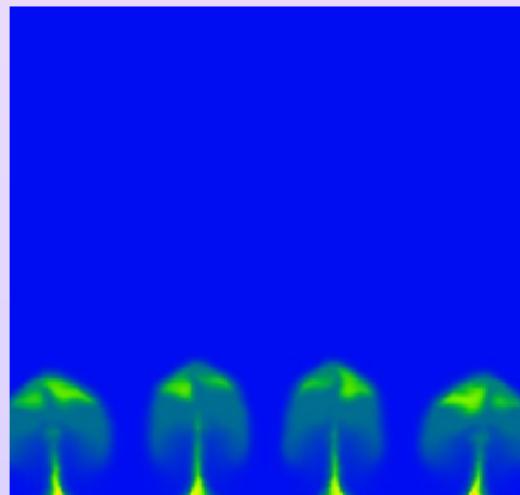
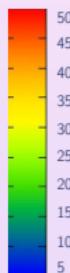
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

# TRANSITION TO A FILM BOILING

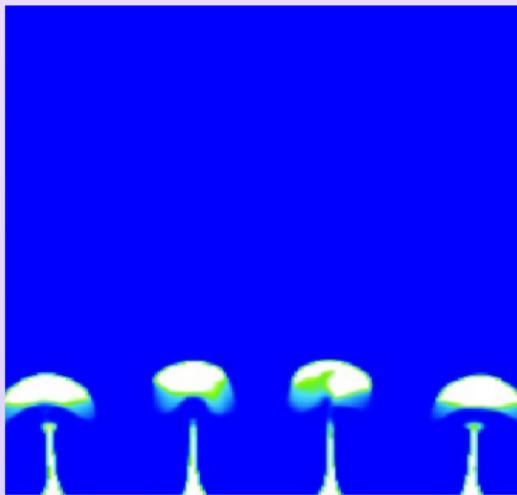
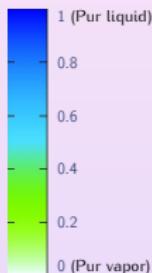
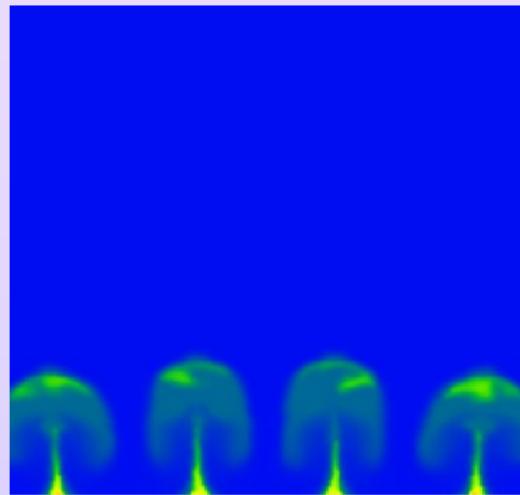
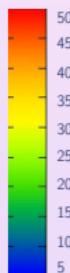
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

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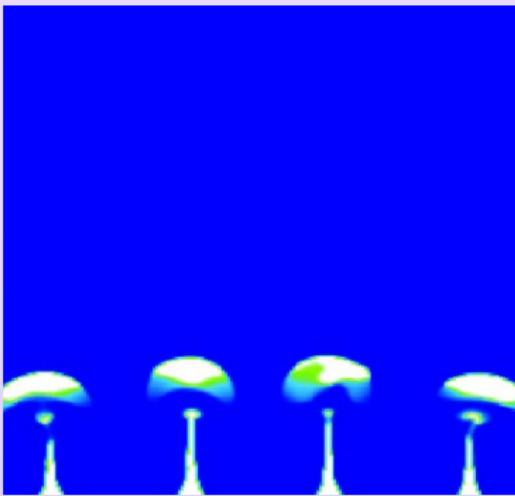
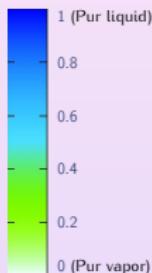
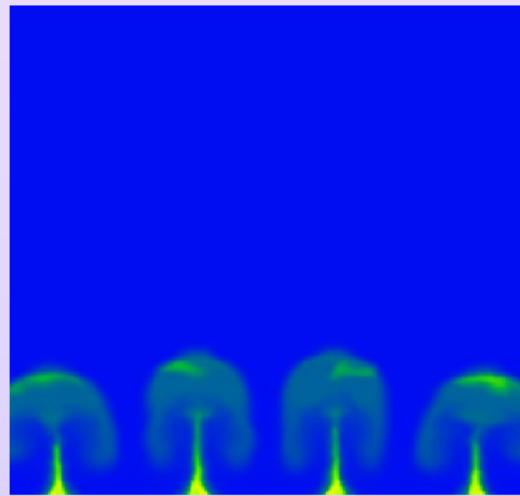
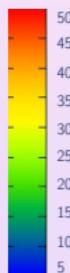
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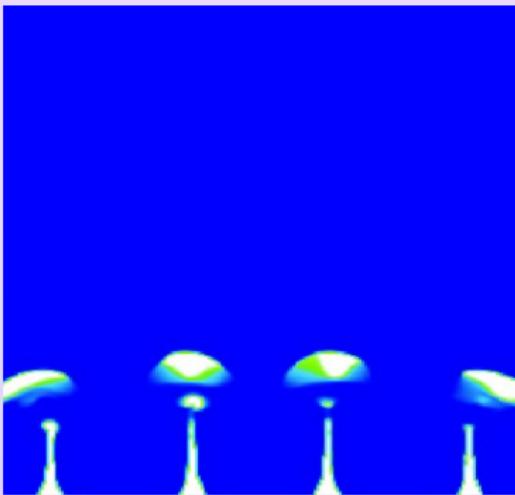
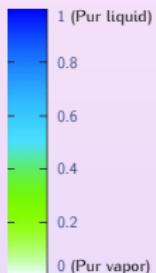
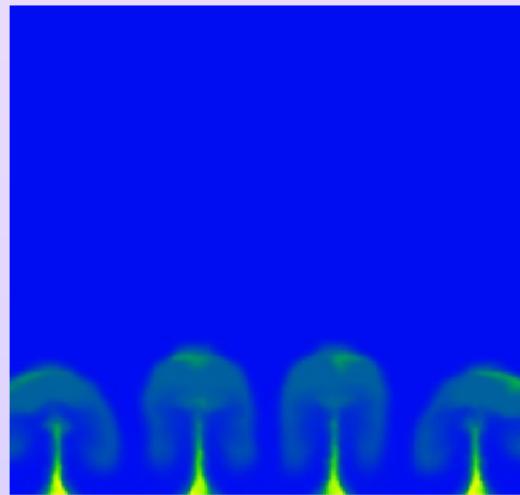
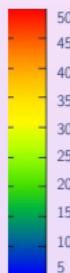
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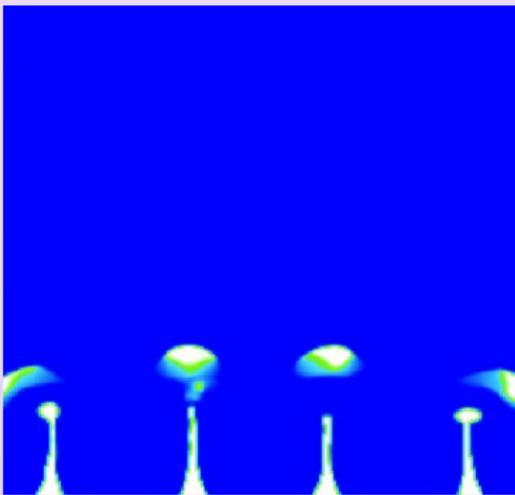
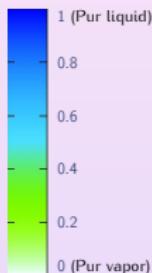
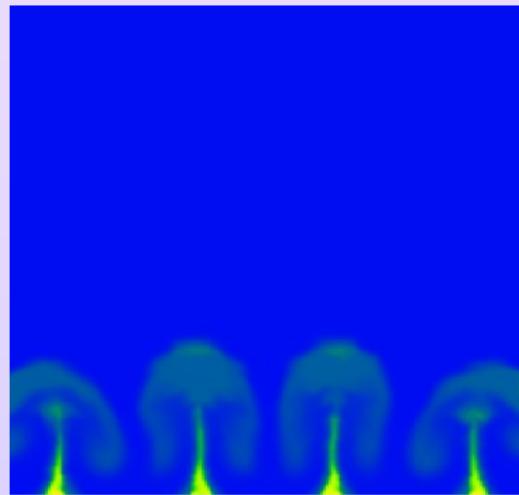
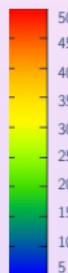
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◀ Geometry

