

October 28-29, 2010

MODELLING AND SIMULATION OF NUCLEATE BOILING

A CONTRIBUTION TO THE STUDY OF THE BOILING CRISIS

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OUTLINE

1 Context

2 Model

3 Numerical Approximation and Example

4 Conclusion

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2 Model

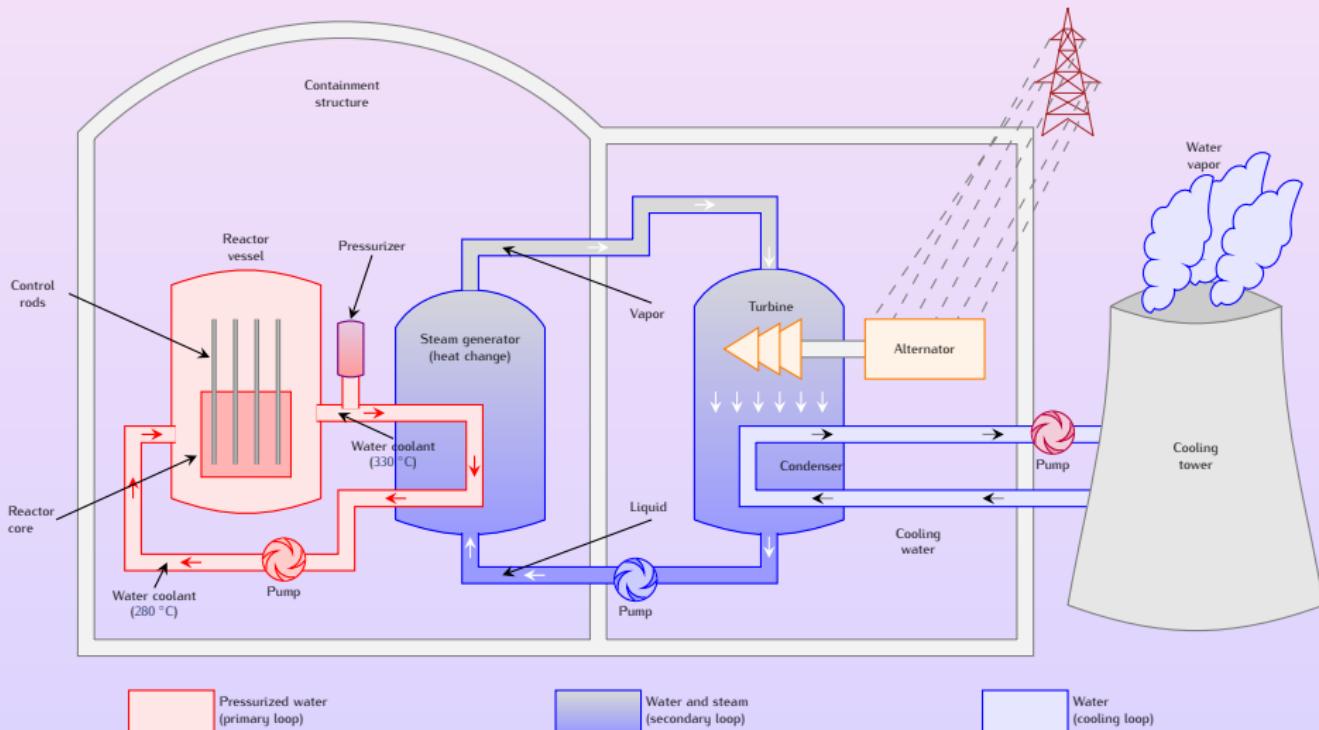
- Equation of State
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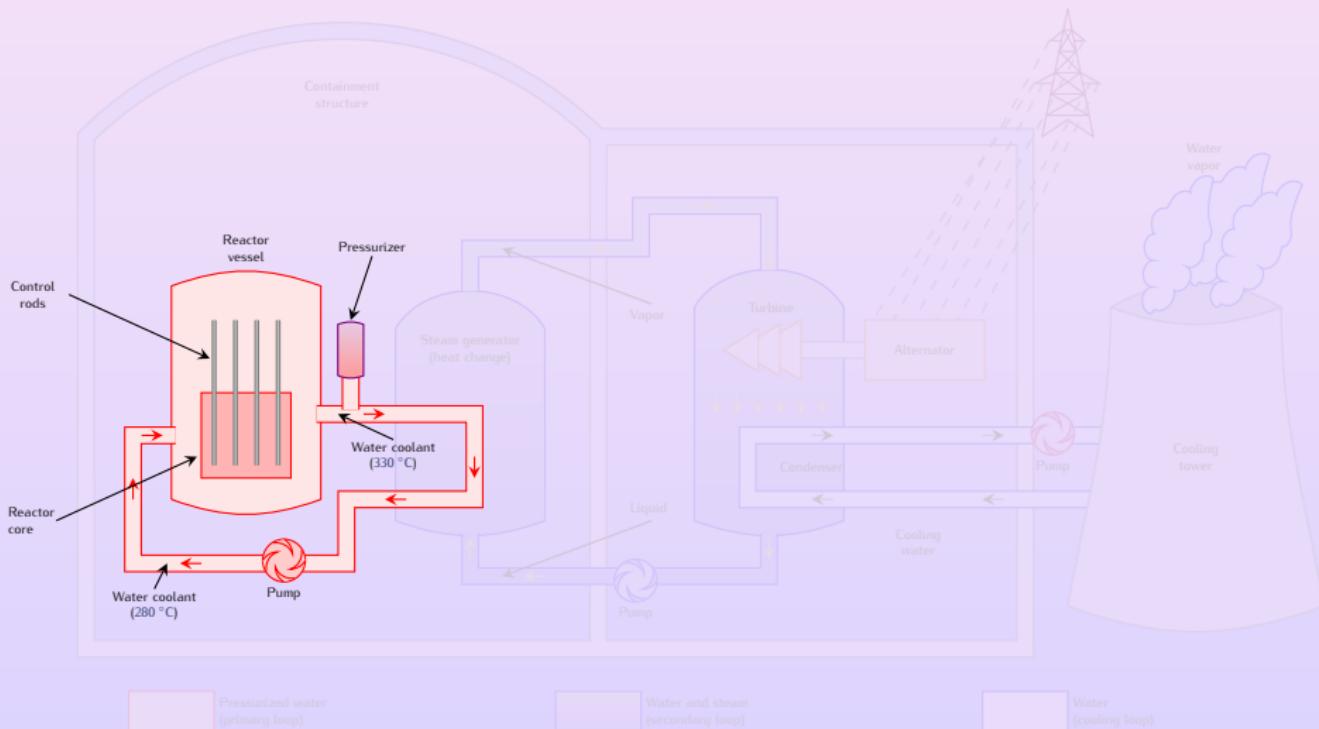
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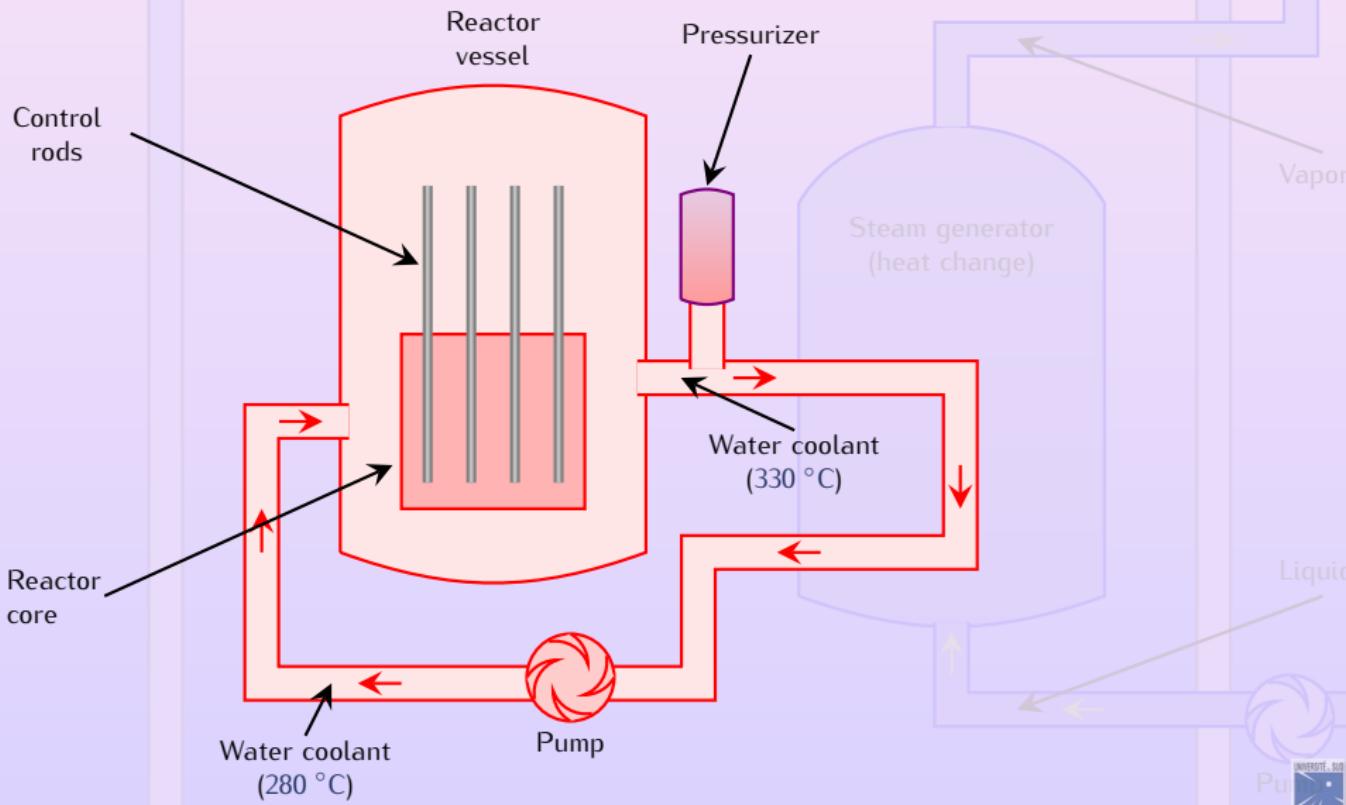
PRESSURIZED WATER REACTOR



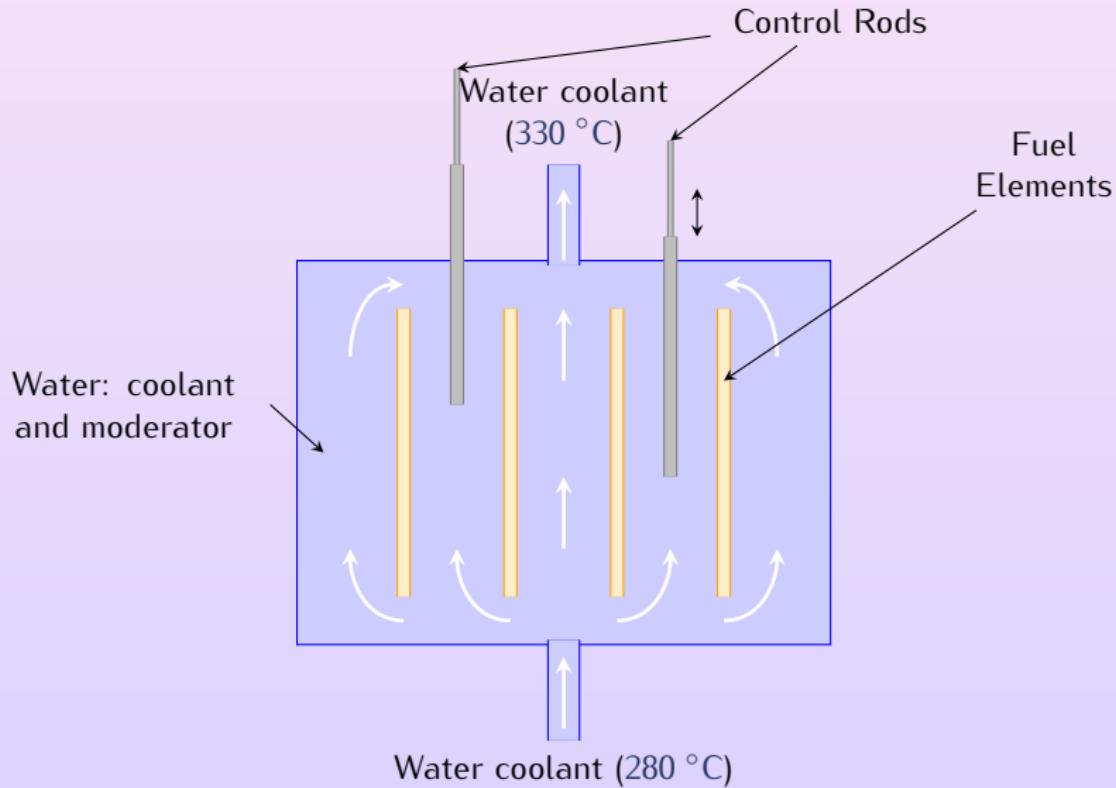
PRESSURIZED WATER REACTOR



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CORE OF A PRESSURIZED WATER REACTOR

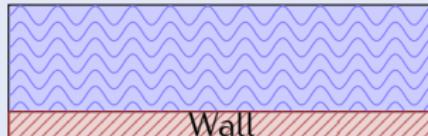


BOILING CRISIS

PHENOMENON

Liquid phase heated by a wall at a fixed temperature T^{wall} .

When T^{wall} increases, we switch from a **Nucleate Boiling** to a **Film Boiling**.

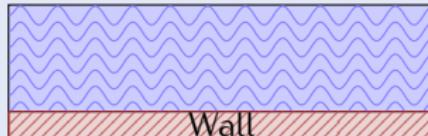


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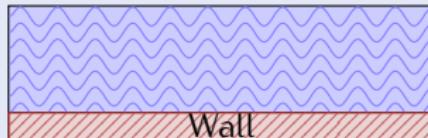
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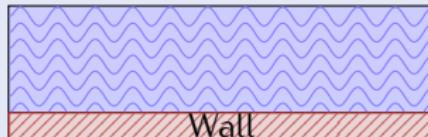
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OMEGA - CEA GRENOBLE



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“INGREDIENTS” OF THE MODEL

✓ Simulating all bubbles (DNS),

- System of PDEs for the fluid flow (monophasic or diphasic),
- Phase transition (pressure and/or temperature variations),
- Heat Diffusion,
- Surface Tension,
- Gravity.



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EULER SYSTEM

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0, \\ \partial_t (\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = \mathfrak{V}_{\text{vf}} - \mathfrak{S}_{\text{sf}}, \\ \partial_t \left(\varrho \left(\frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \right) + \operatorname{div} \left(\varrho \left(\frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \mathbf{u} + P \mathbf{u} \right) = (\mathfrak{V}_{\text{vf}} - \mathfrak{S}_{\text{sf}}) \cdot \mathbf{u} - \operatorname{div}(q). \end{cases}$$

- $(\mathbf{x}, t) \mapsto \varrho$ specific density,
- $(\mathbf{x}, t) \mapsto \varepsilon$ specific internal energy,
- $(\mathbf{x}, t) \mapsto \mathbf{u}$ velocity;
- $(\varrho, \varepsilon) \mapsto \mathfrak{V}_{\text{vf}}$ body forces,
- $(\varrho, \varepsilon) \mapsto \mathfrak{S}_{\text{sf}}$ surface forces,
- $(\varrho, \varepsilon) \mapsto \operatorname{div}(q)$ heat transfer.

$(\varrho, \varepsilon) \mapsto P$ pressure law.

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EOS OF EACH PHASE $\alpha = \text{liq}, \text{vap}$

$$\left. \begin{array}{l} \tau_\alpha \text{ specific volume} \\ \varepsilon_\alpha \text{ specific internal energy} \end{array} \right\} \Rightarrow \mathbf{w}_\alpha \stackrel{\text{def}}{=} (\tau_\alpha, \varepsilon_\alpha);$$

$\mathbf{w}_\alpha \mapsto s_\alpha$ specific entropy (Hessian matrix neg. def.);



$$\left\{ \begin{array}{ll} T_\alpha & \stackrel{\text{def}}{=} \left(\frac{\partial s_\alpha}{\partial \varepsilon_\alpha} \Big|_{\tau_\alpha} \right)^{-1} > 0 & \text{temperature,} \\ P_\alpha & \stackrel{\text{def}}{=} T_\alpha \left. \frac{\partial s_\alpha}{\partial \tau_\alpha} \right|_{\varepsilon_\alpha} > 0 & \text{pressure,} \\ g_\alpha & \stackrel{\text{def}}{=} \varepsilon_\alpha + P_\alpha \tau_\alpha - T_\alpha s_\alpha & \text{free enthalpy (Gibbs potential).} \end{array} \right.$$

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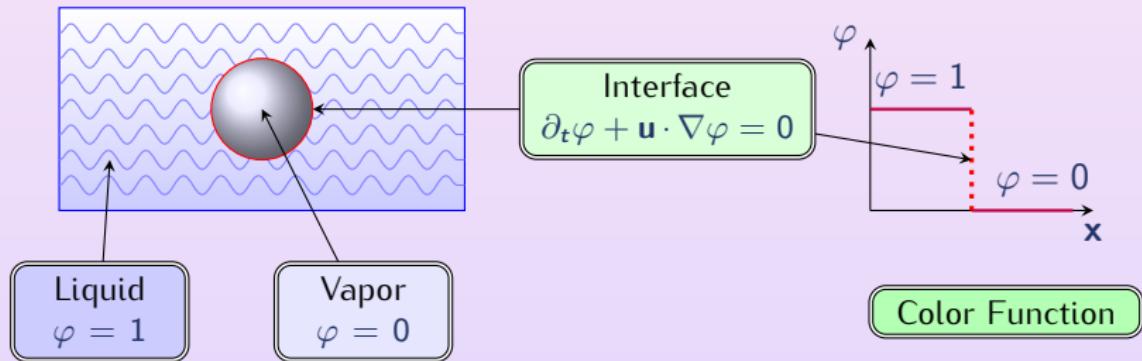
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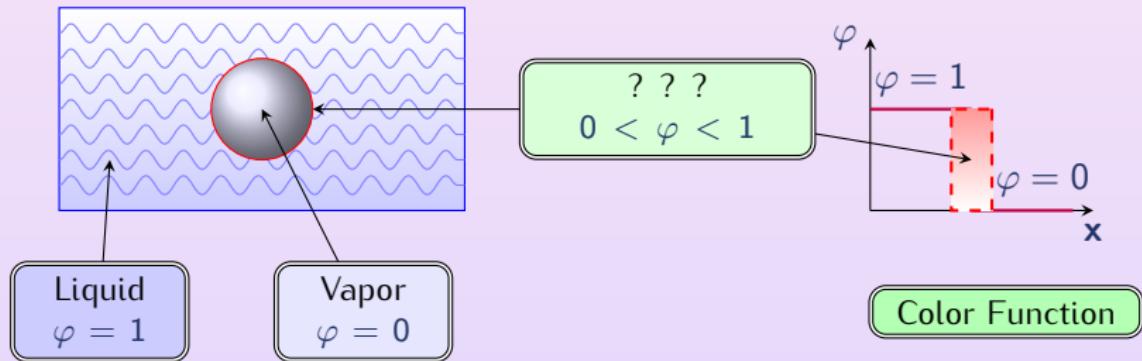