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▶ Skip

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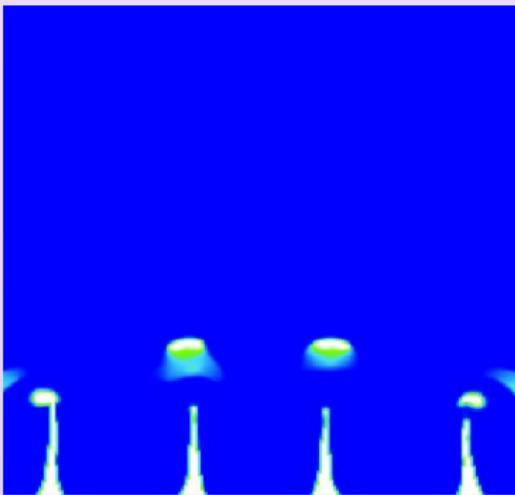
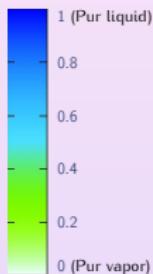
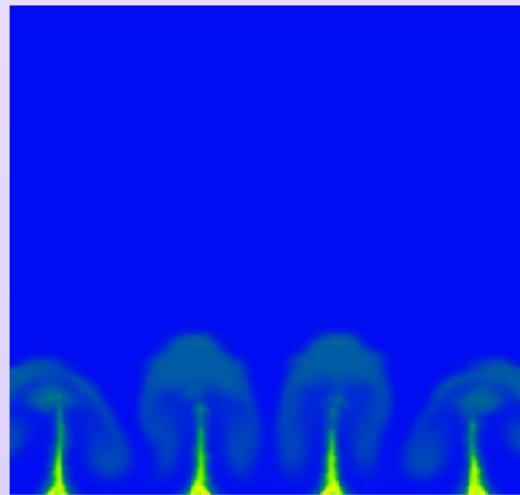
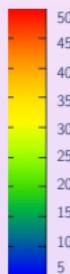
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◀ Geometry

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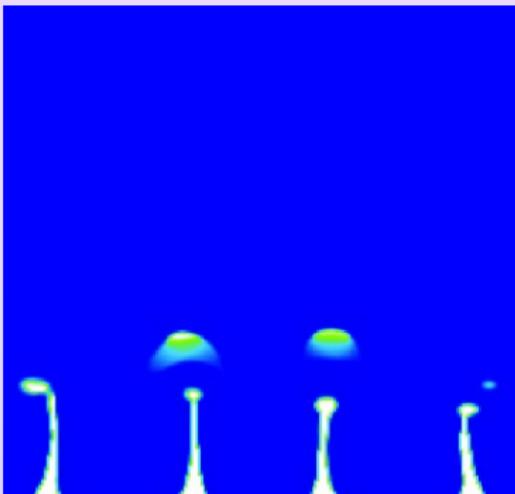
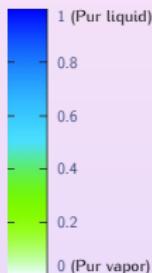
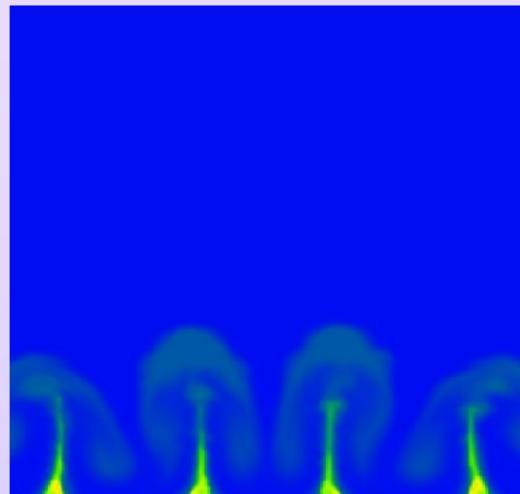
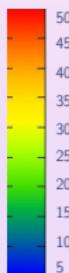
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◀ Geometry

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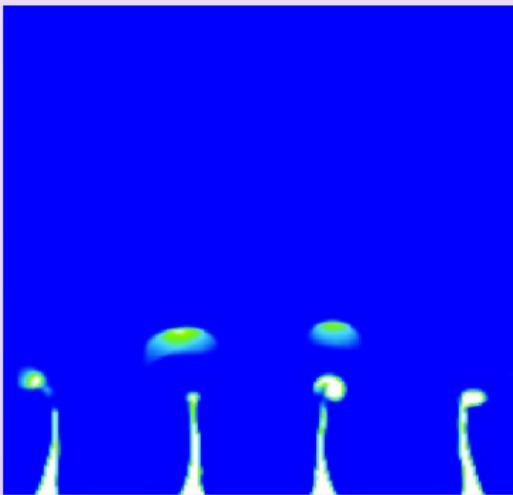
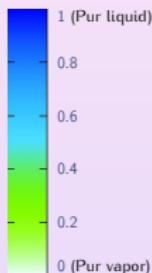
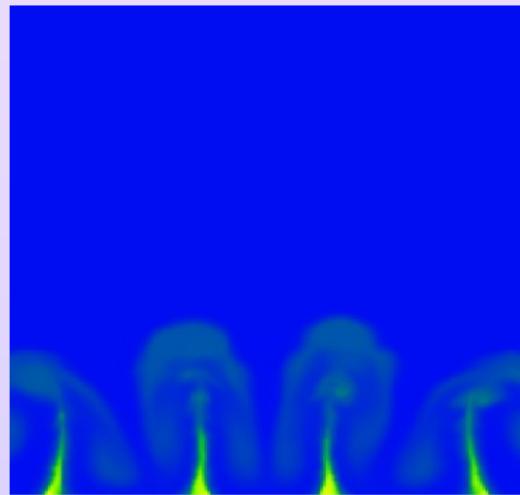
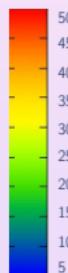
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◀ Geometry

▶ Play

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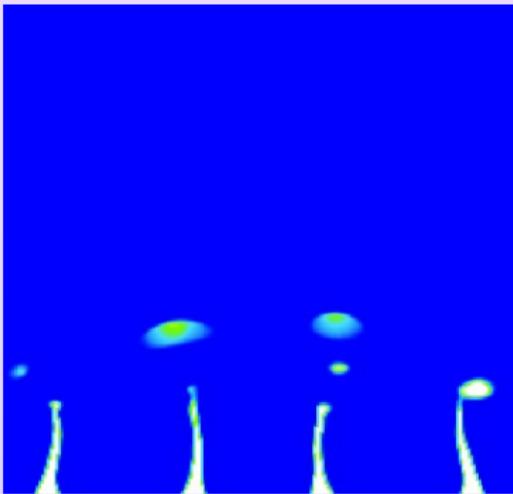
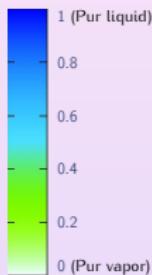
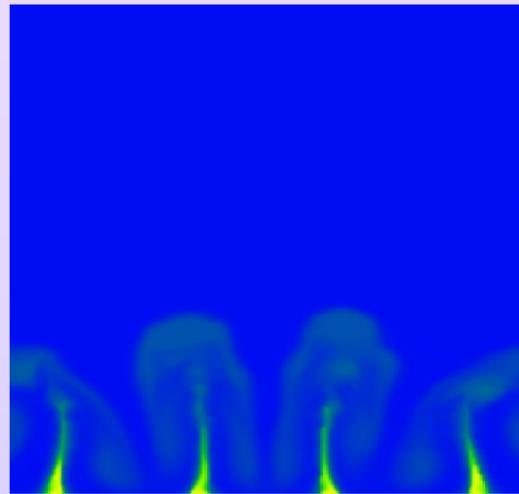
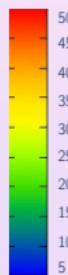
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

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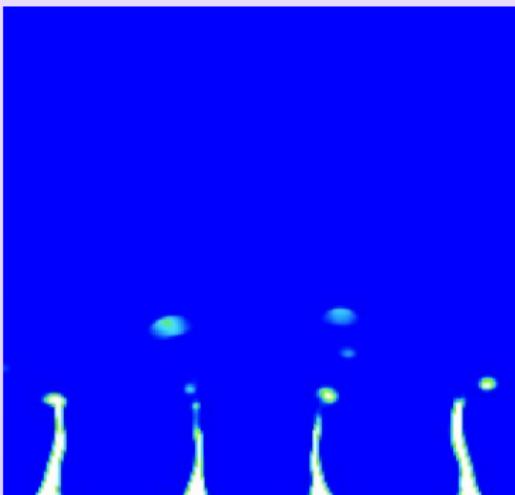
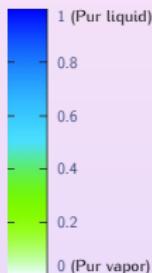
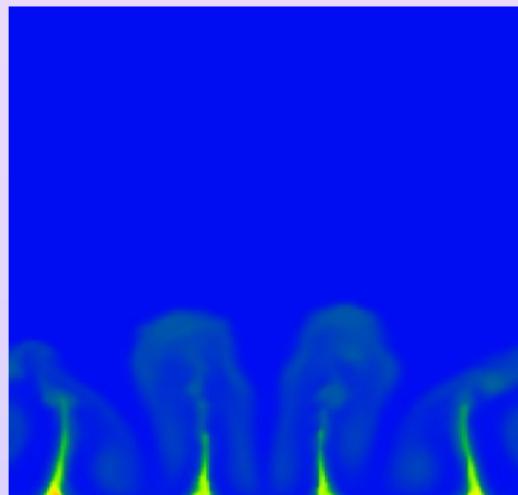
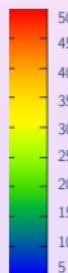
Massee fraction  $y$ Temperature  $T$ 

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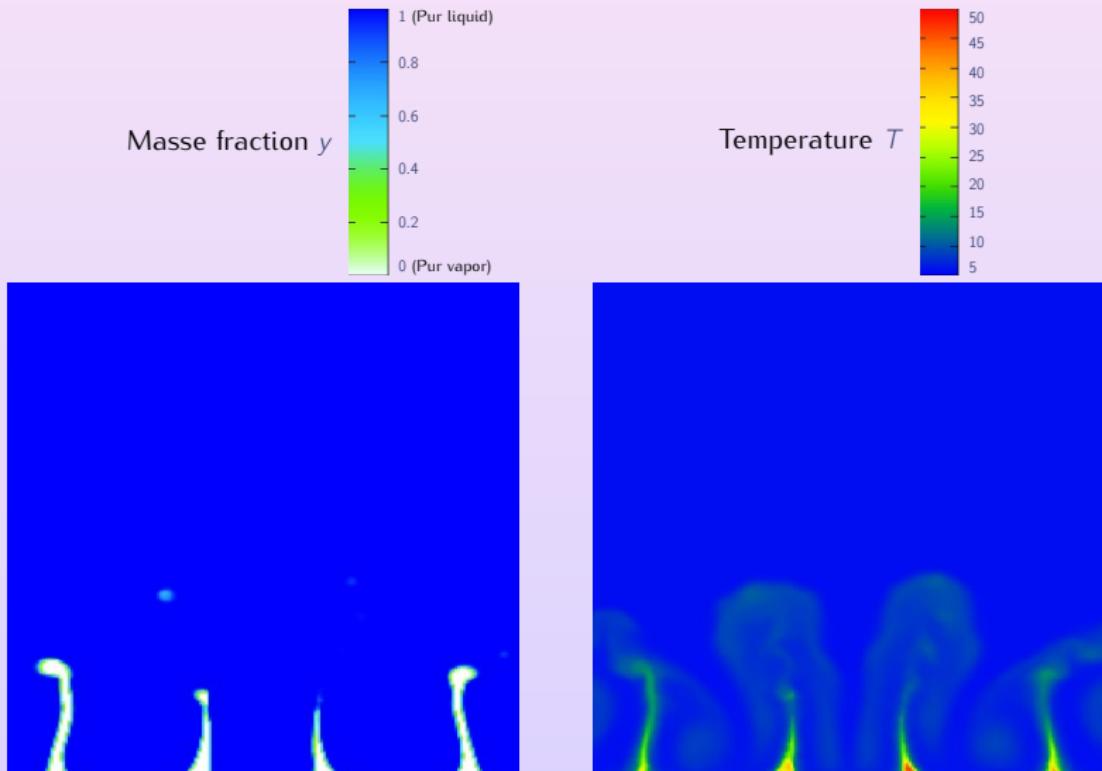
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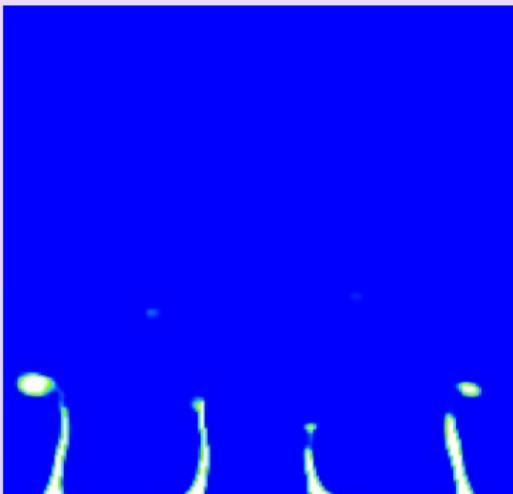
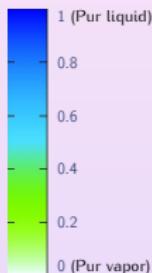
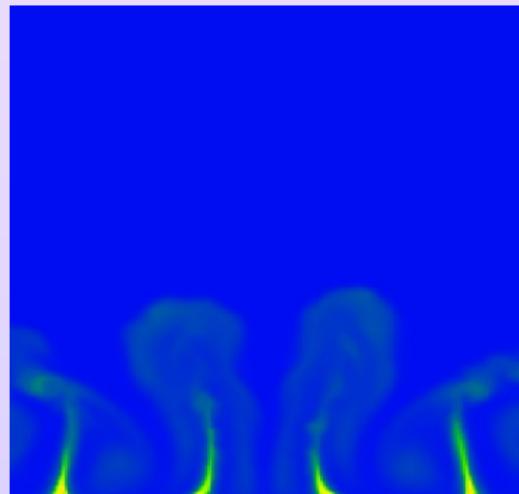
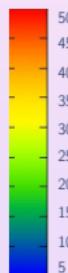


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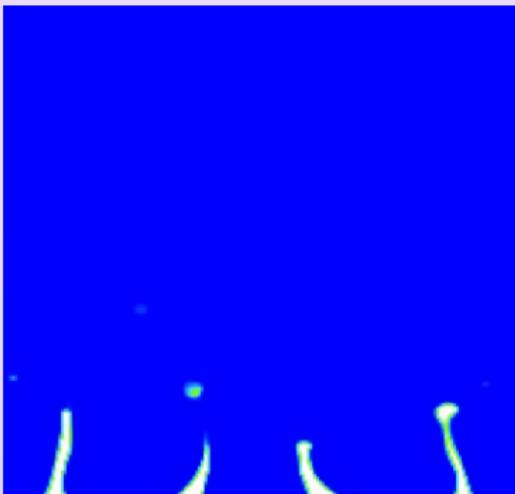
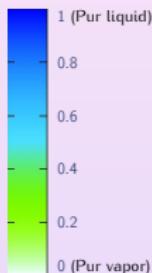
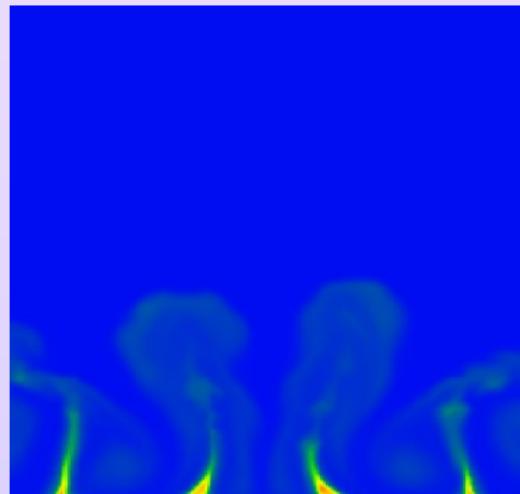
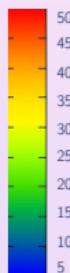
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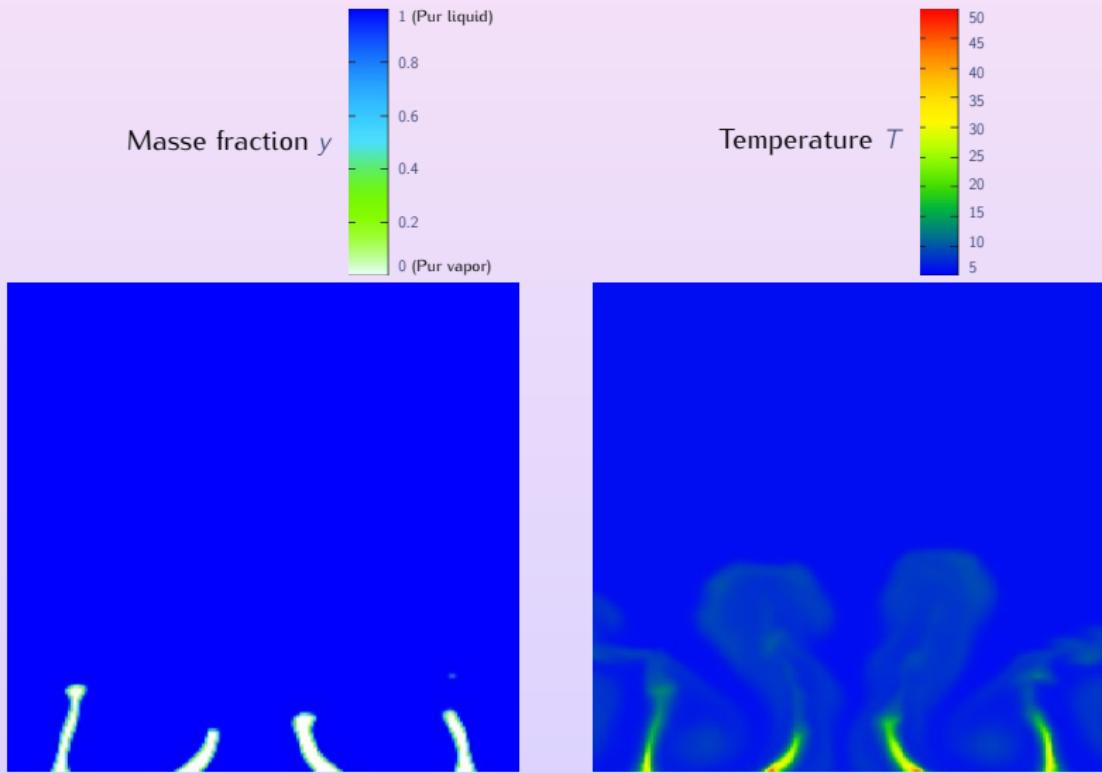
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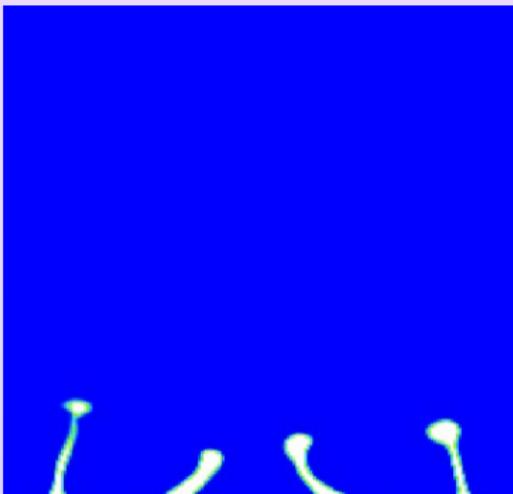
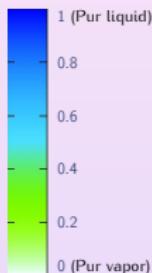
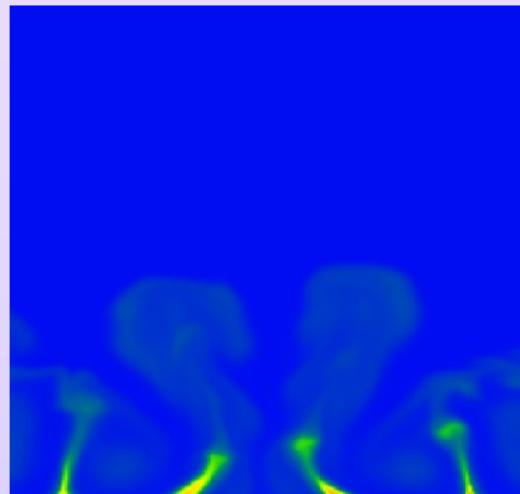
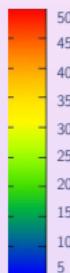