LIQUID-VAPOR INTERFACE



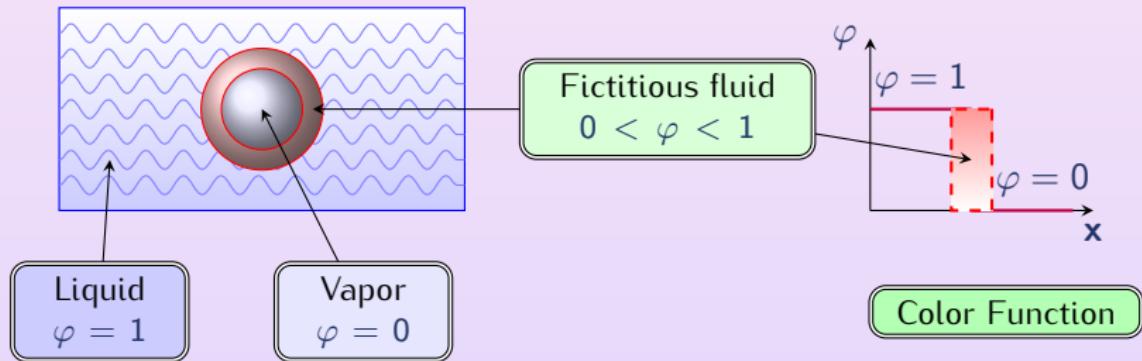
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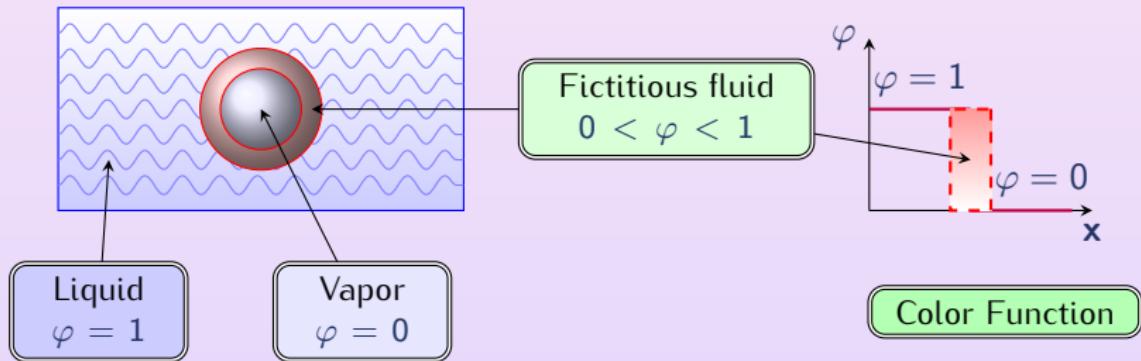
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LIQUID-VAPOR INTERFACE



➡ Goal: define a global pressure law such that

- $(\varrho, \varepsilon, \mathbf{u}, P)$ are continuous (3 zones)
- the interface position and the phase change are implicit (i.e. ~~fixed~~)
- coherence with classical thermodynamics [H. CALLEN]

EOS OF A MIXTURE

- $\mathbf{w} \stackrel{\text{def}}{=} y\mathbf{w}_{\text{liq}} + (1 - y)\mathbf{w}_{\text{vap}}$;
- y mass fraction;
- z volume fraction s.t. $y\tau_{\text{liq}} = z\tau$;
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ENTROPY WITHOUT PHASE CHANGE

$$\sigma \stackrel{\text{def}}{=} y s_{\text{liq}}(\mathbf{w}_{\text{liq}}) + (1 - y)s_{\text{vap}}(\mathbf{w}_{\text{vap}}) = y s_{\text{liq}}\left(\frac{z}{y}\tau, \frac{\psi}{y}\varepsilon\right) + (1 - y)s_{\text{vap}}\left(\frac{1-z}{1-y}\tau, \frac{1-\psi}{1-y}\varepsilon\right)$$

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EOS OF PHASE CHANGE

ENTROPY AT EQUILIBRIUM

$$\mathbf{w} \mapsto s^{\text{eq}}(\mathbf{w}) = \sigma(\mathbf{w}, z^{\text{eq}}(\mathbf{w}), y^{\text{eq}}(\mathbf{w}), \psi^{\text{eq}}(\mathbf{w}))$$

DEFINITION [H. CALLEN, PH. HELLUY ...]

Optimization Problem:

$$s^{\text{eq}}(\mathbf{w}) \stackrel{\text{def}}{=} \max_{z, y, \psi \in [0,1]^3} \sigma(\mathbf{w}, z, y, \psi)$$

Optimality Condition: $\begin{cases} T_1(z, y, \psi) = T_2(z, y, \psi) \\ P_1(z, y, \psi) = P_2(z, y, \psi) \\ g_1(z, y, \psi) = g_2(z, y, \psi) \end{cases}$

Solution: (z^*, y^*, ψ^*)



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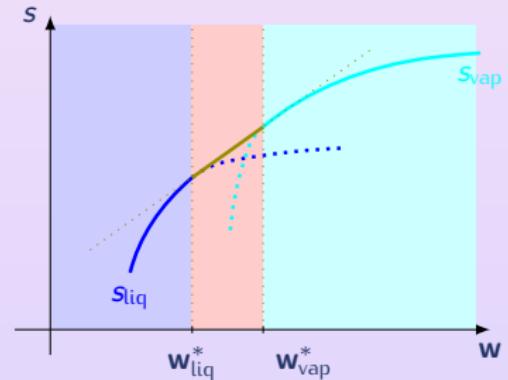
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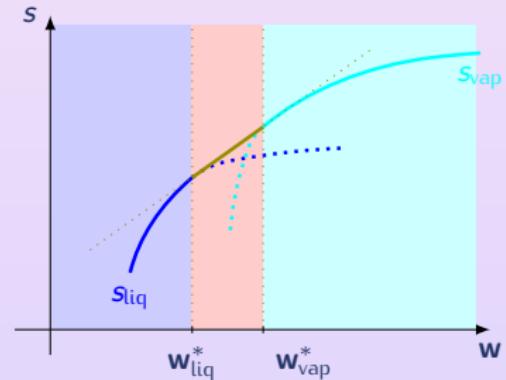
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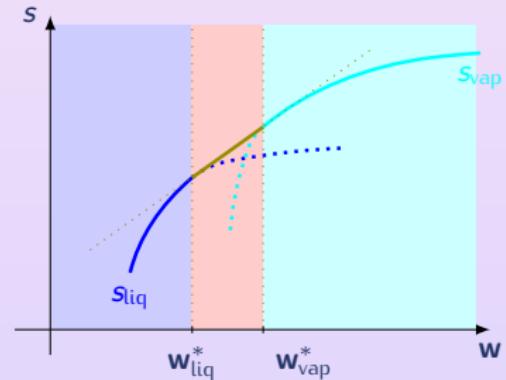
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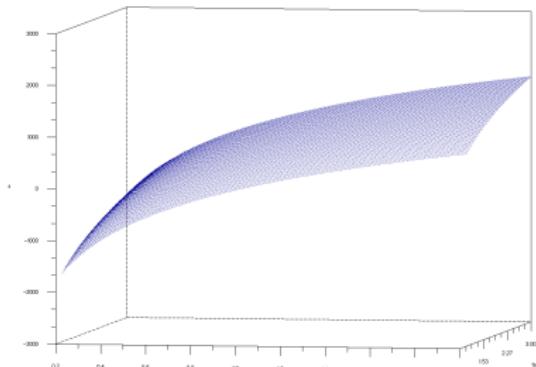


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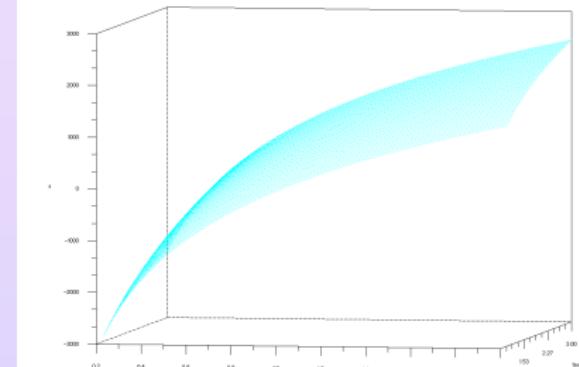
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CONCAVE HULL WITH TWO PERFECT GASES

$$(\tau, \varepsilon) \mapsto s_{\text{liq}}$$

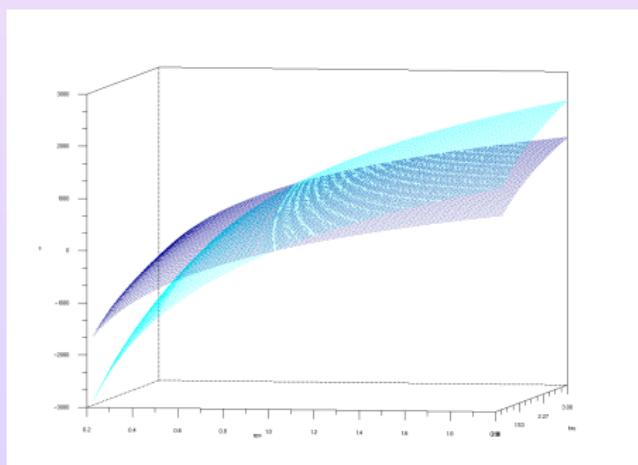


$$(\tau, \varepsilon) \mapsto s_{\text{vap}}$$



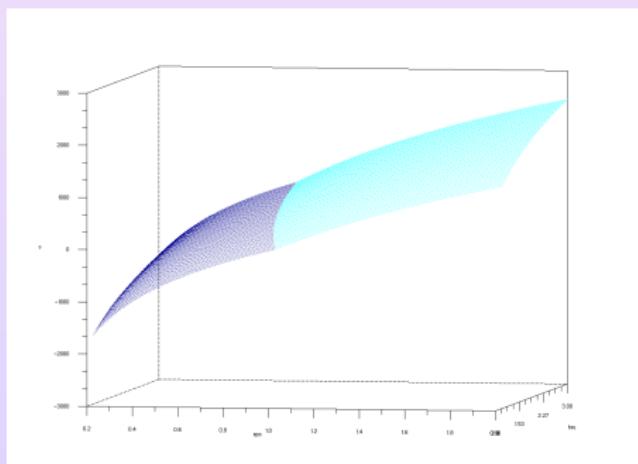
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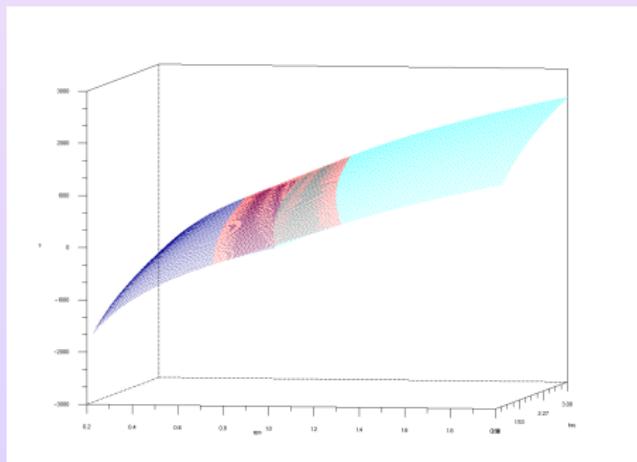
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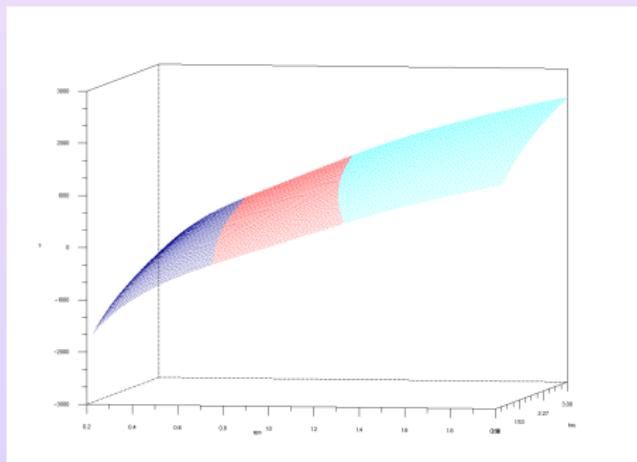
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FROM $\mathbf{w} \mapsto s^{\text{eq}}$ TO $\mathbf{w} \mapsto P^{\text{eq}}$

For all $\tilde{\mathbf{w}}$ fixed, we seek $(\mathbf{w}_{\text{liq}}^*, \mathbf{w}_{\text{vap}}^*, y^*)$ as the solution of the system

$$\begin{cases} P_{\text{liq}}(\mathbf{w}_{\text{liq}}) = P_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ T_{\text{liq}}(\mathbf{w}_{\text{liq}}) = T_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ g_{\text{liq}}(\mathbf{w}_{\text{liq}}) = g_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ \tilde{\mathbf{w}} = y\mathbf{w}_{\text{liq}} + (1 - y)\mathbf{w}_{\text{vap}} \end{cases}$$

- if $y^* \in]0, 1[$ then $\tilde{\mathbf{w}}$ is an equilibrium mixture state

$$s^{\text{eq}}(\tilde{\mathbf{w}}) = y^* s_{\text{liq}}(\mathbf{w}_{\text{liq}}^*) + (1 - y^*) s_{\text{vap}}(\mathbf{w}_{\text{vap}}^*),$$

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$$s^{\text{eq}}(\tilde{\mathbf{w}}) = \max\{s_{\text{liq}}(\tilde{\mathbf{w}}), s_{\text{vap}}(\tilde{\mathbf{w}})\},$$

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FROM $\mathbf{w} \mapsto s^{\text{eq}}$ TO $\mathbf{w} \mapsto P^{\text{eq}}$

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- ① if $y^* \in]0, 1[$ then $\tilde{\mathbf{w}}$ is an **equilibrium mixture state**

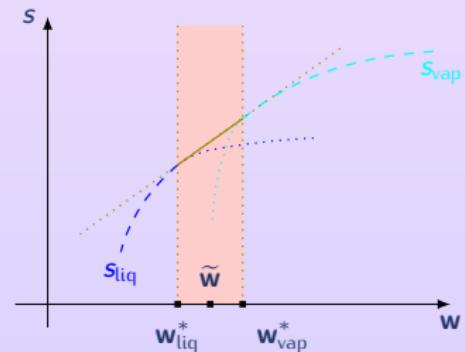
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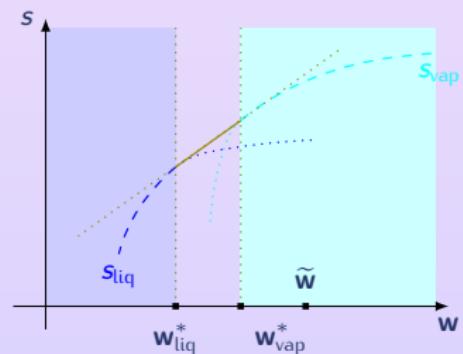
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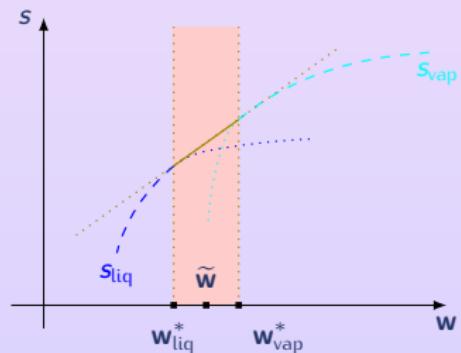
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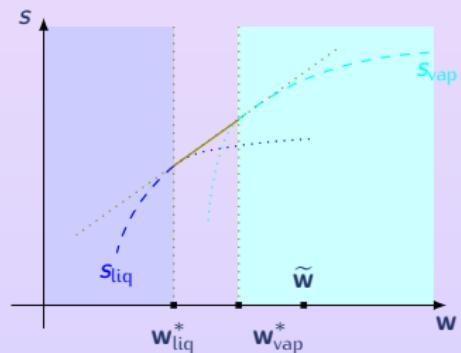
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OUTLINE

1 Context

2 Model

- Equation of State
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3 Numerical Approximation and Example

- The Phase Change Equation
- Numerical Scheme and Example

4 Conclusion

DYNAMIC LIQUID-VAPOR PHASE CHANGE

EULER SYSTEM

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0, \\ \partial_t (\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t \left(\varrho \left(\frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \right) + \operatorname{div} \left(\varrho \left(\frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \mathbf{u} + P^{\text{eq}} \mathbf{u} \right) = 0 \end{cases} \quad \text{with } P^{\text{eq}} \stackrel{\text{def}}{=} \frac{s_{\tau}^{\text{eq}}}{s_{\varepsilon}^{\text{eq}}}.$$

MATHEMATICAL PROPERTIES

If $\tau_1^* \neq \tau_2^*$ and $\varepsilon_1^* \neq \varepsilon_2^*$ (first order phase transition) then

- Euler system with hyperbolic (or -system)
- Riemann problem: multitude of entropy (lax) solutions in vacuum
- Small differences in (τ, ε)



DYNAMIC LIQUID-VAPOR PHASE CHANGE

EULER SYSTEM

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0, \\ \partial_t (\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t \left(\varrho \left(\frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \right) + \operatorname{div} \left(\varrho \left(\frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \mathbf{u} + P^{\text{eq}} \mathbf{u} \right) = 0 \end{cases} \quad \text{with } P^{\text{eq}} \stackrel{\text{def}}{=} \frac{s_{\tau}^{\text{eq}}}{s_{\varepsilon}^{\text{eq}}}.$$

MATHEMATICAL PROPERTIES

If $\tau_1^* \neq \tau_2^*$ and $\varepsilon_1^* \neq \varepsilon_2^*$ (first order phase transition) then

$$\textcircled{1} \ c(\mathbf{w}) > 0, \quad \textcircled{2} \ s_{\tau \varepsilon}^{\text{eq}}(\mathbf{w}) > 0$$

① Euler system: strict hyperbolicity ($\neq p$ -system).

② Riemann problem: multitude of entropy (Lax) solutions [R. MENIKOFF, B. J. PLOHR], uniqueness of Liu solution.