◀ Geometry

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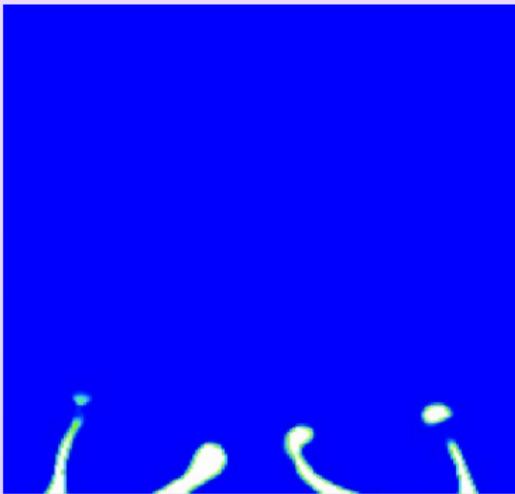
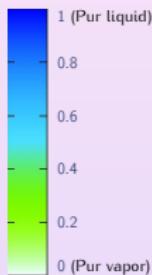
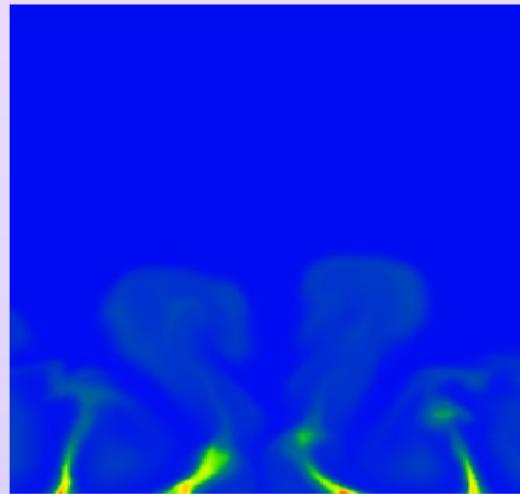
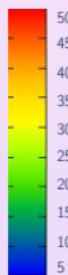
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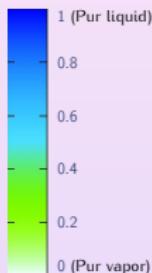
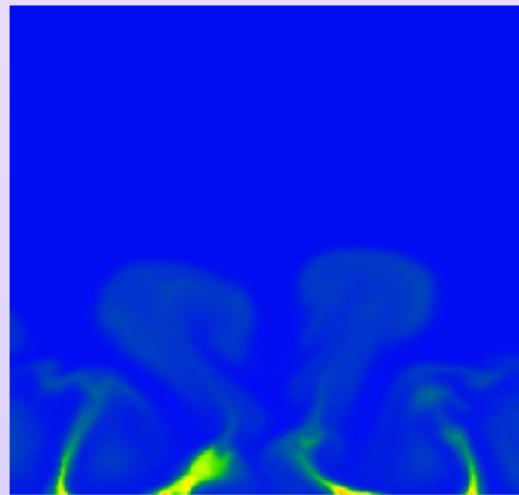
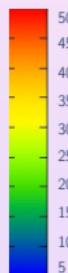
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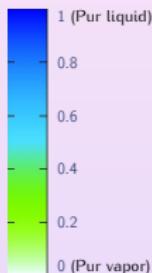
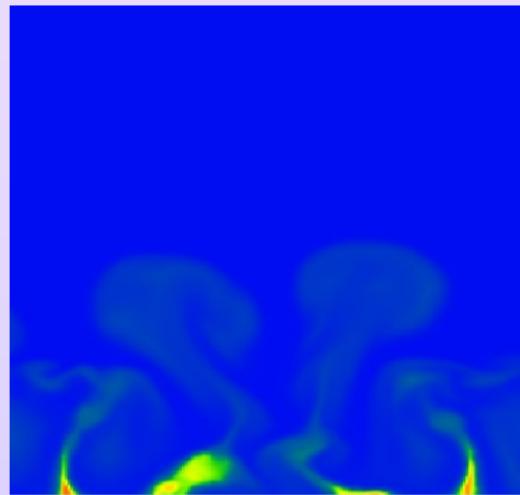
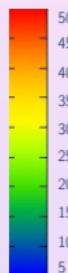
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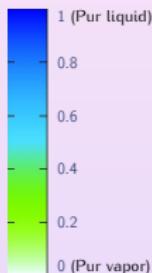
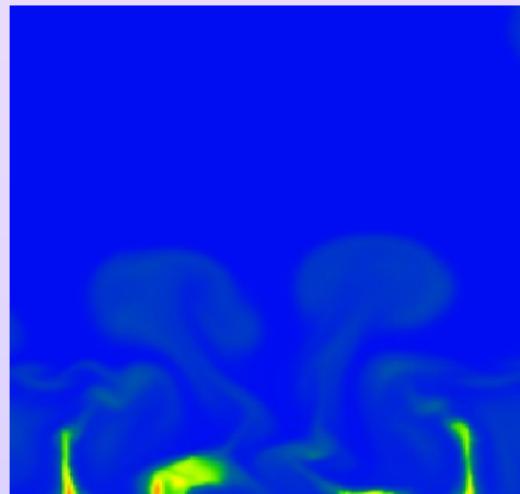
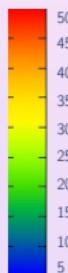
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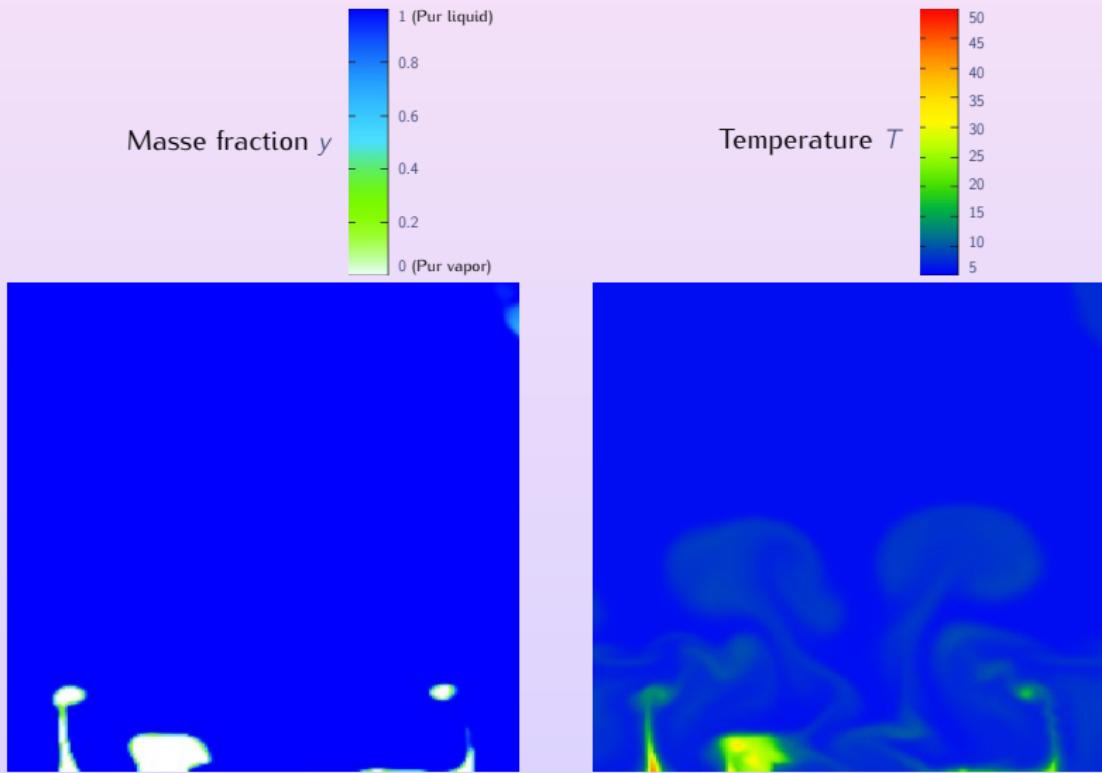
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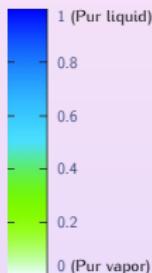
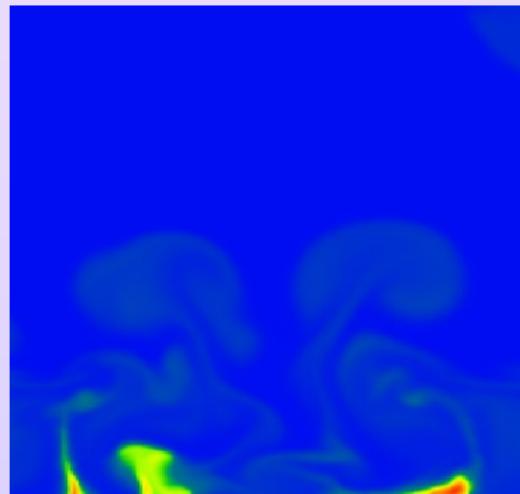
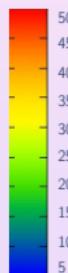