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SUMMARY OF THE MODEL

Euler System

$$\mathbf{w} \mapsto P^{\text{eq}}$$

$$\mathbf{w} \mapsto S^{\text{eq}}$$

$$\begin{cases} g_1(w_1) = g_2(w_2) \\ P_1(w_1) = P_2(w_2) \\ T_1(w_1) = T_2(w_2) \\ w = yw_1 + (1-y)w_2 \end{cases}$$

Phase Change Equation

$$\frac{\tau - \tau_{\text{vap}}^{\text{sat}}}{\tau_{\text{liq}}^{\text{sat}} - \tau_{\text{vap}}^{\text{sat}}} = \frac{\varepsilon - \varepsilon_{\text{vap}}^{\text{sat}}}{\varepsilon_{\text{liq}}^{\text{sat}} - \varepsilon_{\text{vap}}^{\text{sat}}}$$



SUMMARY OF THE MODEL

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Euler System

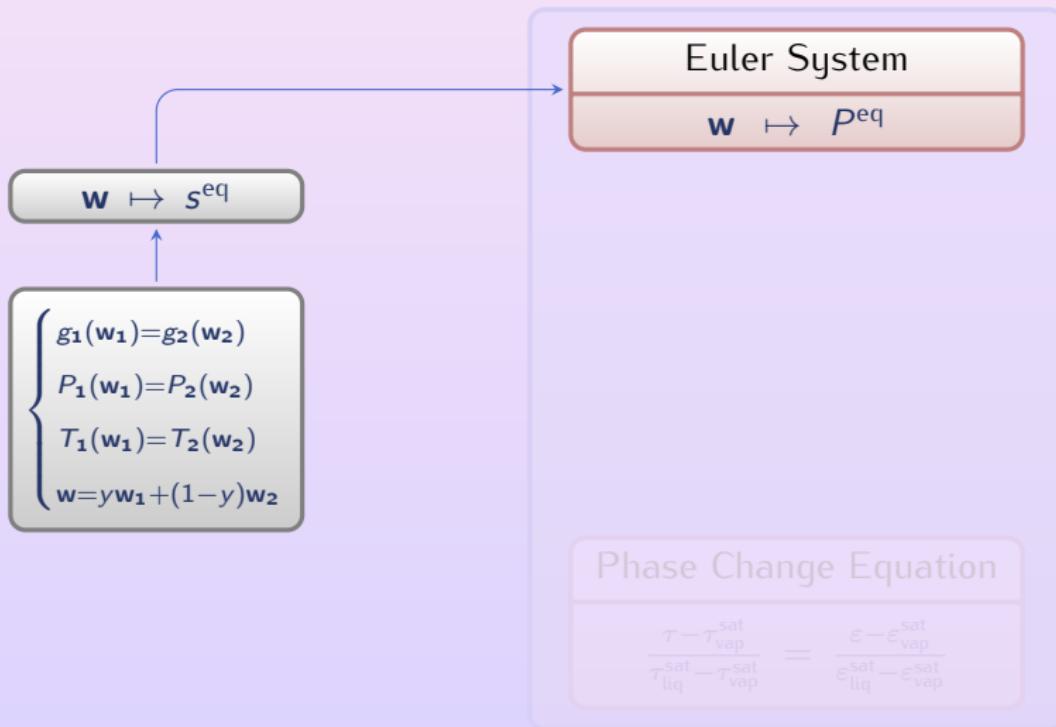
$$\mathbf{w} \mapsto P^{\text{eq}}$$

Phase Change Equation

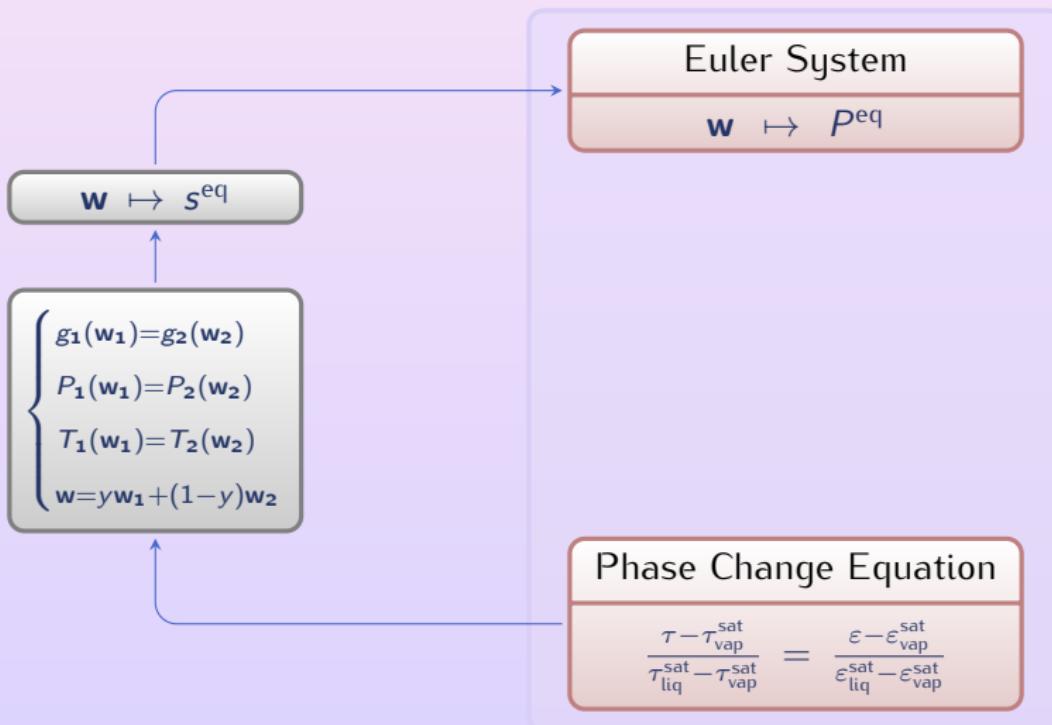
$$\frac{T - T_{\text{vap}}^{\text{sat}}}{T_{\text{liq}}^{\text{sat}} - T_{\text{vap}}^{\text{sat}}} = \frac{\varepsilon - \varepsilon_{\text{vap}}^{\text{sat}}}{\varepsilon_{\text{liq}}^{\text{sat}} - \varepsilon_{\text{vap}}^{\text{sat}}}$$



SUMMARY OF THE MODEL



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SUMMARY OF THE MODEL

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ANALYTICAL EOS

(τ, ε) fixed

$(\tau_1, \varepsilon_1, \tau_2, \varepsilon_2, y)$ SOLUTION OF

$$\begin{cases} g_1(\tau_1, \varepsilon_1) = g_2(\tau_2, \varepsilon_2) \\ P_1(\tau_1, \varepsilon_1) = P_2(\tau_2, \varepsilon_2) \\ T_1(\tau_1, \varepsilon_1) = T_2(\tau_2, \varepsilon_2) \\ \tau = y\tau_1 + (1-y)\tau_2 \\ \varepsilon = y\varepsilon_1 + (1-y)\varepsilon_2 \end{cases}$$

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$$\begin{cases} g_1(P, T) = g_2(P, T) \\ \frac{\tau - \tau_2(P, T)}{\tau_1(P, T) - \tau_2(P, T)} = \frac{\varepsilon - \varepsilon_2(P, T)}{\varepsilon_1(P, T) - \varepsilon_2(P, T)} \end{cases}$$

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$T \mapsto P = \hat{P}^{\text{sat}}(T) \approx P^{\text{sat}}(T)$

least square approximation

T SOLUTION OF

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TABULATED EOS

T (K)	P^{sat} (MPa)	Volume (m ³ /kg)		Internal Energy (kJ/kg)	
		$\tau_{\text{liq}}^{\text{sat}}$	$\tau_{\text{vap}}^{\text{sat}}$	$\varepsilon_{\text{liq}}^{\text{sat}}$	$\varepsilon_{\text{vap}}^{\text{sat}}$
275	0,00069845	0,0010001	181,60	7,7590	2377,5
278	0,00086349	0,0010001	148,48	20,388	2381,6
281	0,0010621	0,0010002	122,01	32,996	2385,7
284	0,0012999	0,0010004	100,74	45,586	2389,8
287	0,0015835	0,0010008	83,560	58,162	2393,9
290	0,0019200	0,0010012	69,625	70,727	2398,0
293	0,0023177	0,0010018	58,267	83,284	2402,1
296	0,0027856	0,0010025	48,966	95,835	2406,2
299	0,0033342	0,0010032	41,318	108,38	2410,3
302	0,0039745	0,0010041	35,002	120,92	2414,4
305	0,0047193	0,0010050	29,764	133,46	2418,4
308	0,0055825	0,0010060	25,403	146	2422,5
...

Source: <http://webbook.nist.gov/chemistry/fluid/>



TABULATED EOS

(τ, ε) fixed

T SOLUTION OF

$$\frac{\tau - \tau_2^{\text{sat}}(T)}{\tau_1^{\text{sat}}(T) - \tau_2^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_2^{\text{sat}}(T)}{\varepsilon_1^{\text{sat}}(T) - \varepsilon_2^{\text{sat}}(T)} \quad \text{with} \quad \left(\frac{\tau}{\varepsilon}\right)_\alpha^{\text{sat}}(T) \quad \text{tabulated}$$

Q

$$\frac{\tau - \hat{\tau}_2^{\text{sat}}(T)}{\hat{\tau}_1^{\text{sat}}(T) - \hat{\tau}_2^{\text{sat}}(T)} = \frac{\varepsilon - \hat{\varepsilon}_2^{\text{sat}}(T)}{\hat{\varepsilon}_1^{\text{sat}}(T) - \hat{\varepsilon}_2^{\text{sat}}(T)} \quad \text{with} \quad \left(\frac{\hat{\tau}}{\hat{\varepsilon}}\right)_\alpha^{\text{sat}}(T)$$



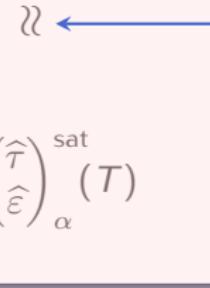
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least square
approximations

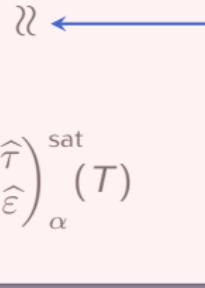
TABULATED EOS

(τ, ε) fixed

T SOLUTION OF

$$\frac{\tau - \tau_2^{\text{sat}}(T)}{\tau_1^{\text{sat}}(T) - \tau_2^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_2^{\text{sat}}(T)}{\varepsilon_1^{\text{sat}}(T) - \varepsilon_2^{\text{sat}}(T)} \quad \text{with} \quad \left(\begin{matrix} \tau \\ \varepsilon \end{matrix}\right)_\alpha^{\text{sat}}(T) \quad \text{tabulated}$$

$$\frac{\tau - \hat{\tau}_2^{\text{sat}}(T)}{\hat{\tau}_1^{\text{sat}}(T) - \hat{\tau}_2^{\text{sat}}(T)} = \frac{\varepsilon - \hat{\varepsilon}_2^{\text{sat}}(T)}{\hat{\varepsilon}_1^{\text{sat}}(T) - \hat{\varepsilon}_2^{\text{sat}}(T)} \quad \text{with} \quad \left(\begin{matrix} \hat{\tau} \\ \hat{\varepsilon} \end{matrix}\right)_\alpha^{\text{sat}}(T)$$



least square
approximations

OUTLINE

1 Context

2 Model

- Equation of State
- Conservation Laws

3 Numerical Approximation and Example

- The Phase Change Equation
- Numerical Scheme and Example

4 Conclusion

NUMERICAL SCHEME BASED ON RELAXATION APPROACH

$$\sigma(y, z, \psi, \tau, \varepsilon)$$

Optimization

$$s^{\text{eq}}(\tau, \varepsilon)$$

Off Equilibrium

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0 \\ \partial_t(\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = 0 \\ \partial_t(\varrho e) + \operatorname{div}((\varrho e + P)\mathbf{u}) = 0 \\ \partial_t z + \mathbf{u} \cdot \operatorname{grad} z = \\ \partial_t y + \mathbf{u} \cdot \operatorname{grad} y = \\ \partial_t \psi + \mathbf{u} \cdot \operatorname{grad} \psi = \end{cases}$$

$$\mu_j \rightarrow \infty$$

Equilibrium

$$\begin{cases} \partial_t \varrho + \operatorname{div}(\varrho \mathbf{u}) = 0 \\ \partial_t(\varrho \mathbf{u}) + \operatorname{div}(\varrho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t(\varrho e) + \operatorname{div}((\varrho e + P^{\text{eq}})\mathbf{u}) = 0 \\ P^{\text{eq}}(\varrho, \varepsilon) = \frac{s_{\tau}^{\text{eq}}}{s_{\varepsilon}^{\text{eq}}} \end{cases}$$

Two Steps:

- ① Hydrodynamic (+ gravity, surface tension, heat diffusion, ...)
- > Projection by solving the Phase-Change Equation

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$$P(\varrho, \varepsilon, z, y, \psi) = \frac{\sigma_\tau}{\sigma_\varepsilon}$$

$\mu_j \rightarrow \infty$

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$$P(\varrho, z, y, \psi) = \frac{\sigma_z}{\sigma_\varepsilon}$$

$$\mu_j \rightarrow \infty$$

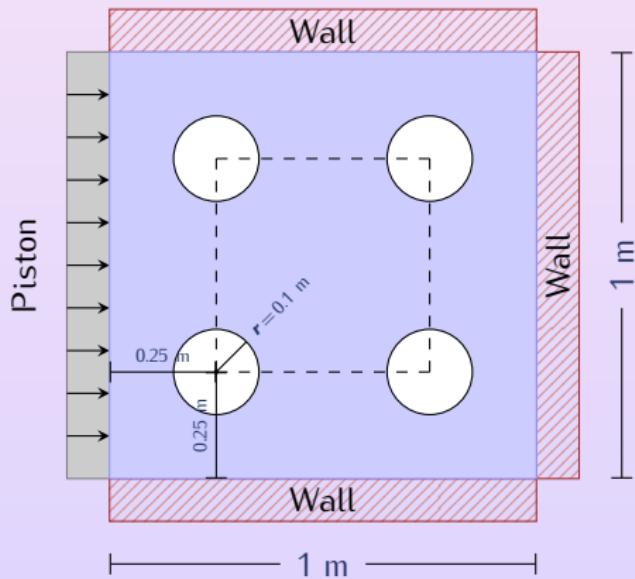
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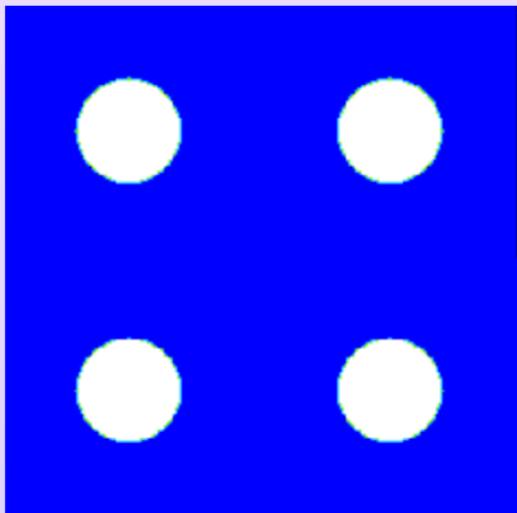
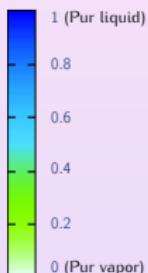
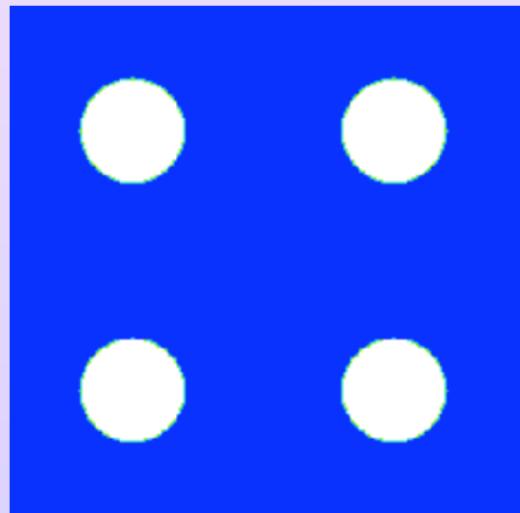
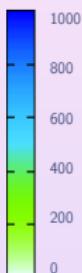
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COMPRESSION OF VAPOR BUBBLES



COMPRESSION OF VAPOR BUBBLES

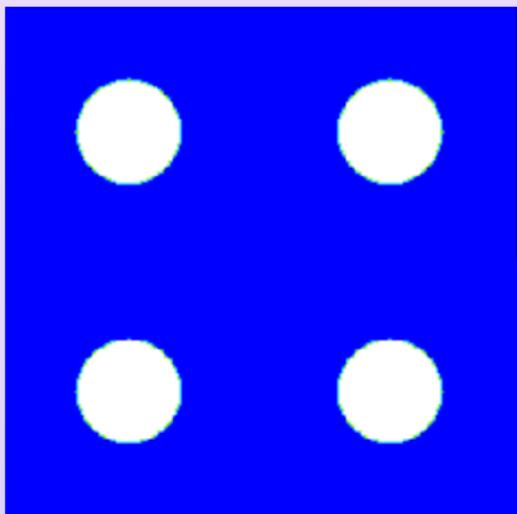
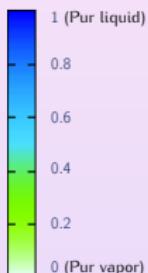
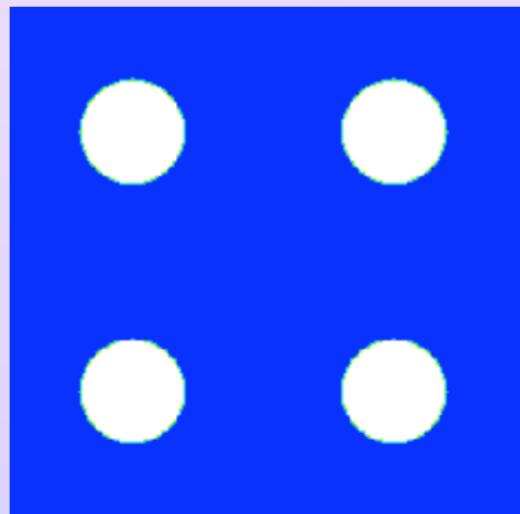
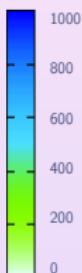
Massee fraction y Density ϱ 

◀ Geometry

▶ Play

▶ Skip

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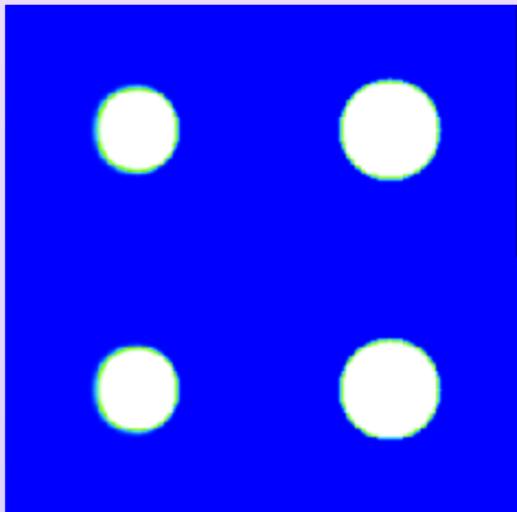
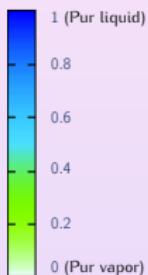
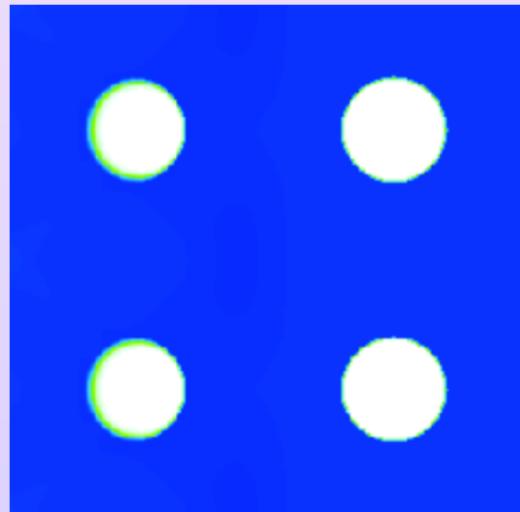
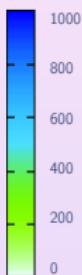
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◀ Geometry

▶ Play

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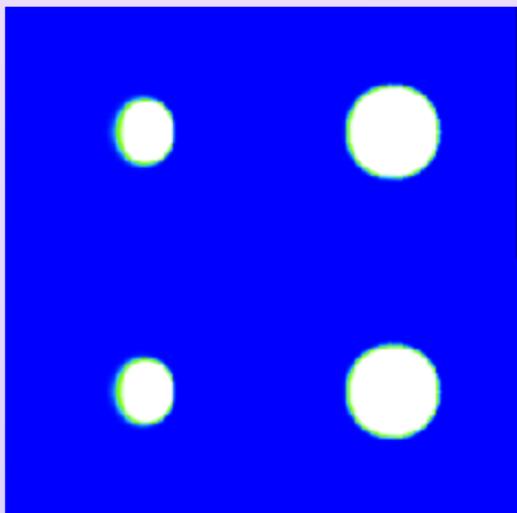
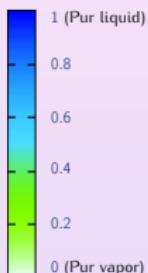
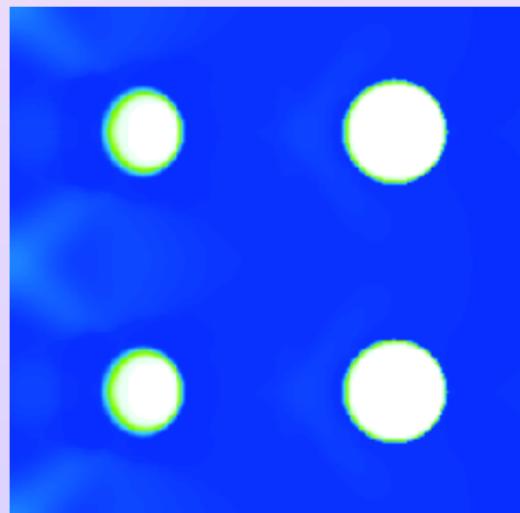
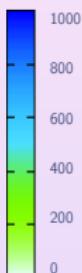
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◀ Geometry

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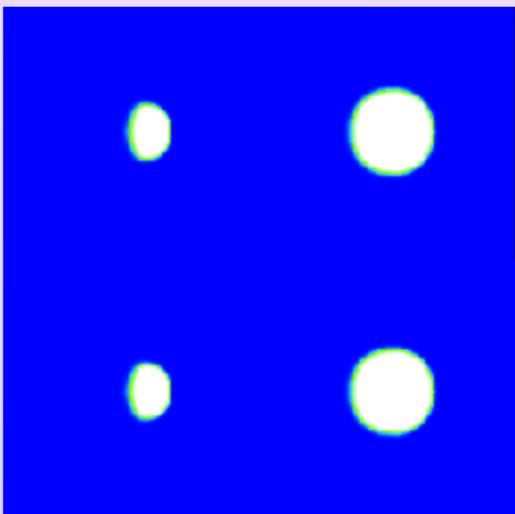
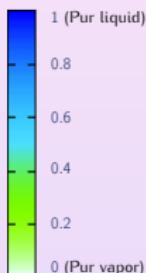
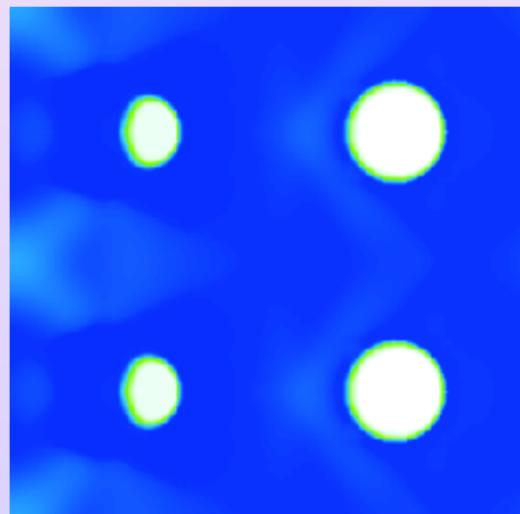
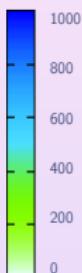
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◀ Geometry

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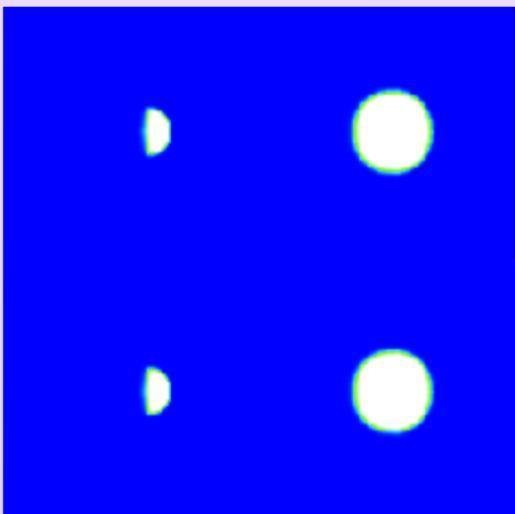
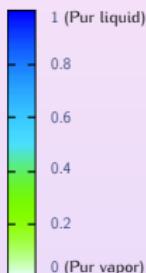
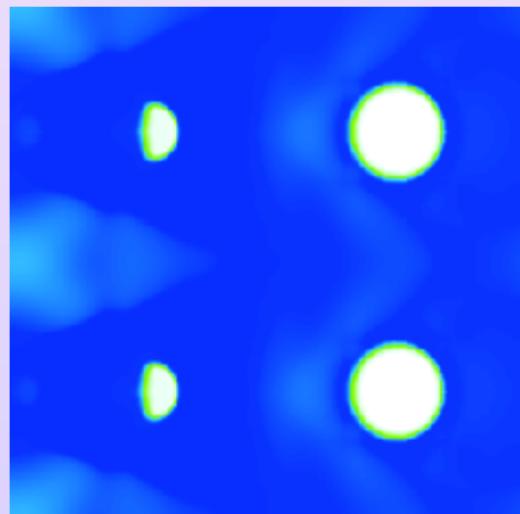
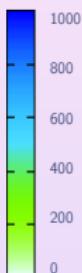
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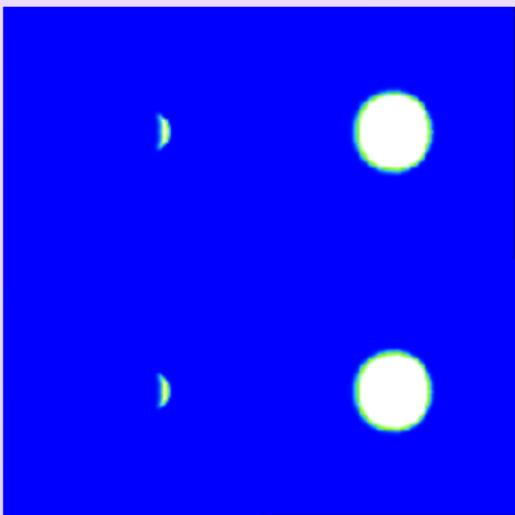
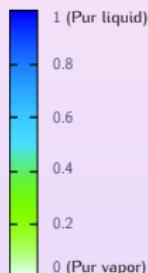
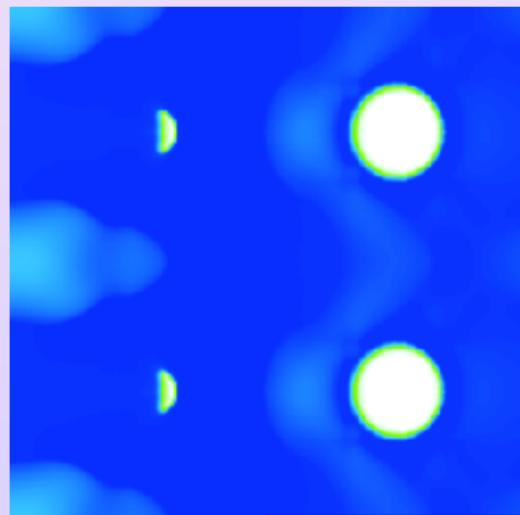
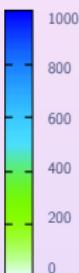
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◀ Geometry

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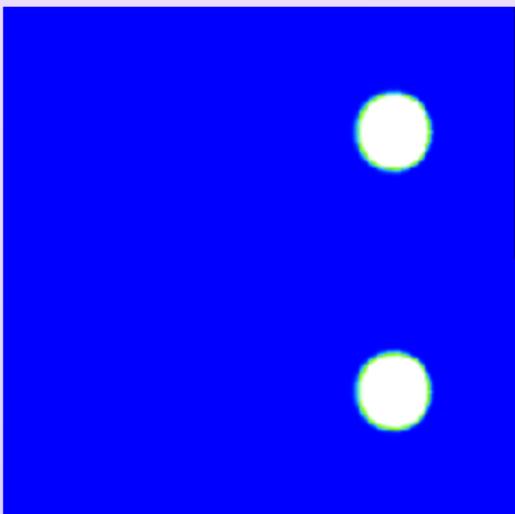
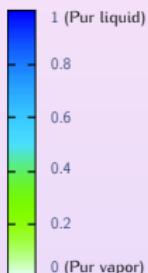
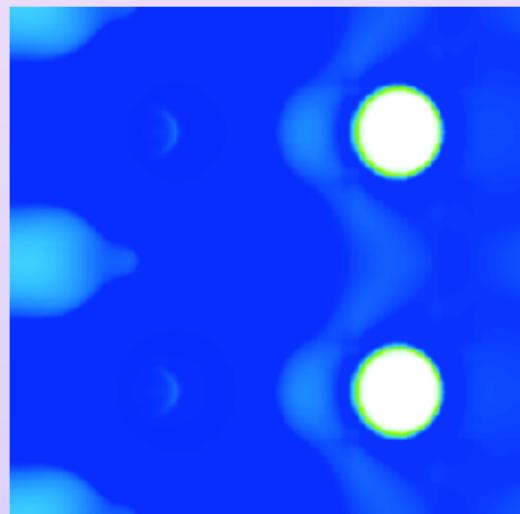
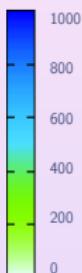
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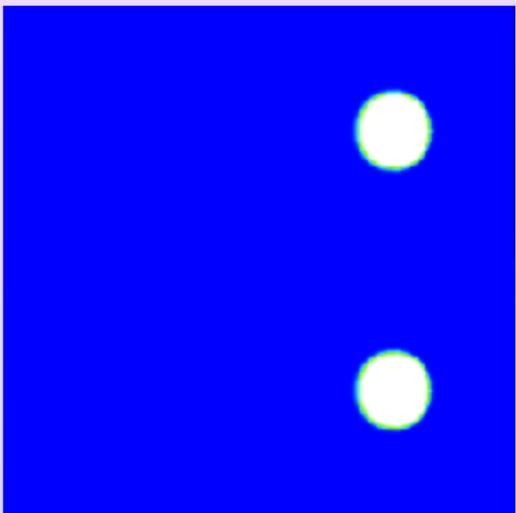
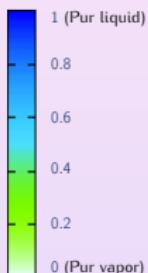
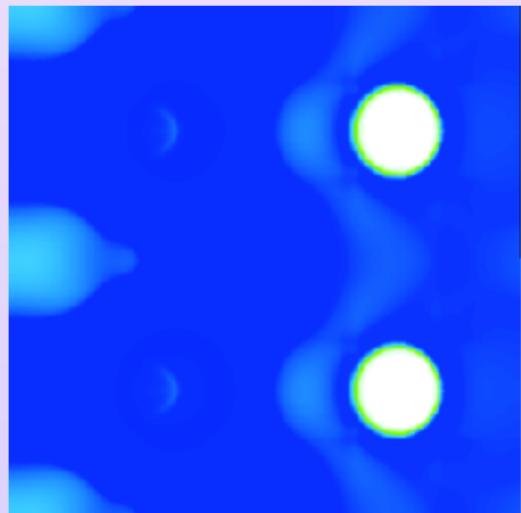
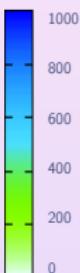
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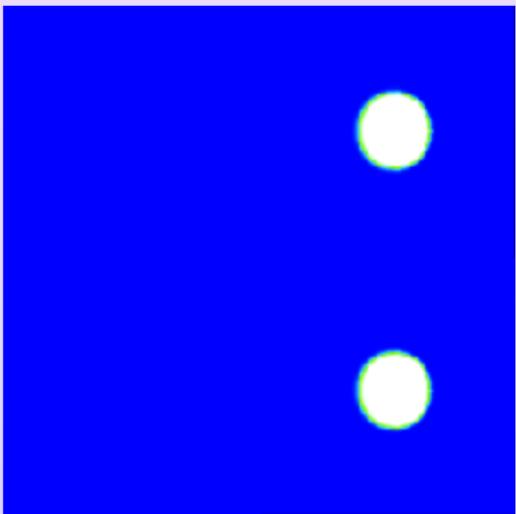
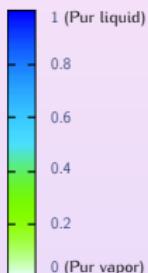
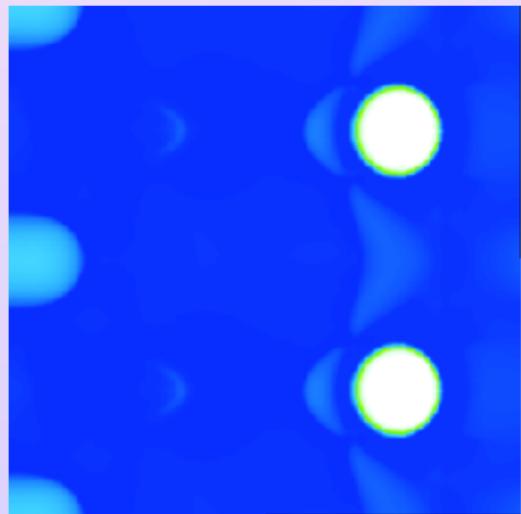
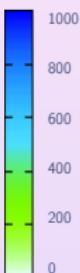
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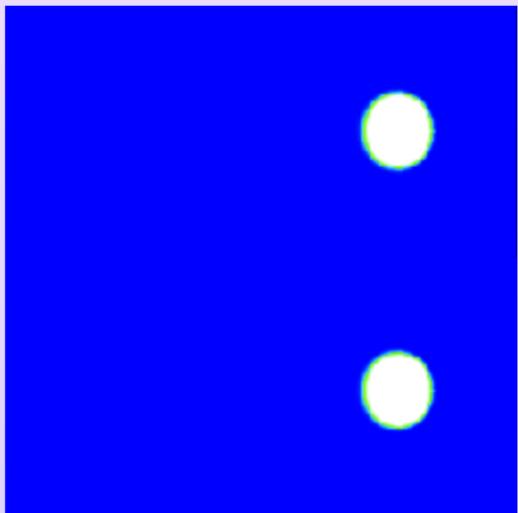
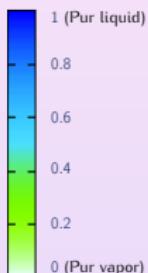
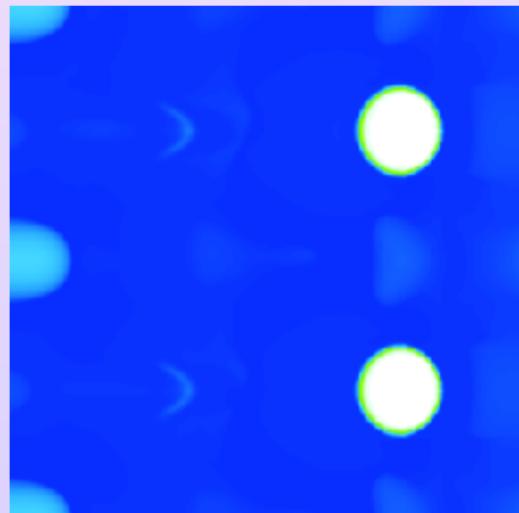
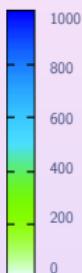
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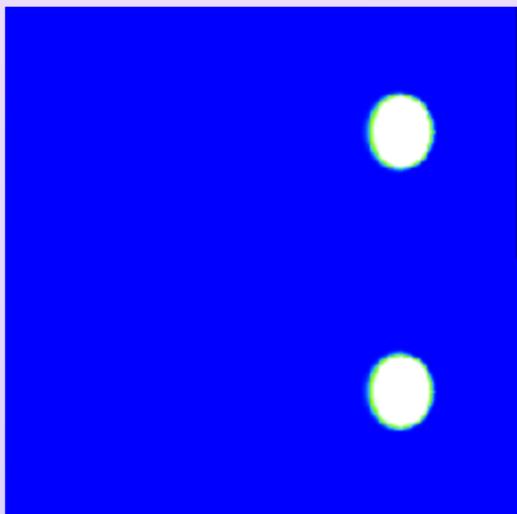
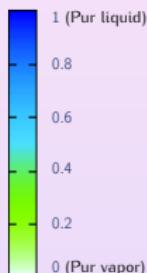
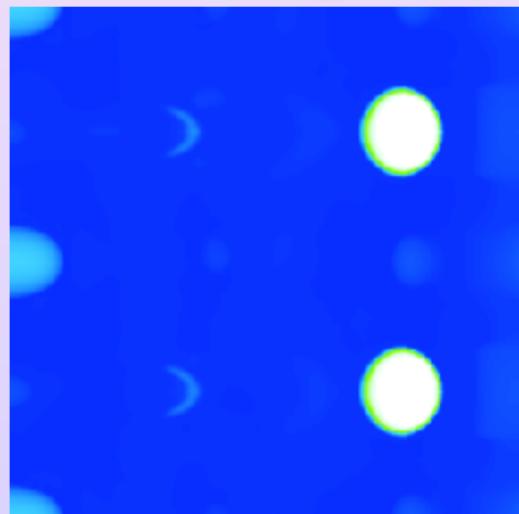
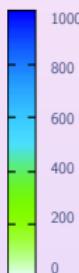
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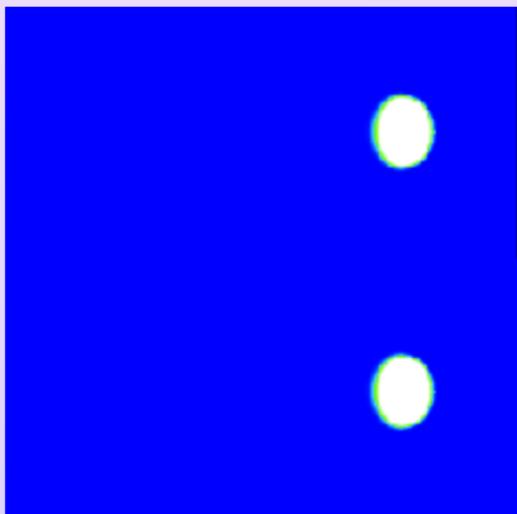
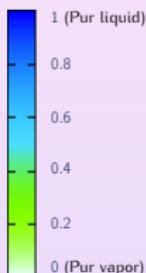
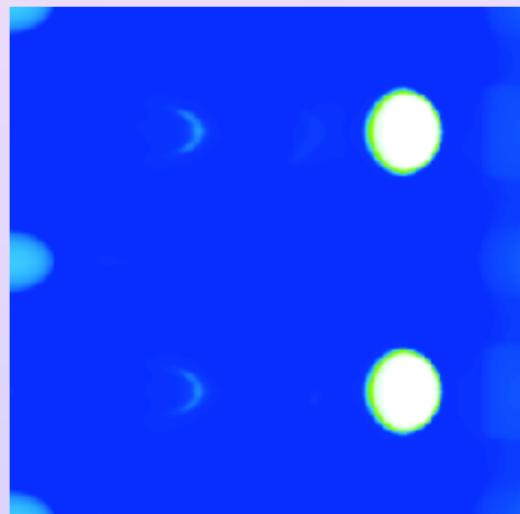
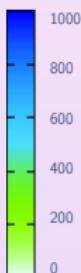
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◀ Geometry