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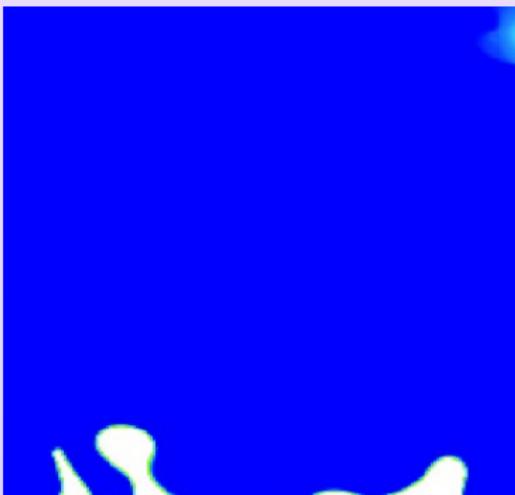
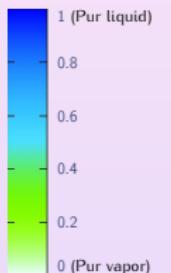
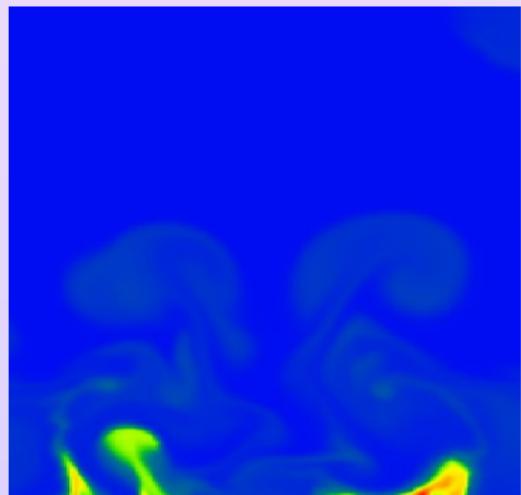
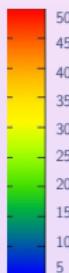
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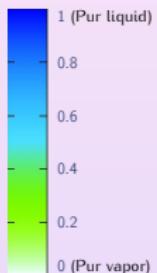
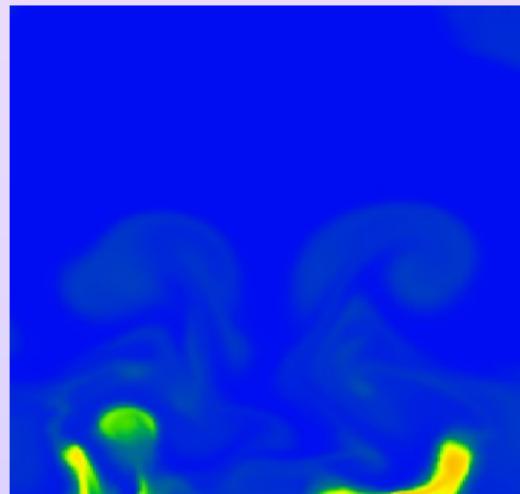
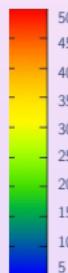
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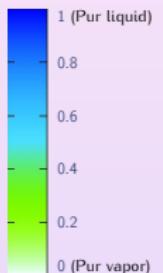
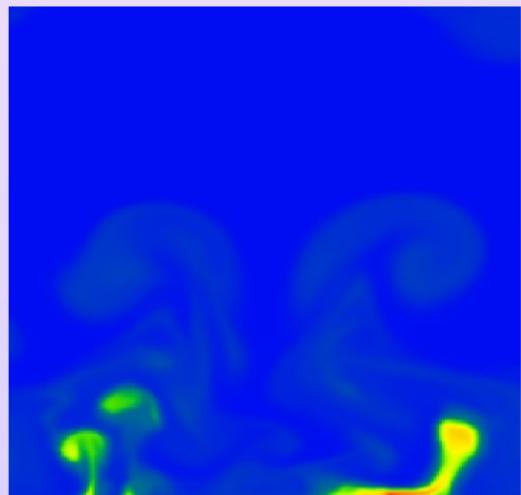
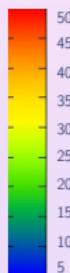
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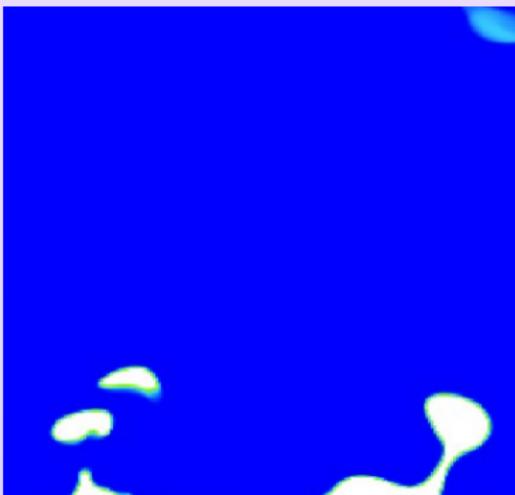
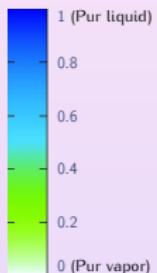
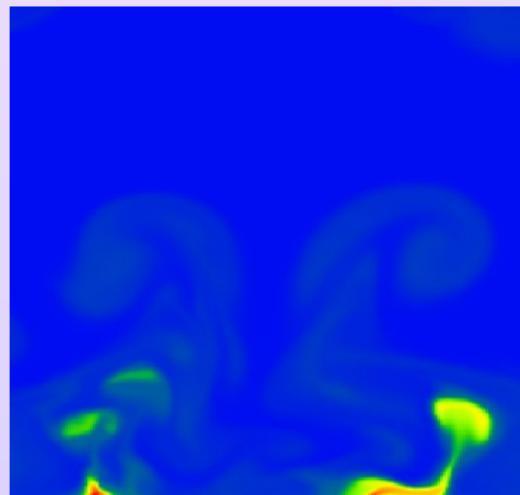
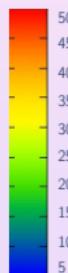
Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