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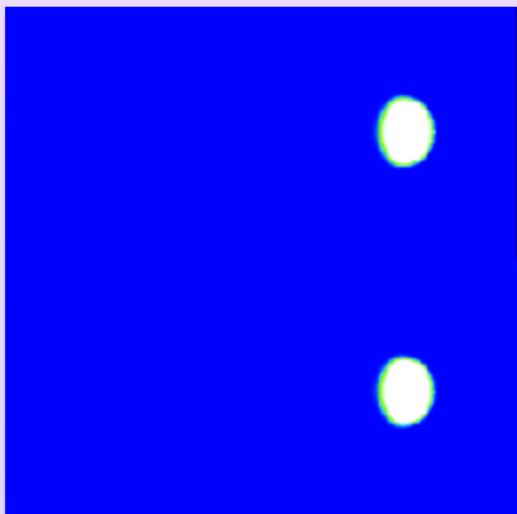
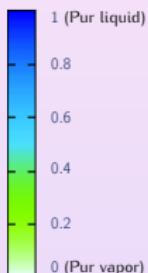
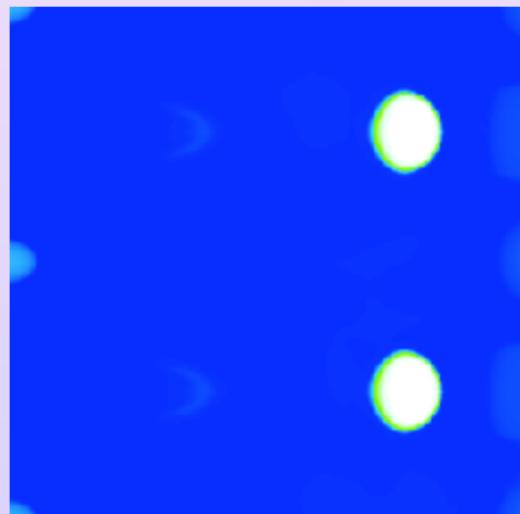
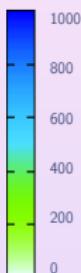
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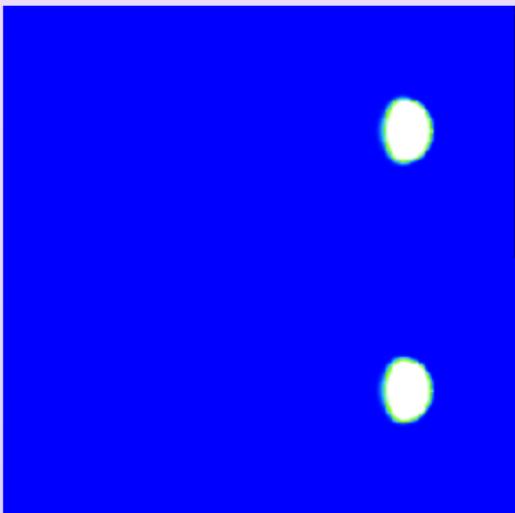
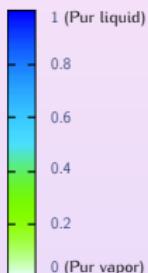
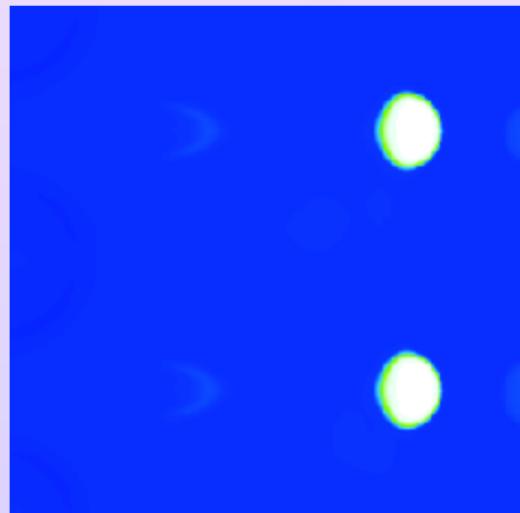
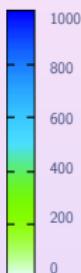
Massee fraction y Density ϱ 

◀ Geometry

▶ Play

▶ Skip

COMPRESSION OF VAPOR BUBBLES

Massee fraction y Density ϱ 

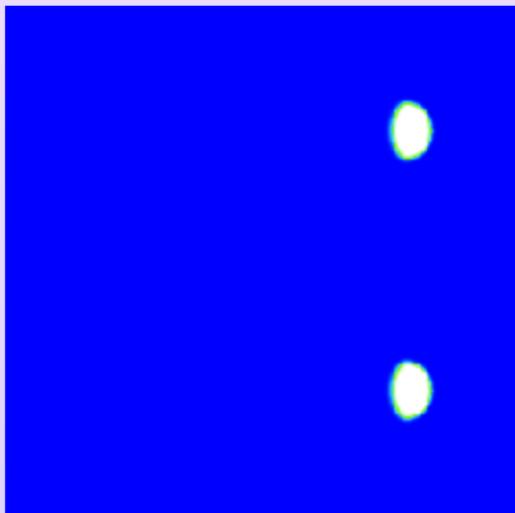
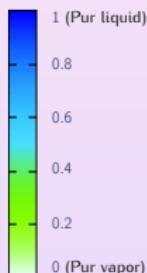
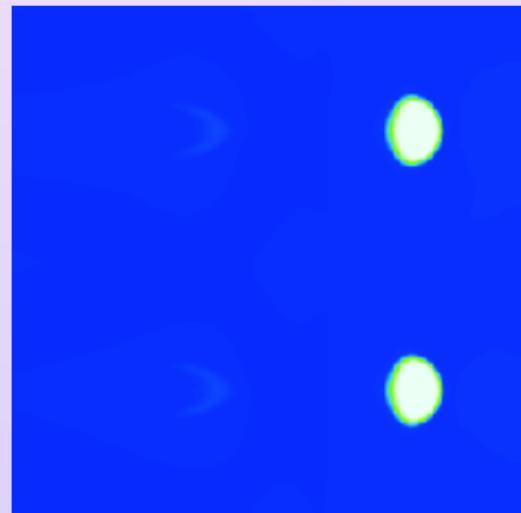
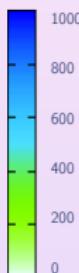
◀ Geometry

▶ Play

▶ Skip



COMPRESSION OF VAPOR BUBBLES

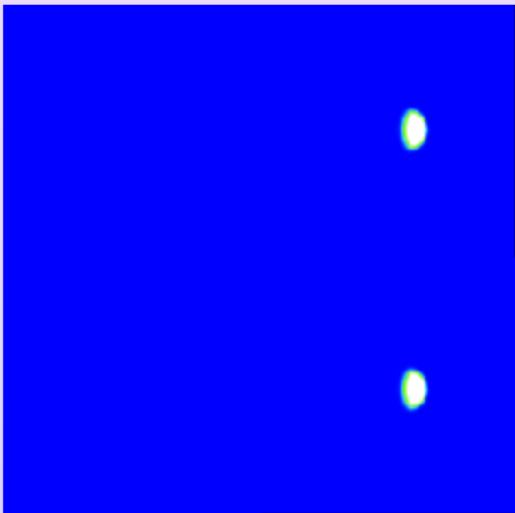
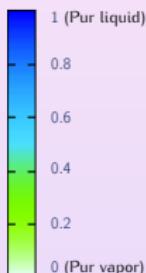
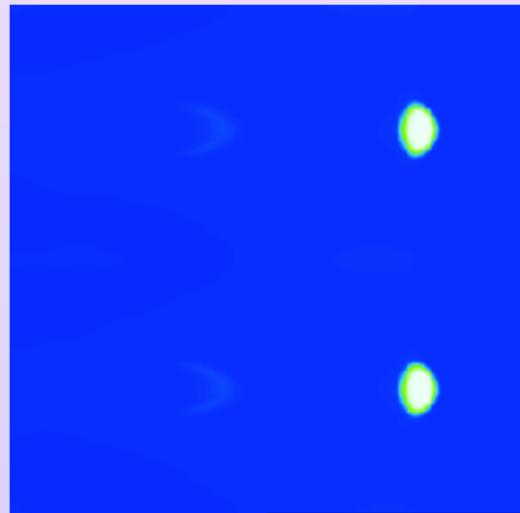
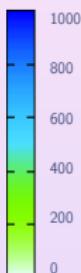
Massee fraction y Density ϱ 

◀ Geometry

▶ Play

▶ Skip

COMPRESSION OF VAPOR BUBBLES

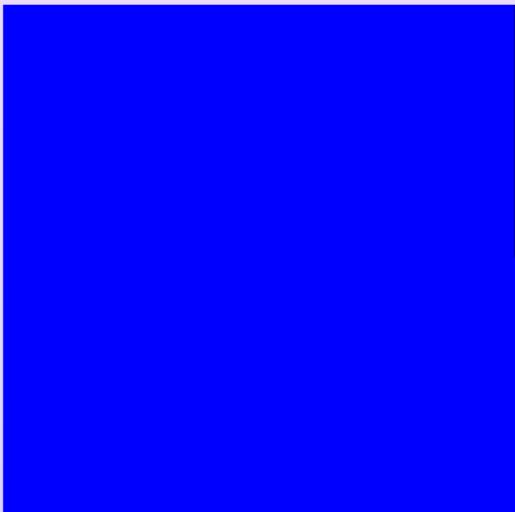
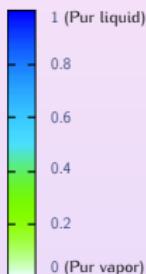
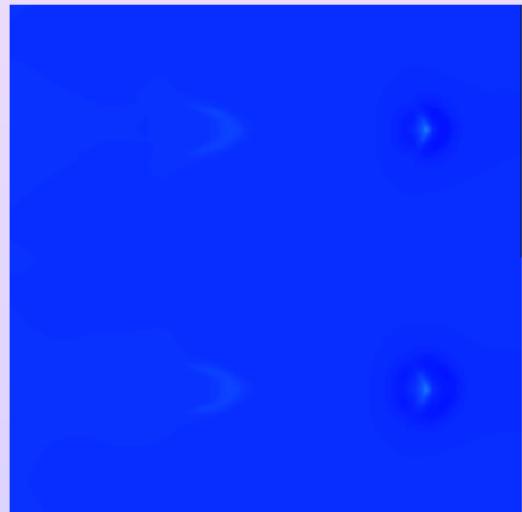
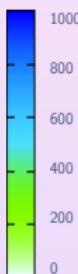
Massee fraction y Density ϱ 

◀ Geometry

▶ Play

▶ Skip

COMPRESSION OF VAPOR BUBBLES

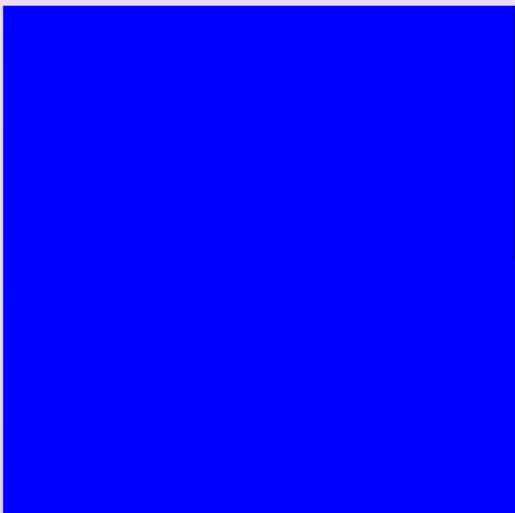
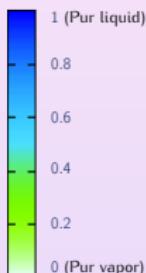
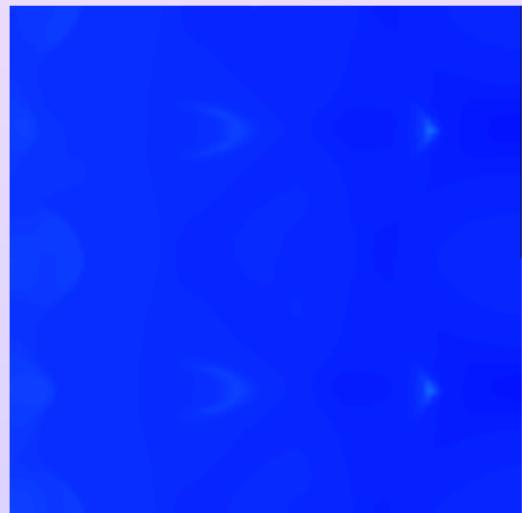
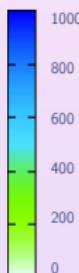
Massee fraction y Density ϱ 

◀ Geometry

▶ Play

▶ Skip

COMPRESSION OF VAPOR BUBBLES

Massee fraction y Density ϱ 

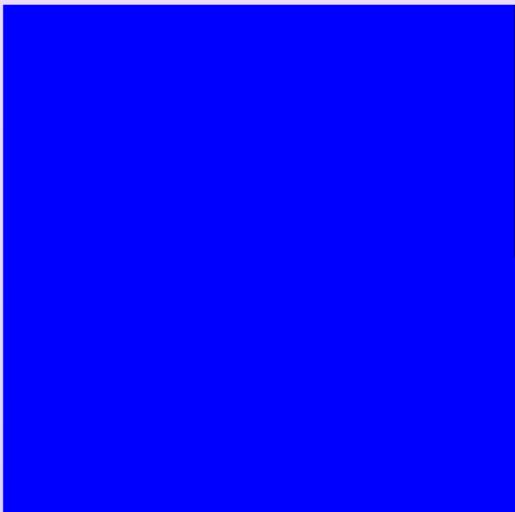
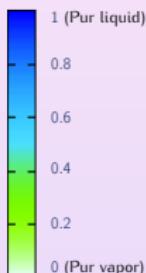
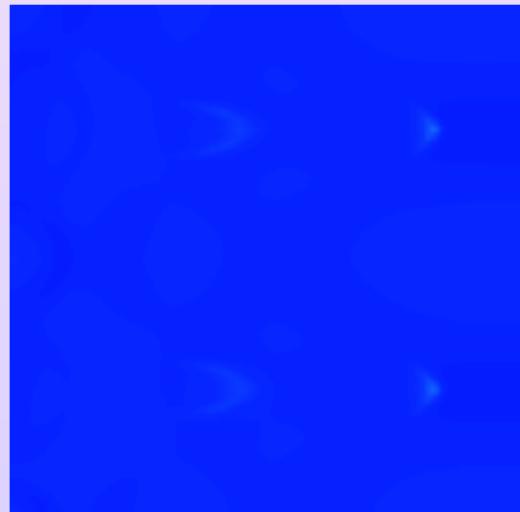
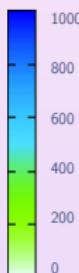
◀ Geometry

▶ Play

▶ Skip



COMPRESSION OF VAPOR BUBBLES

Massee fraction y Density ϱ 

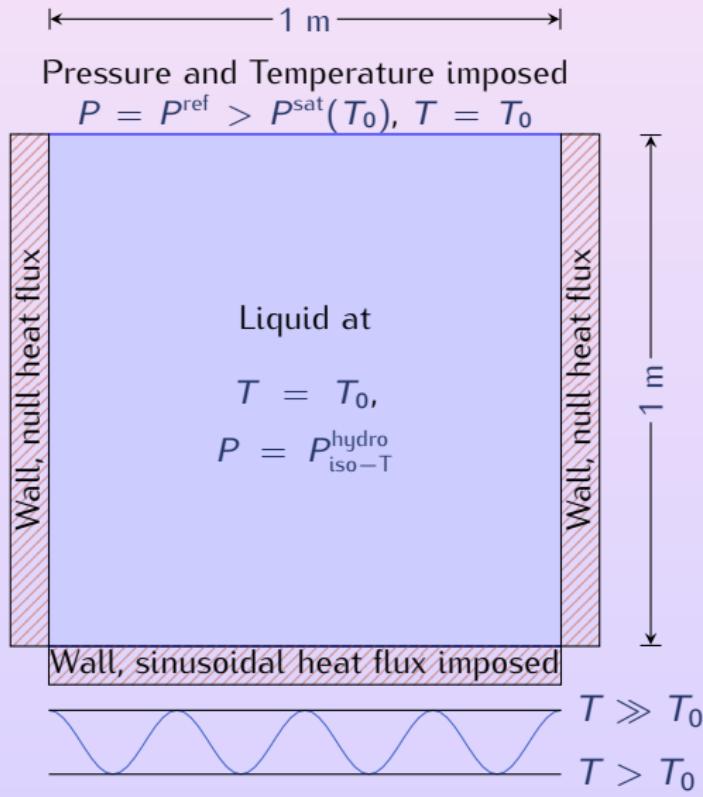
◀ Geometry

▶ Play

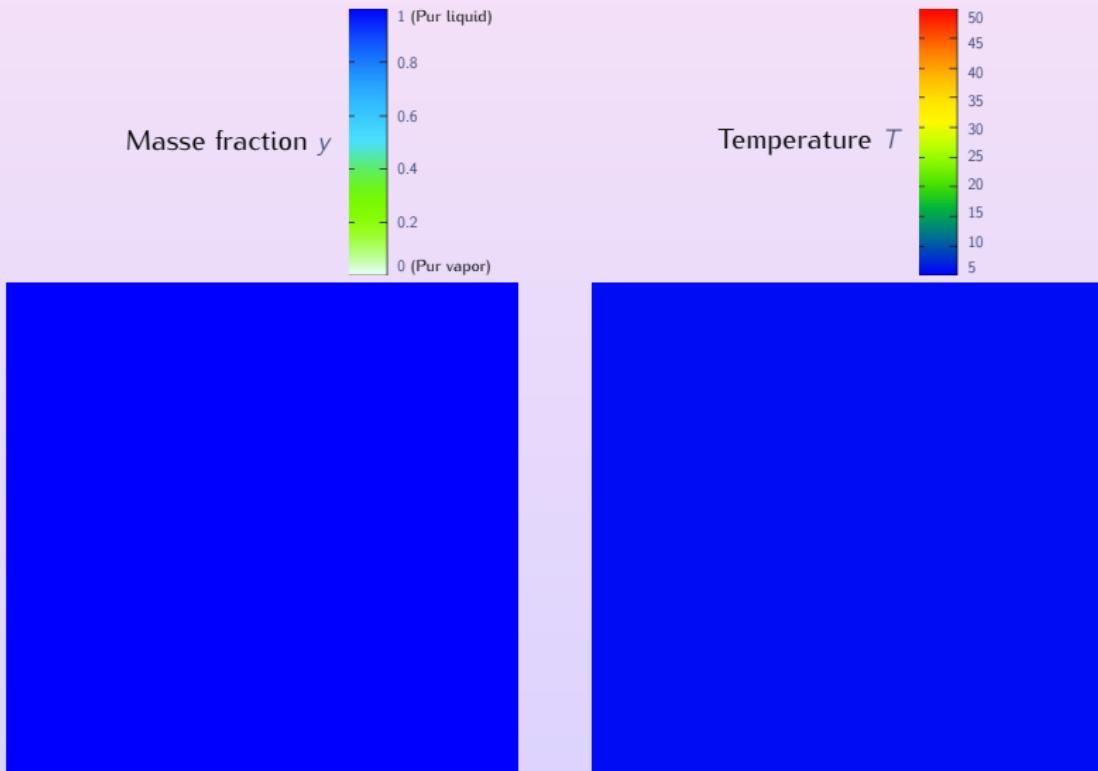
▶ Skip



TRANSITION TO A FILM BOILING



TRANSITION TO A FILM BOILING

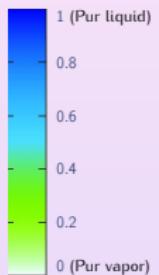
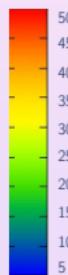


◀ Geometry

▶ Play

▶ Skip

TRANSITION TO A FILM BOILING

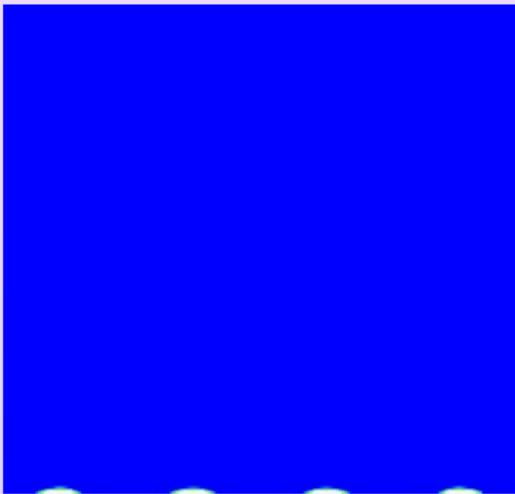
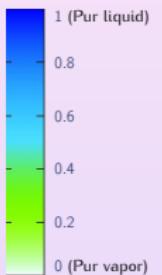
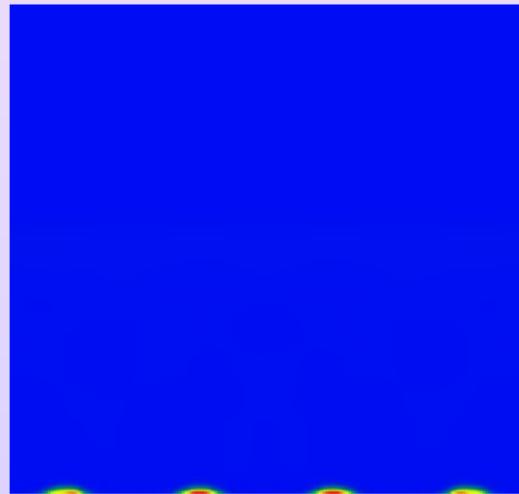
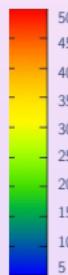
Massee fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

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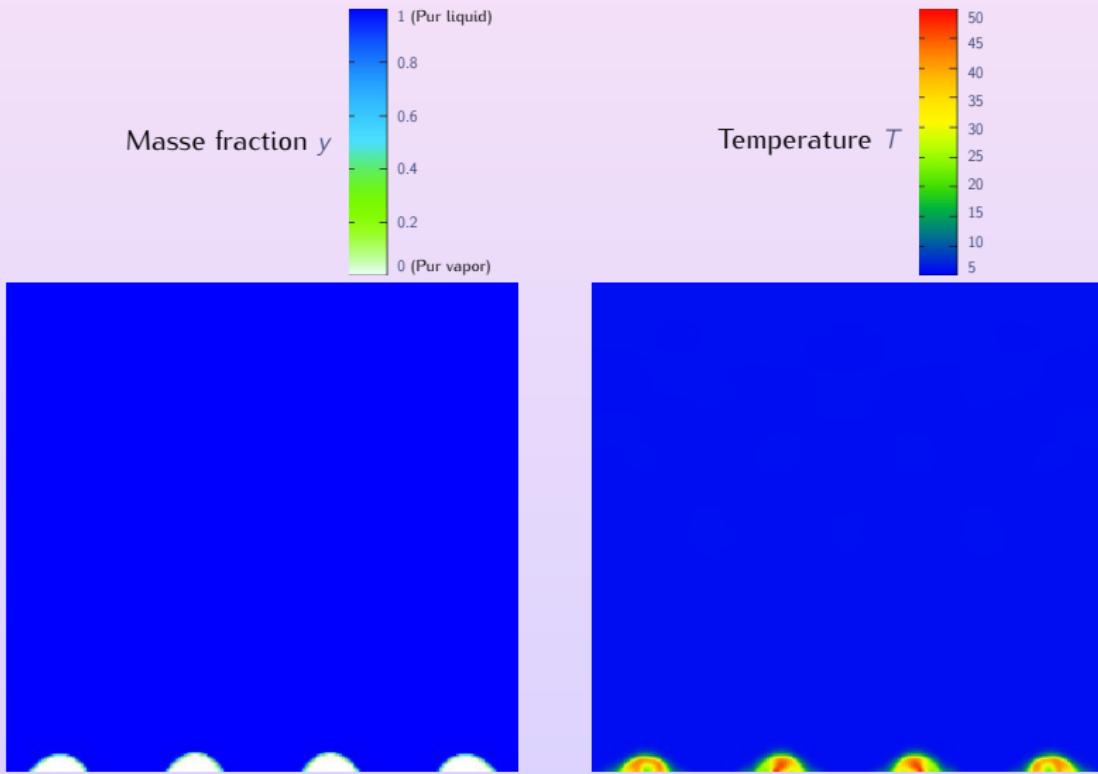
Massee fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

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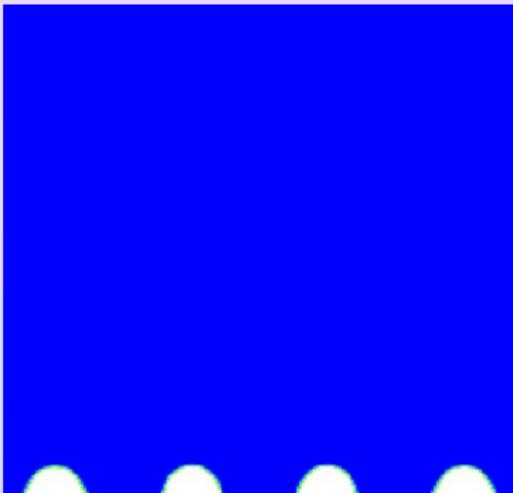
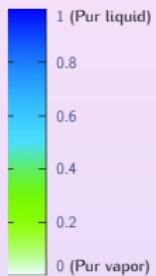
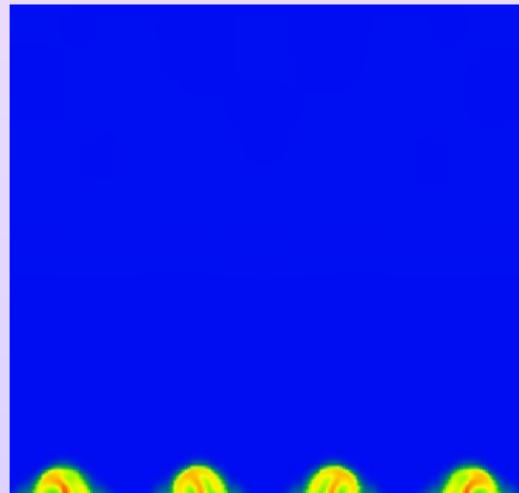


◀ Geometry

▶ Play

▶ Skip

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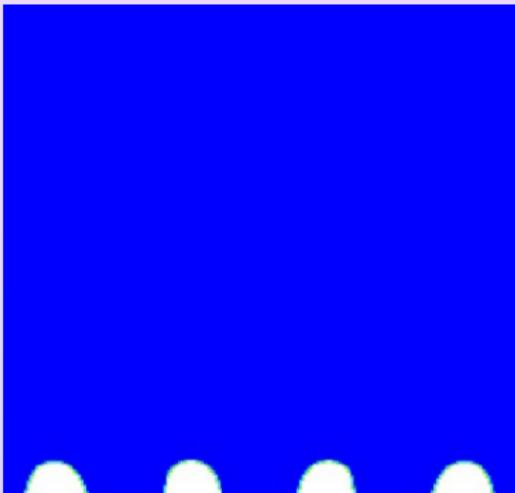
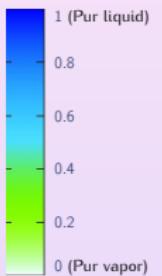
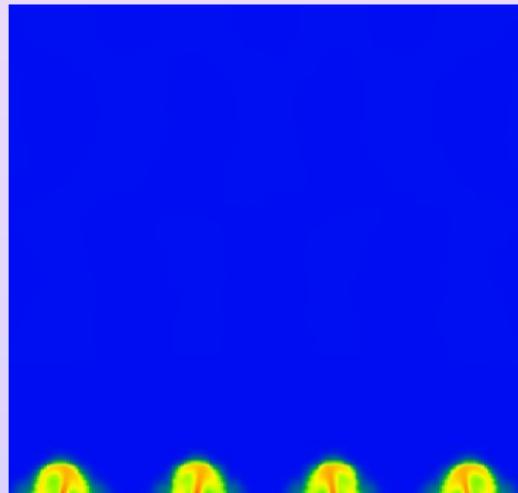
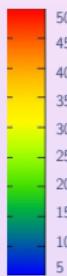
Massee fraction y Temperature T 

◀ Geometry

▶ Play

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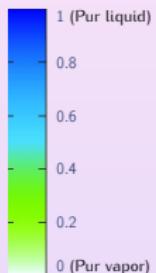
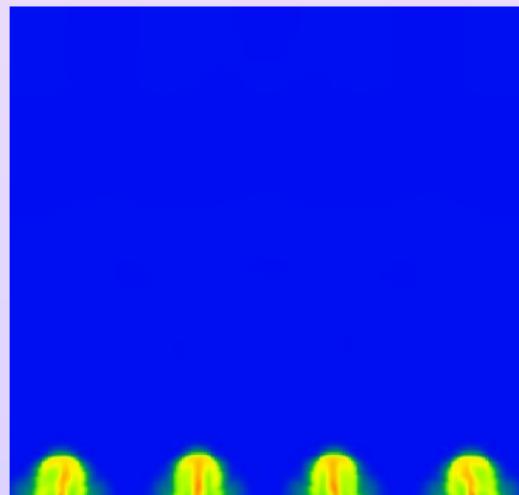
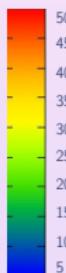
Massee fraction y Temperature T 

◀ Geometry

▶ Play

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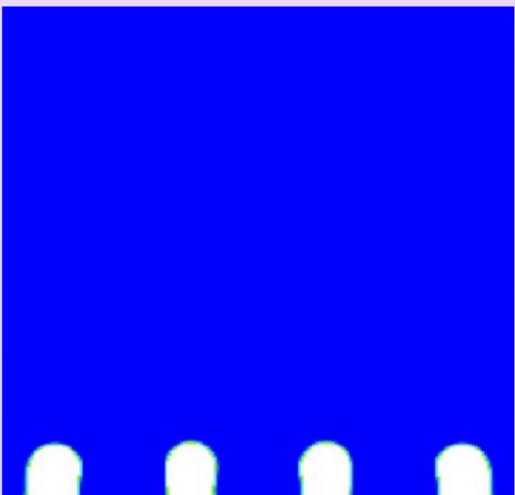
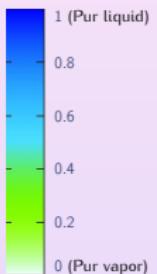
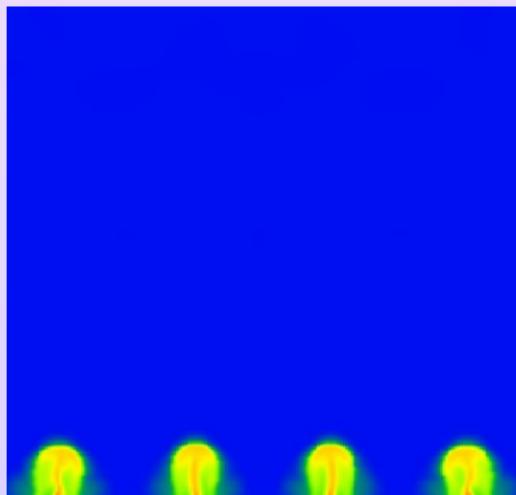
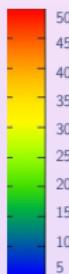
Massee fraction y Temperature T 

◀ Geometry

▶ Play

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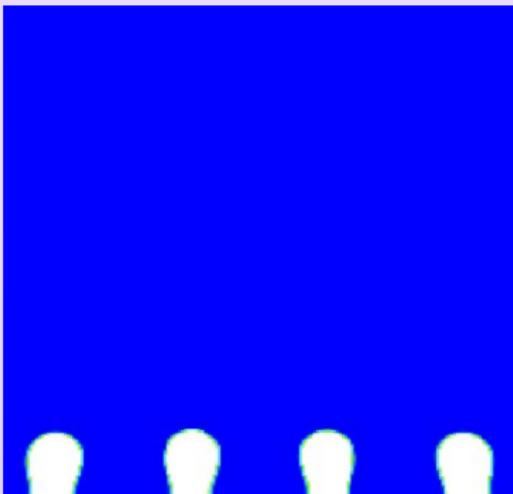
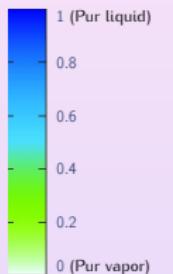
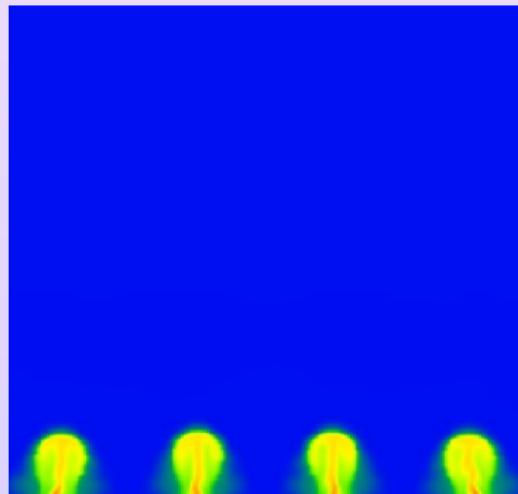
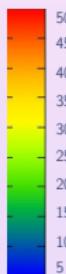
Massee fraction y Temperature T 