# TRANSITION TO A FILM BOILING

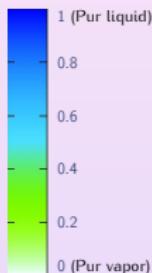
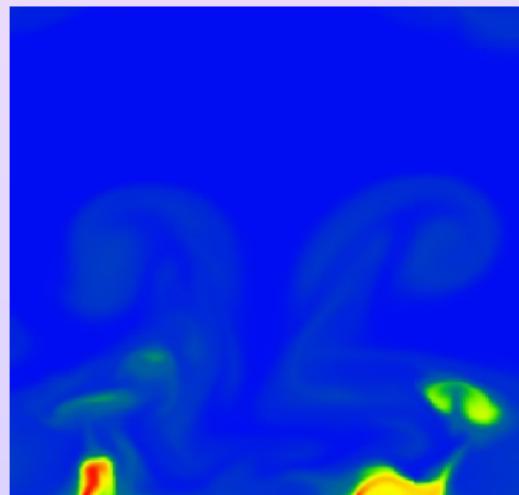
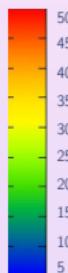
Massee fraction  $y$ Temperature  $T$ 

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▶ Play

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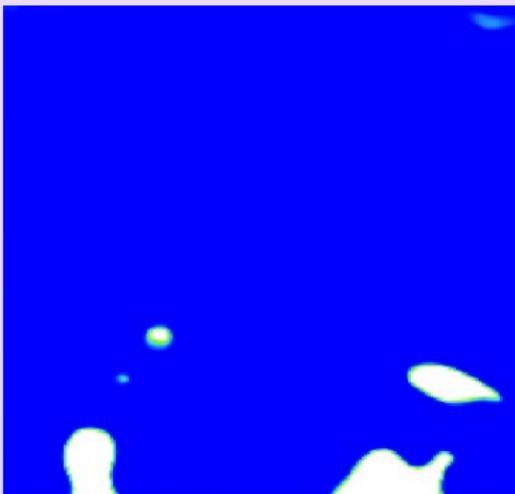
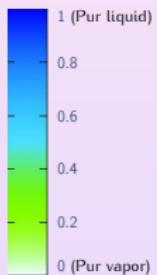
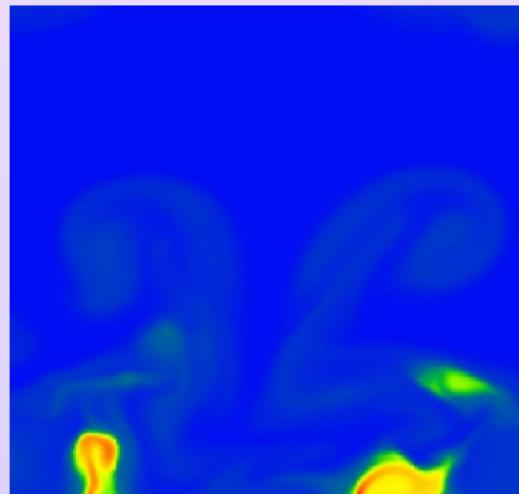
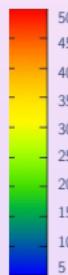
Mass fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

# TRANSITION TO A FILM BOILING

Massee fraction  $y$ Temperature  $T$ 

◀ Geometry

▶ Play

▶ Skip

# OUTLINE

## 1 Context

## 2 Model

- Equation of State
- Conservation Laws

## 3 Numerical Approximation and Example

- The Phase Change Equation
- Numerical Scheme and Example

## 4 Conclusion

# SUMMARY & PERSPECTIVES

## • Model

- ✓ based on a general construction of the Equilibrium EOS (also for tabulated data),
- Numerical Method based on the relaxation approach: off-equilibrium system with relaxation terms
  - ✓ preliminary results: dynamic generation of a phase in a 2D-flow in a pure phase with surface tension, gravity and heat diffusion,
  - ✓ transition: liquid phase → nucleating boiling → film boiling

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- Model

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- ✓ transition: liquid phase → nucleating boiling → film boiling
- ✗ quantitative simulations: tabulated EOS for pure phases, implicit transport step (Low Mach) and 3D (parallelization).



# APPENDIX

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- ▶ Stiffened Gas for Water
- ▶ Tabulated EOS for Water
- ▶ Speed of Sound
- ▶ Isentropic Curves
- ▶ Surface Tension
- ▶ Metastability
- ▶ Critical Point
- ▶ Summary & To Do

# STIFFENED GAS FOR WATER

Phase	$c_v$ [J/(kg · K)]	$\gamma$	$\pi$ [Pa]	$q$ [J/kg]	$m$ [J/(kg · K)]
Water	1816.2	2.35	$10^9$	$-1167.056 \times 10^3$	-32765.55596
Steam	1040.14	1.43	0	$2030.255 \times 10^3$	-33265.65947

**Table:** Parameters proposed by [O. LE METAYER] for water.

$$(\tau_\alpha, \varepsilon_\alpha) \mapsto s_\alpha = c_{v_\alpha} \ln(\varepsilon_\alpha - q_\alpha - \pi_\alpha \tau_\alpha) + c_{v_\alpha} (\gamma_\alpha - 1) \ln \tau_\alpha + m_\alpha$$

$$(P, T) \mapsto \varepsilon_\alpha = c_{v_\alpha} T \frac{P + \pi_\alpha \gamma_\alpha}{P + \pi_\alpha} + q_\alpha, \quad (P, T) \mapsto \tau_\alpha = c_{v_\alpha} (\gamma_\alpha - 1) \frac{T}{P + \pi_\alpha}.$$

$$\left. \begin{array}{l} T^i = 278\text{K} \dots 610\text{K}, \\ g_1(P, T^i) = g_2(P, T^i) \Rightarrow P^{\text{sat}}(T^i) \end{array} \right\} \Rightarrow \mathfrak{A} = \{(T^i, P^{\text{sat}}(T^i))\}_{i=0}^{83}$$

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# WATER TABULATED EOS

$$T^i = 278\text{K} \dots 610\text{K}, \quad \varepsilon_\alpha^{\text{sat}}(T^i), \tau_\alpha^{\text{sat}}(T^i) \text{ found in the tables} \quad \left. \right\} \Rightarrow \begin{cases} \mathfrak{A} = \left\{ \left( T_i, \frac{1}{\varepsilon_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{B} = \left\{ \left( T_i, \frac{\varepsilon_{\text{liq}}^{\text{sat}}(T_i)}{\varepsilon_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{C} = \left\{ \left( T_i, \frac{1}{\tau_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{D} = \left\{ \left( T_i, \frac{\tau_{\text{liq}}^{\text{sat}}(T_i)}{\tau_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \end{cases}$$

$\hat{\varepsilon}_\alpha^{\text{sat}}$  and  $\hat{\tau}_\alpha^{\text{sat}}$  defined by using a least square approximation of  $\mathfrak{A}$ ,  $\mathfrak{B}$ ,  $\mathfrak{C}$  and  $\mathfrak{D}$ :

$$T \mapsto \varepsilon_{\text{vap}}^{\text{sat}} \approx \hat{\varepsilon}_{\text{vap}}^{\text{sat}} \stackrel{\text{def}}{=} \frac{1}{\sum_{k=0}^6 a_k T^k}$$

$$T \mapsto \tau_{\text{vap}}^{\text{sat}} \approx \hat{\tau}_{\text{vap}}^{\text{sat}} \stackrel{\text{def}}{=} \frac{1}{\sum_{k=0}^8 c_k T^k}$$

$$T \mapsto \varepsilon_{\text{liq}}^{\text{sat}} \approx \hat{\varepsilon}_{\text{liq}}^{\text{sat}} \stackrel{\text{def}}{=} \hat{\varepsilon}_{\text{vap}}^{\text{sat}}(T) \sum_{k=0}^6 b_k T^k$$

$$T \mapsto \tau_{\text{liq}}^{\text{sat}} \approx \hat{\tau}_{\text{liq}}^{\text{sat}} \stackrel{\text{def}}{=} \hat{\tau}_{\text{vap}}^{\text{sat}}(T) \sum_{k=0}^9 d_k T^k$$

# SPEED OF SOUND

$$c^2 \stackrel{\text{def}}{=} \tau^2 \left( P^{\text{eq}} \frac{\partial P^{\text{eq}}}{\partial \varepsilon} \Big|_{\tau} - \frac{\partial P^{\text{eq}}}{\partial \tau} \Big|_{\varepsilon} \right) = \boxed{-\tau^2 T^{\text{eq}}} \quad \boxed{[P^{\text{eq}}, -1] \begin{bmatrix} S_{\varepsilon\varepsilon}^{\text{eq}} & S_{\tau\varepsilon}^{\text{eq}} \\ S_{\tau\varepsilon}^{\text{eq}} & S_{\tau\tau}^{\text{eq}} \end{bmatrix} \begin{bmatrix} P^{\text{eq}} \\ -1 \end{bmatrix}} \leq 0$$