◀ Geometry

▶ Play

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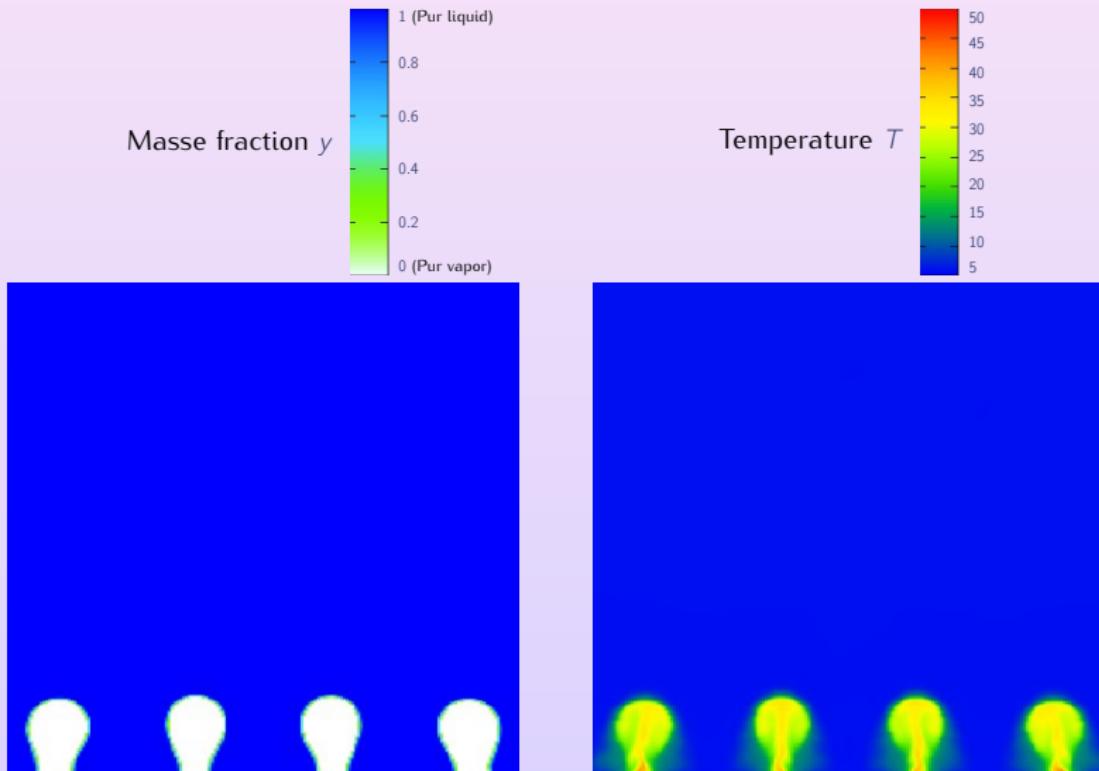
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◀ Geometry

▶ Play

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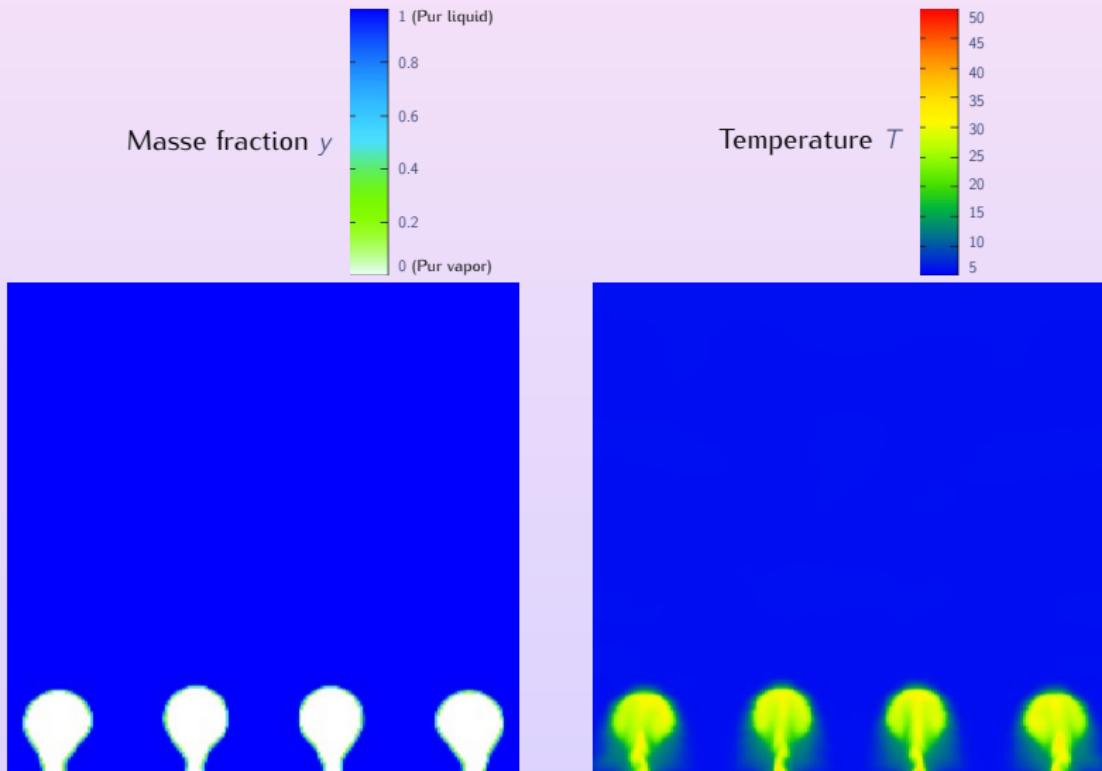


◀ Geometry

▶ Play

▶ Skip

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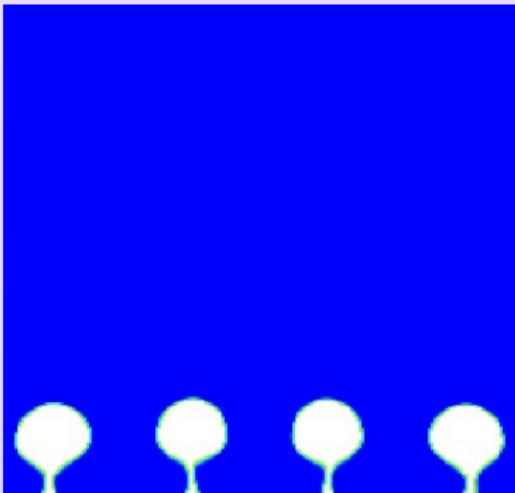
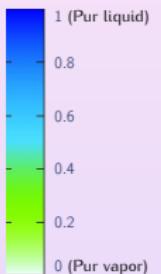
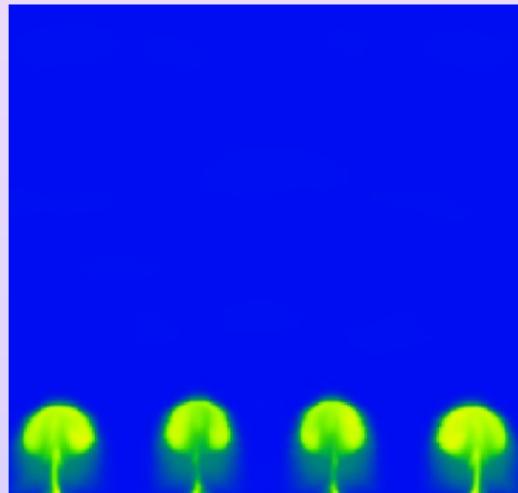
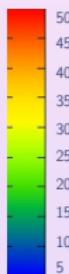


◀ Geometry

▶ Play

▶ Skip

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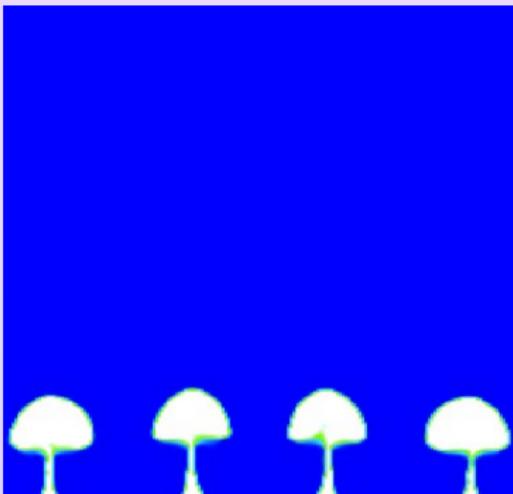
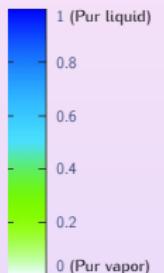
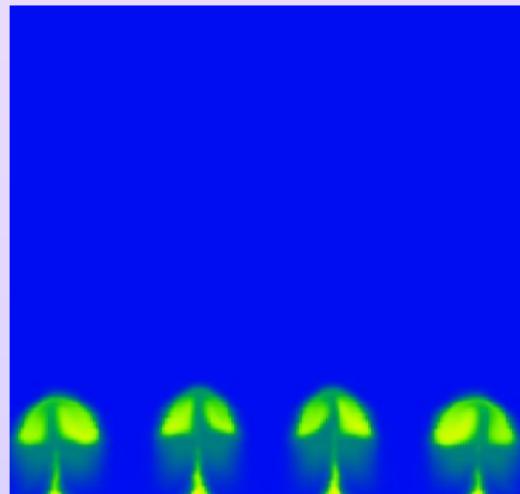
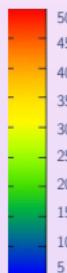
Massee fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

TRANSITION TO A FILM BOILING

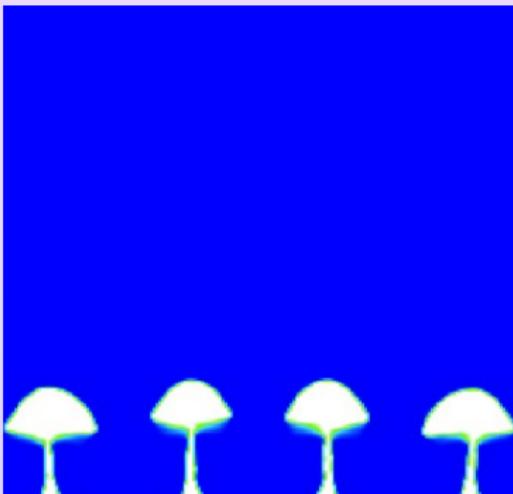
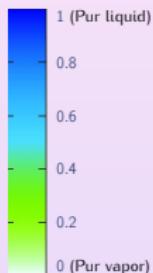
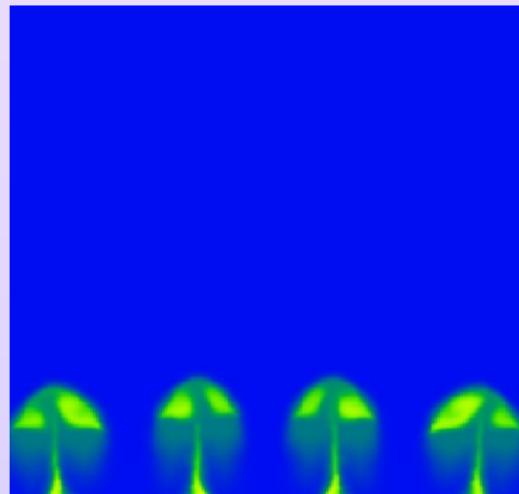
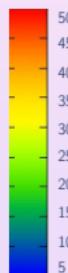
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◀ Geometry

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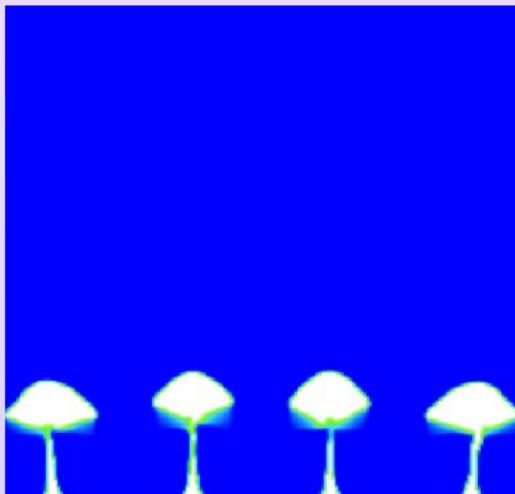
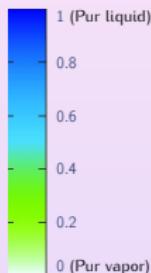
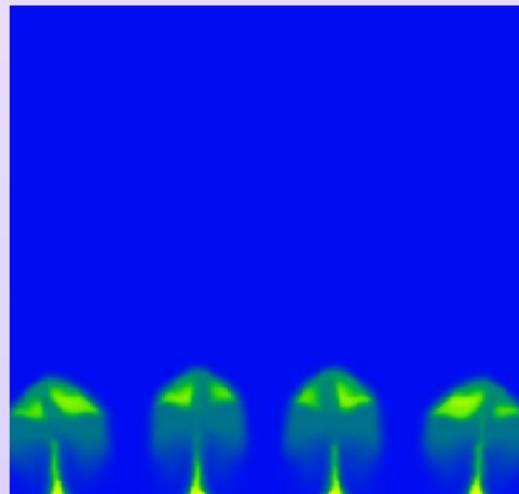
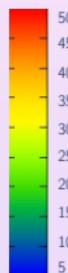
Massee fraction y Temperature T 

◀ Geometry

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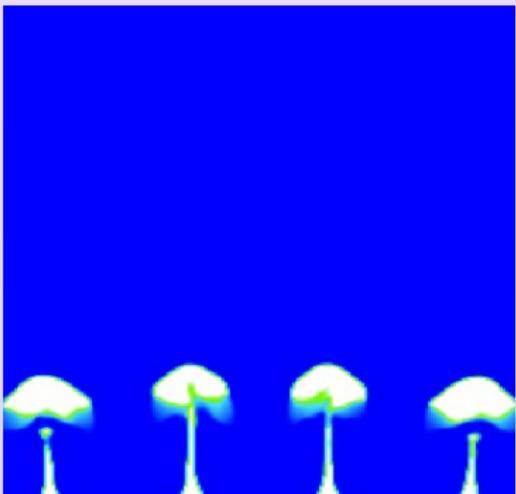
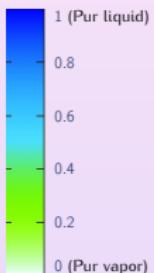
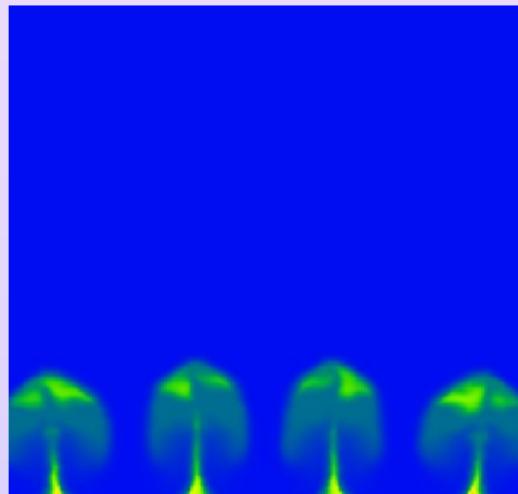
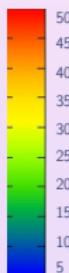
Massee fraction y Temperature T 

◀ Geometry

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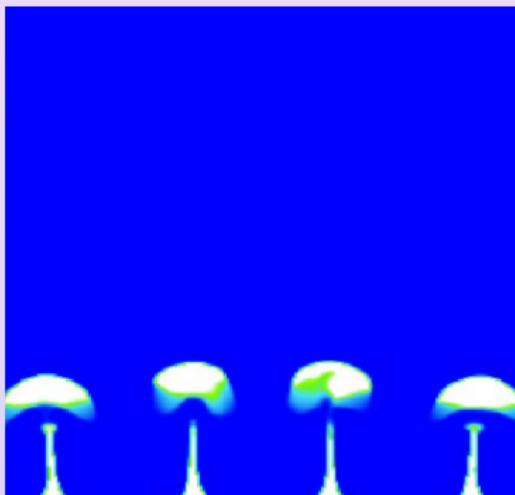
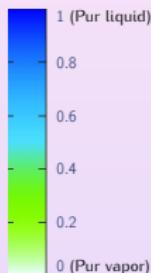
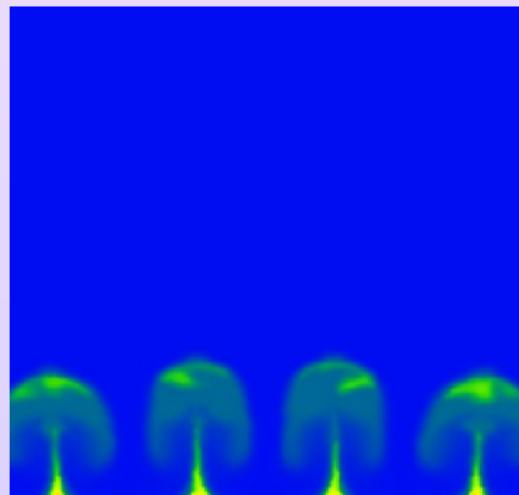
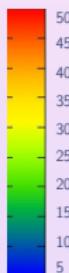
Massee fraction y Temperature T 

◀ Geometry

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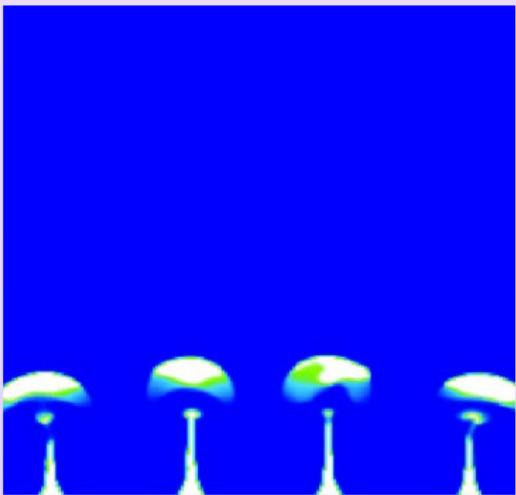
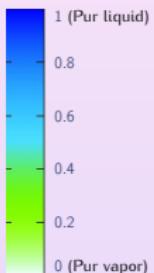
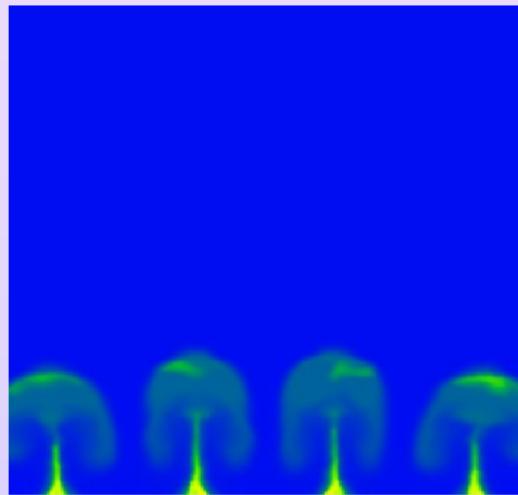
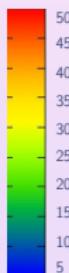
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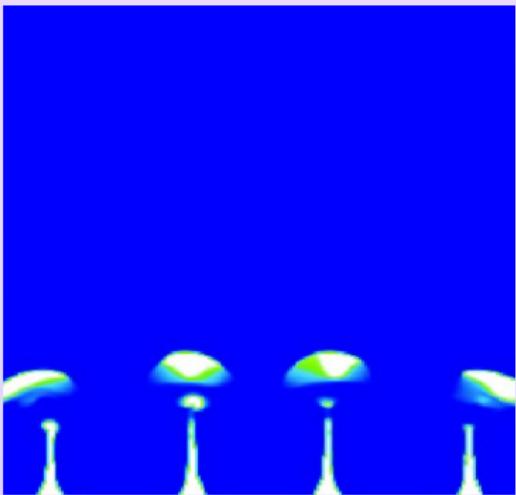
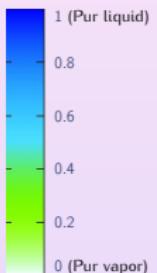
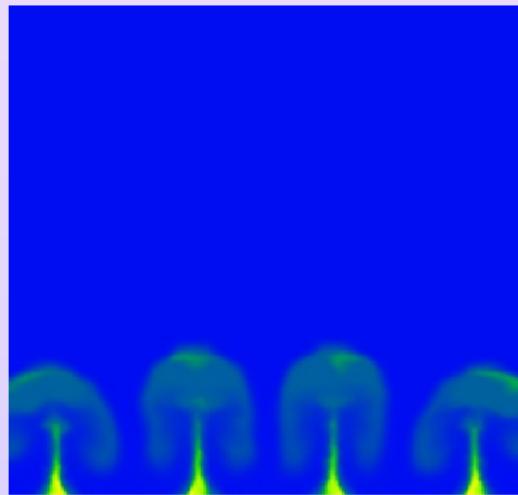
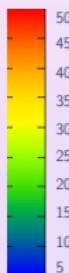
Massee fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