HESSIAN MATRIX OF  $w \mapsto s^{\text{eq}}$

- for all  $w$  pure phase state

$$\mathbf{v}^T d^2 s^{\text{eq}}(\mathbf{w}) \mathbf{v} < 0 \quad \forall \mathbf{v} \neq 0,$$

- for all  $w$  equilibrium mixture state

$$\exists \mathbf{v}(\mathbf{w}) \neq 0 \text{ s.t. } (\mathbf{v}(\mathbf{w}))^T d^2 s^{\text{eq}}(\mathbf{w}) \mathbf{v}(\mathbf{w}) = 0.$$

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$$v^T d^2 s^{\text{eq}}(w) v < 0 \quad \forall v \neq 0,$$

- for all  $w$  equilibrium mixture state

$$\exists v(w) \neq 0 \text{ s.t. } (v(w))^T d^2 s^{\text{eq}}(w) v(w) = 0.$$

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$\forall \mathbf{w}$  equilibrium mixture state,  $\mathbf{v}(\mathbf{w}) \stackrel{?}{\equiv} [P^{\text{eq}}(\mathbf{w}), -1]$

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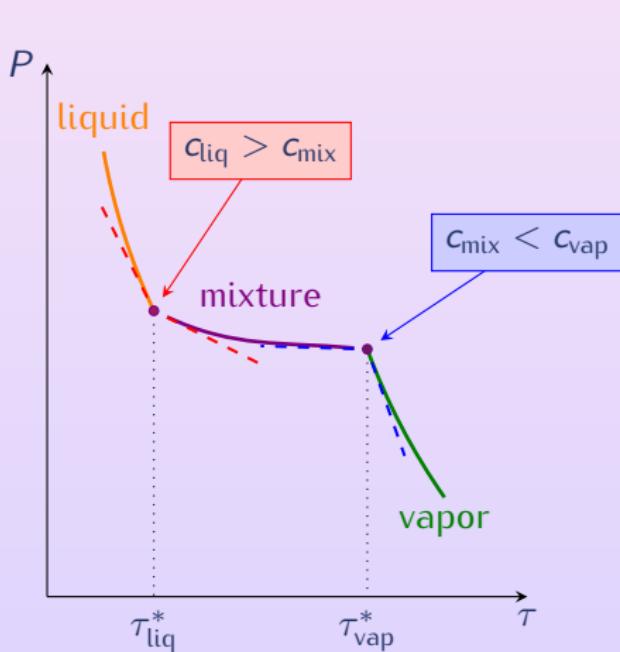
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# ISENTROPIC CURVES



$$\gamma \stackrel{\text{def}}{=} -\frac{\tau}{P} \left. \frac{\partial P}{\partial \tau} \right|_s$$

$$\Gamma \stackrel{\text{def}}{=} \tau \left. \frac{\partial P}{\partial \varepsilon} \right|_\tau$$

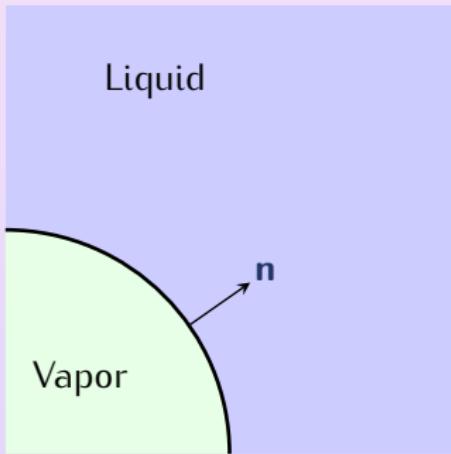
$$\mathfrak{G} \stackrel{\text{def}}{=} \frac{\tau^2}{2\gamma P} \left. \frac{\partial^2 P}{\partial \tau^2} \right|_s$$

- Regularity: [J. CORREIA, P.G. LEFLOCH, M.D. THANH]
- Loss of convexity: [A. Voss]

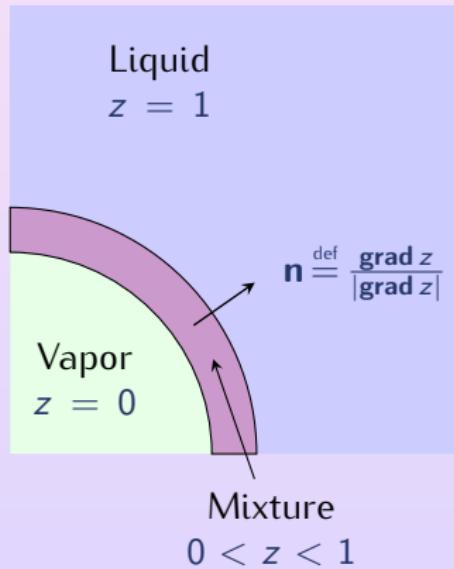
- Pure Phases
  - (H)  $\gamma > 0$
  - (H)  $\Gamma > 0$
  - (H)  $\mathfrak{G} > 0$
- Mixture
  - (P)  $\gamma > 0$
  - (P)  $\Gamma > 0$
  - (H)  $\mathfrak{G} > 0$

# CONTINUUM SURFACE FORCE (CSF) APPROACH

Physical Interface



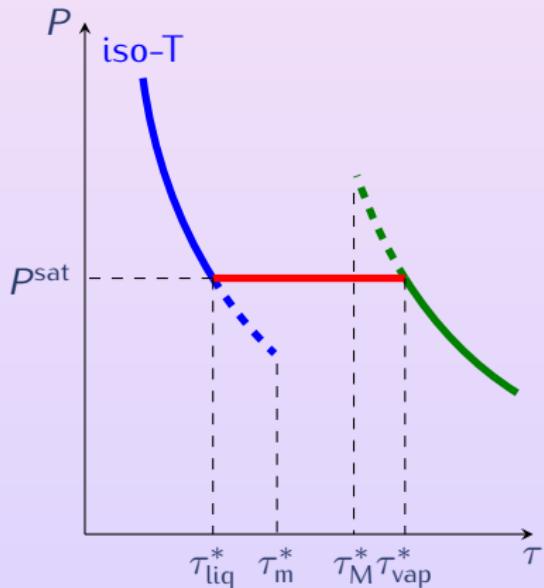
Diffuse Interface



$$\Pi_{\text{tension}} = -\sigma \operatorname{div}(\mathbf{n})\mathbf{n}$$

[J.U. BRACKBILL, D.B. KOTHE, C. ZEMACH]

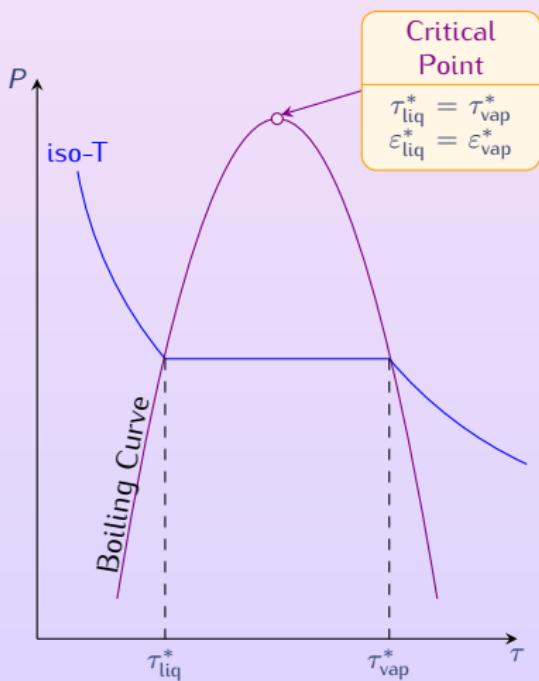
# METASTABILITY



$$P^{\text{eq}} = \begin{cases} P_{\text{liq}}, & \text{if } \tau < \tau_{\text{liq}}^*, \\ P^{\text{sat}}, & \text{if } \tau_{\text{liq}}^* < \tau < \tau_{\text{vap}}^*, \\ P_{\text{vap}}, & \text{if } \tau_{\text{vap}}^* < \tau. \end{cases}$$

$$P^{\text{met}} = \begin{cases} P_{\text{liq}}, & \text{if } \tau < \tau_{\text{liq}}^*, \\ [P^{\text{sat}} \text{ or } P_{\text{liq}}], & \text{if } \tau_{\text{liq}}^* < \tau < \tau_m^*, \\ P^{\text{sat}}, & \text{if } \tau_m^* < \tau < \tau_M^*, \\ [P^{\text{sat}} \text{ or } P_{\text{vap}}], & \text{if } \tau_M^* < \tau < \tau_{\text{vap}}^*, \\ P_{\text{vap}}, & \text{if } \tau_{\text{vap}}^* < \tau, \end{cases}$$

# CRITICAL POINT



Physic

- 2 Pure Phases EOS  $(\tau, \varepsilon) \mapsto P_\alpha$
- 1 Saturation EOS  $\tau \mapsto P^{\text{sat}}$

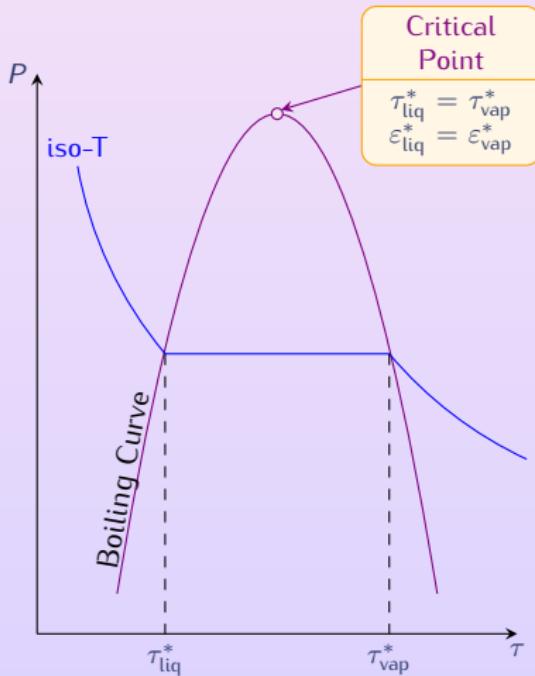
EOS

PG  $\varepsilon_{\text{liq}}^* = \varepsilon_{\text{vap}}^* \Leftrightarrow c_{V_{\text{liq}}} = c_{V_{\text{vap}}} \text{ (indip. of } T\text{)}$

SG  $\left\{ \tau_i, P_i^{\text{sat}, e} \right\}_i \rightsquigarrow (\tau, \varepsilon) \mapsto P_\alpha \rightsquigarrow \tau \mapsto P^{\text{sat}}$

$\tau_{\text{liq}}^* = \tau_{\text{vap}}^* \text{ but } \varepsilon_{\text{liq}}^* \neq \varepsilon_{\text{vap}}^*$

# CRITICAL POINT



## PHYSIC

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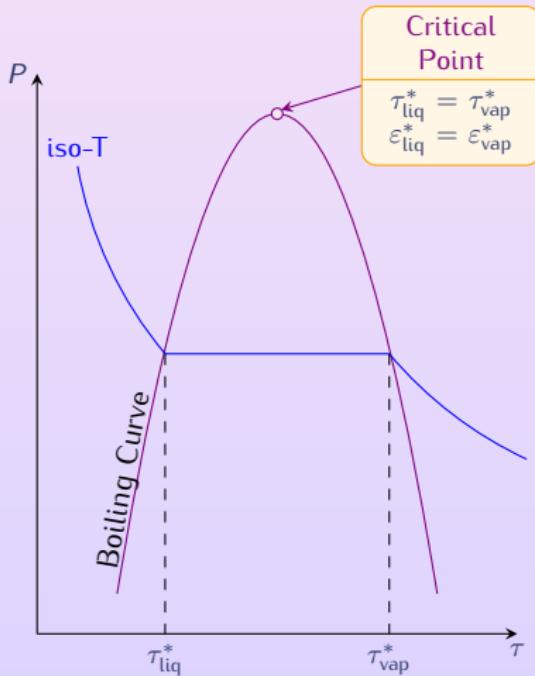
## EOS

PG  $\varepsilon_{liq}^* = \varepsilon_{vap}^* \Leftrightarrow c_{V_{liq}} = c_{V_{vap}}$  (indip. of  $T$ )

SG  $\left\{ \tau_i, P_i^{\text{sat},e} \right\}_i \rightsquigarrow (\tau, \varepsilon) \mapsto P_\alpha \rightsquigarrow \tau \mapsto P^{\text{sat}}$

$\tau_{liq}^* = \tau_{vap}^*$  but  $\varepsilon_{liq}^* \neq \varepsilon_{vap}^*$

# CRITICAL POINT



## PHYSIC

- 2 Pure Phases EOS  $(\tau, \epsilon) \mapsto P_\alpha$
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## EOS

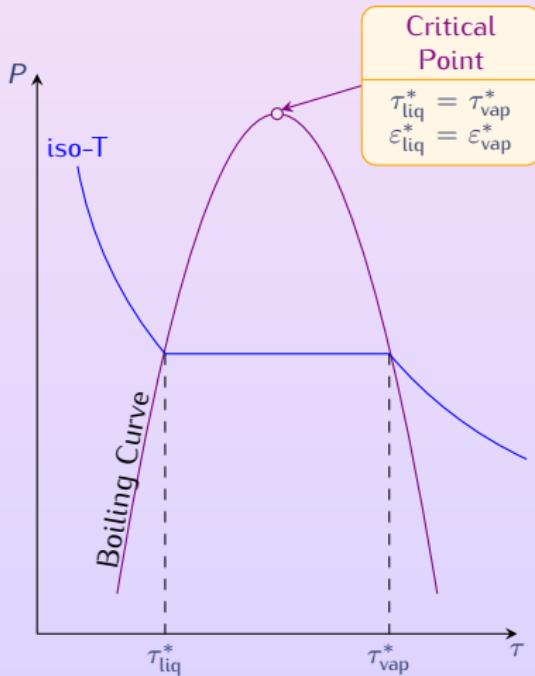
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**TAB**  $\left\{ \tau_i, P_i^{\text{sat},e} \right\}_i \rightsquigarrow \tau \mapsto P^{\text{sat}}$   
 $\{(\tau_i, \epsilon_i), (P_\alpha^e)_i\}_i \rightsquigarrow (\tau, \epsilon) \mapsto P_\alpha$

# CRITICAL POINT



## PHYSIC

- 2 Pure Phases EOS  $(\tau, \varepsilon) \mapsto P_\alpha$
- 1 Saturation EOS  $\tau \mapsto P^{\text{sat}}$

## EOS

**PG**  $\varepsilon_{\text{liq}}^* = \varepsilon_{\text{vap}}^* \Leftrightarrow c_{V_{\text{liq}}} = c_{V_{\text{vap}}} \text{ (indip. of } T\text{)}$

**SG**  $\left\{ \tau_i, P_i^{\text{sat,e}} \right\}_i \rightsquigarrow (\tau, \varepsilon) \mapsto P_\alpha \rightsquigarrow \tau \mapsto P^{\text{sat}}$

$\tau_{\text{liq}}^* = \tau_{\text{vap}}^* \text{ but } \varepsilon_{\text{liq}}^* \neq \varepsilon_{\text{vap}}^*$

**TAB**  $\left\{ \tau_i, P_i^{\text{sat,e}} \right\}_i \rightsquigarrow \tau \mapsto P^{\text{sat}}$   
 $\{(\tau_i, \varepsilon_i), (P_\alpha^e)_i\}_i \rightsquigarrow (\tau, \varepsilon) \mapsto P_\alpha$

# SUMMARY

## PHASE CHANGE EQUATION

$$\frac{\tau - \tau_{\text{vap}}^{\text{sat}}}{\tau_{\text{liq}}^{\text{sat}} - \tau_{\text{vap}}^{\text{sat}}} = \frac{\varepsilon - \varepsilon_{\text{vap}}^{\text{sat}}}{\varepsilon_{\text{liq}}^{\text{sat}} - \varepsilon_{\text{vap}}^{\text{sat}}}$$

with

$$T \mapsto \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(T) = \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}(T, P^{\text{sat}}(T))$$

or

$$P \mapsto \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(P) = \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}(T^{\text{sat}}(P), P)$$

# SUMMARY

## How to compute saturation functions $\tau_\alpha^{\text{sat}}$ and $\varepsilon_\alpha^{\text{sat}}$

- **Analytical EOS:** we compute the saturation functions  $\tau_\alpha^{\text{sat}}$  and  $\varepsilon_\alpha^{\text{sat}}$  by the **Coexistence Curve**:

- Exact:  $T \mapsto P^{\text{sat}}(T)$  or  $P \mapsto T^{\text{sat}}(P)$

$$\begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha^{\text{sat}}(P) = \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha(T^{\text{sat}}(P), P) \quad \text{e.g. Simplified Stiffened Gases}$$

- Approximated:  $T \mapsto \hat{P}^{\text{sat}}(T) \approx P^{\text{sat}}(T)$

$$\begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha^{\text{sat}}(T) \approx \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha(T, \hat{P}^{\text{sat}}(T)) \quad \text{e.g. General Stiffened Gases}$$

- **Tabulated EOS:** the saturation functions  $\tau_\alpha^{\text{sat}}$  and  $\varepsilon_\alpha^{\text{sat}}$  are given by experiments and we set

$$\begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha^{\text{sat}}(T \text{ or } P) \approx \begin{pmatrix} \hat{\tau} \\ \hat{\varepsilon} \end{pmatrix}_\alpha^{\text{sat}}(T \text{ or } P)$$

# To Do

	EOS	Pure Phases	Equilibrium	Cavitation	Boiling	Simulation
	✓	✓	✓	✓	✓	①
Virtual Fluid (SG)	✓	✓	✓	✓	✓	②
Real Fluid (SG)	✓	✓	✓	✓	✓	③
Tabulated	④	✓	⑤	⑥	⑦	