TRANSITION TO A FILM BOILING

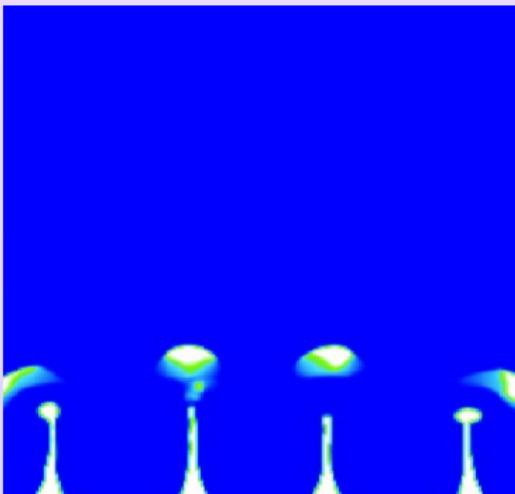
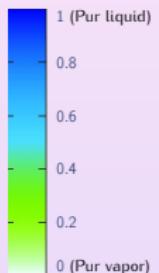
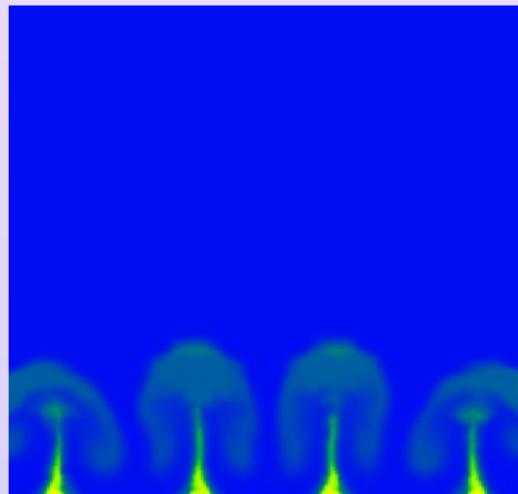
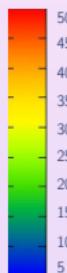
Massee fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

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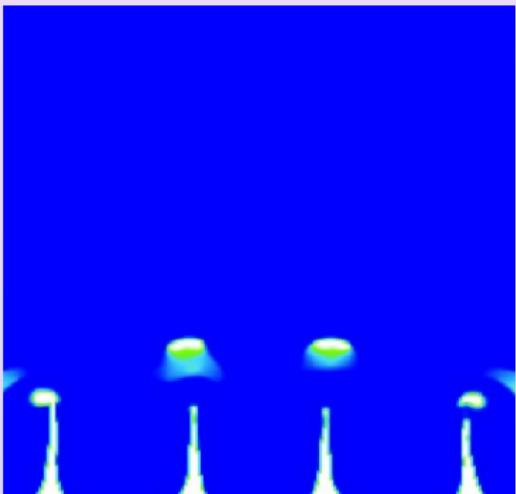
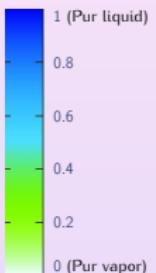
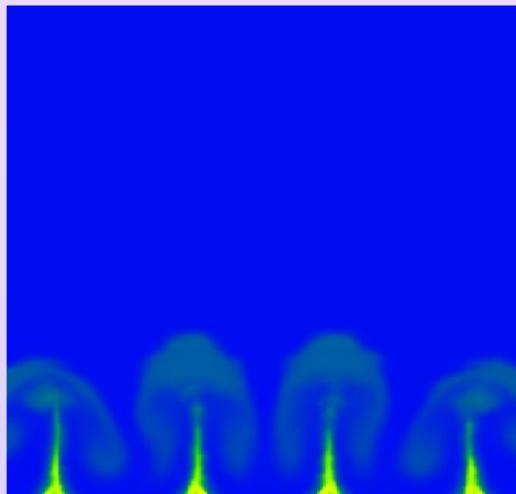
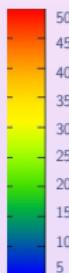
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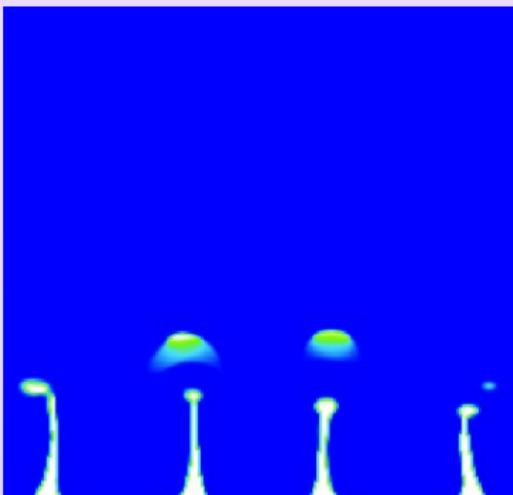
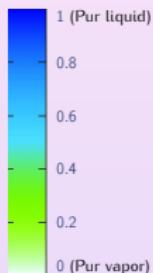
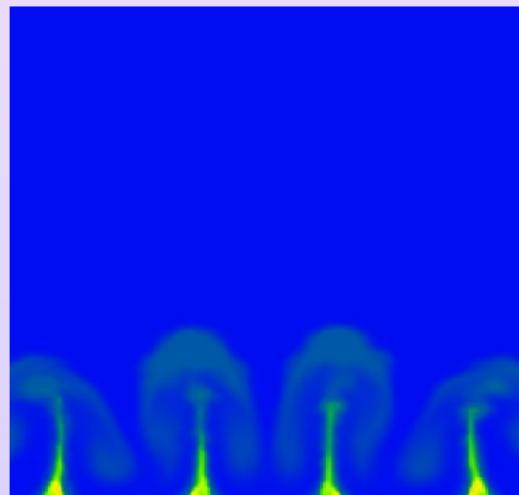
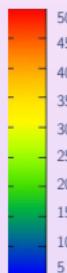
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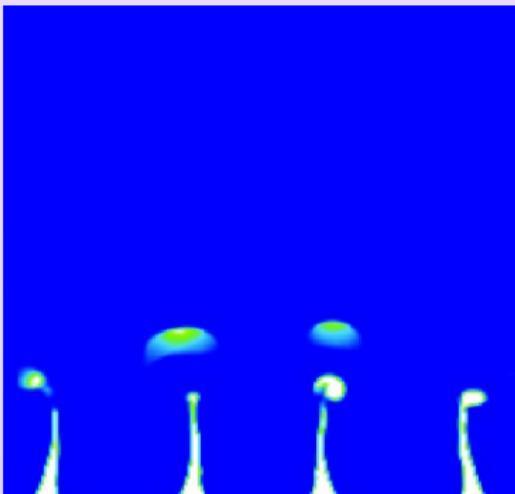
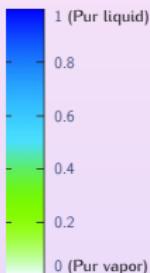
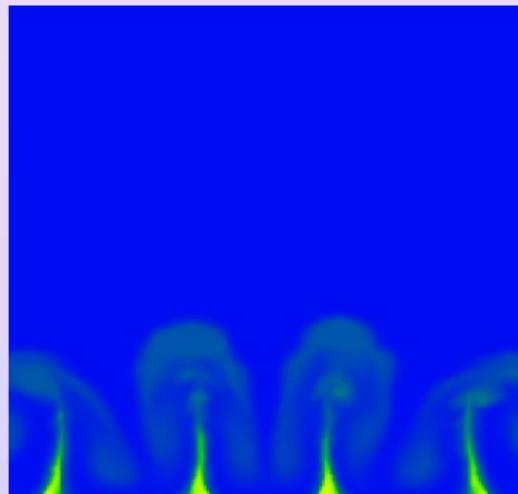
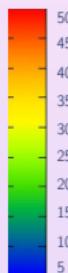
Massee fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

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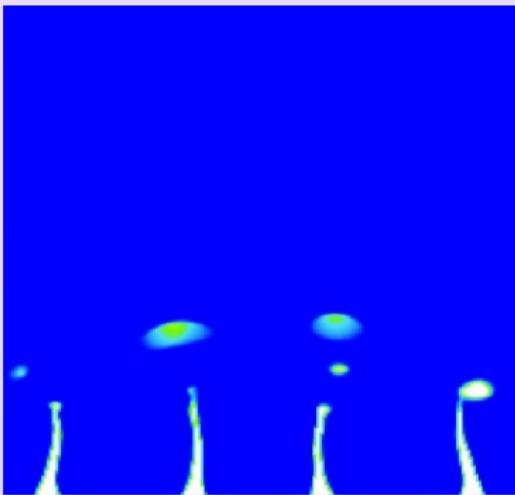
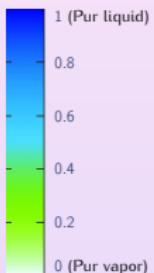
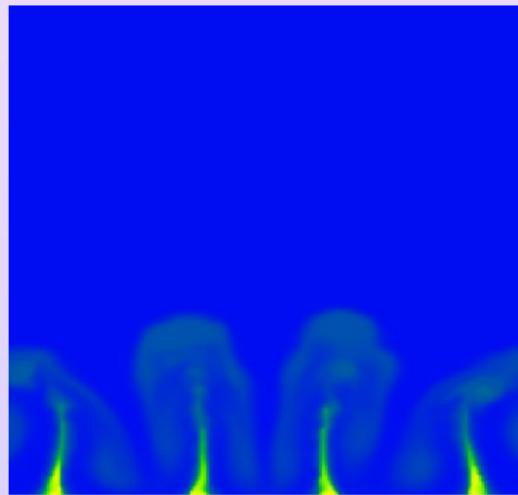
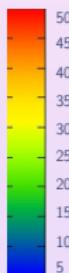
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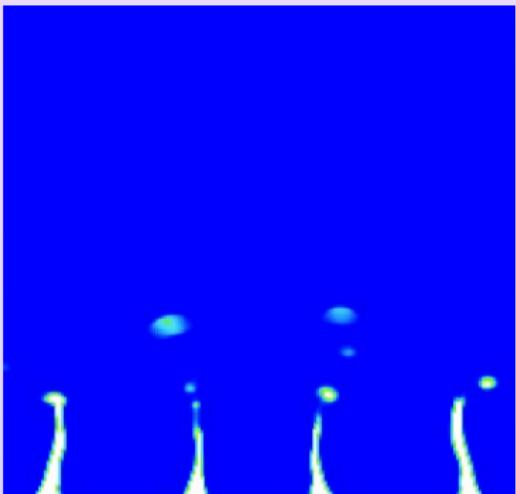
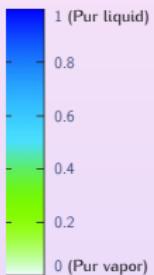
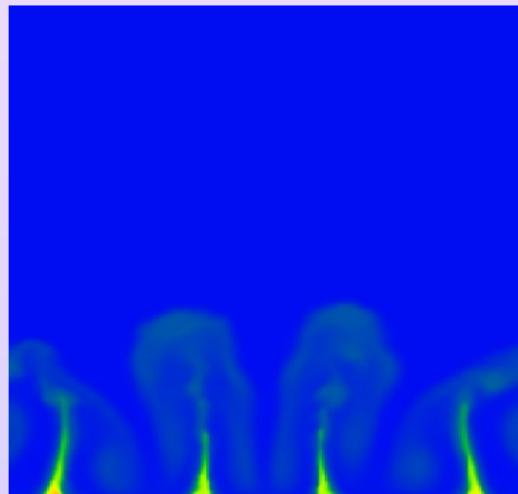
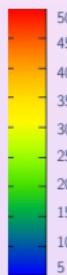
Massee fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

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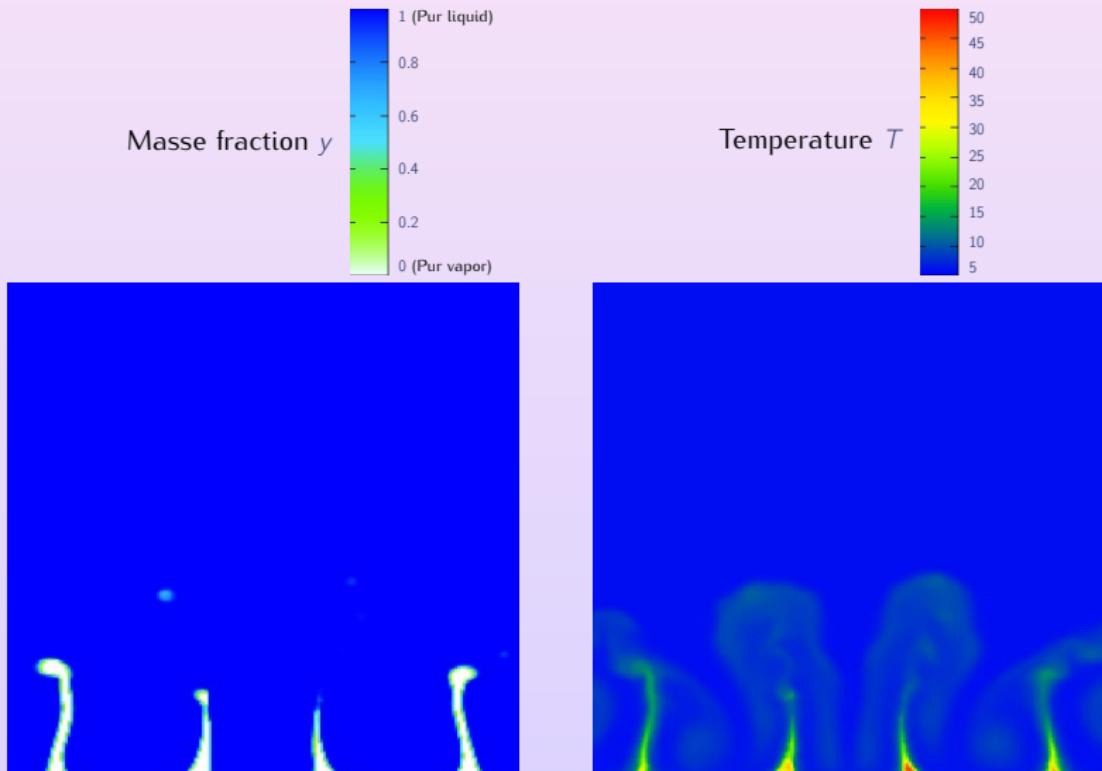
Massee fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

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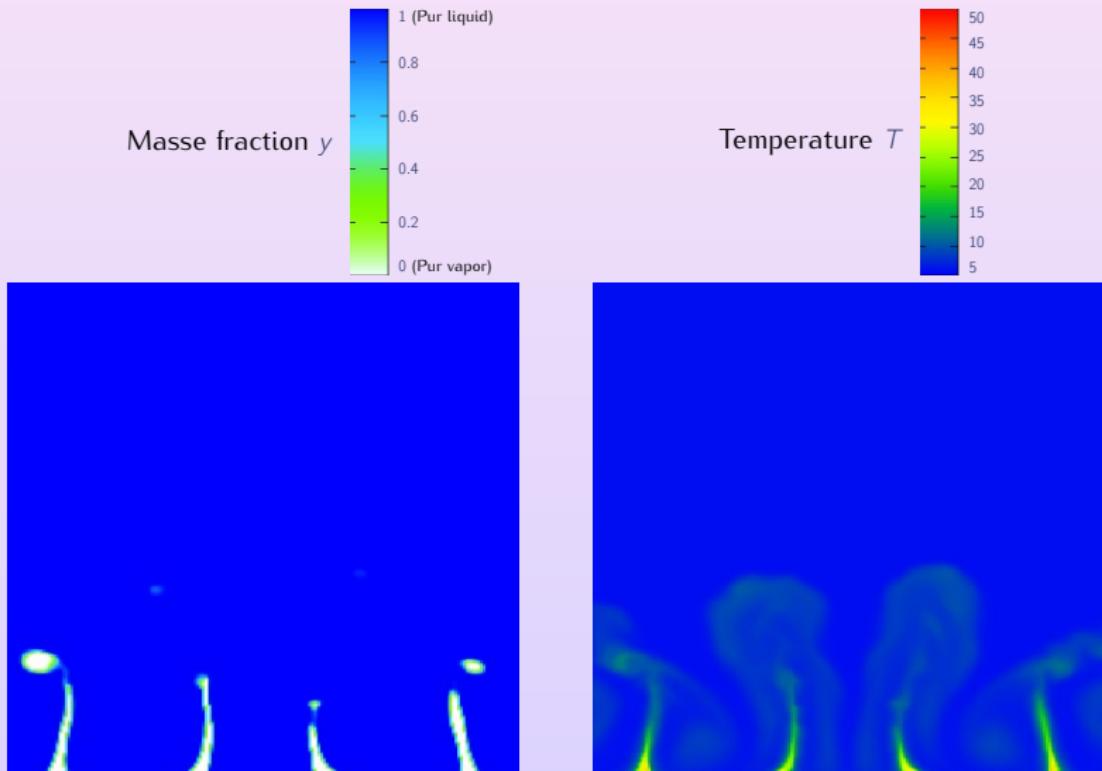


◀ Geometry

▶ Play

▶ Skip

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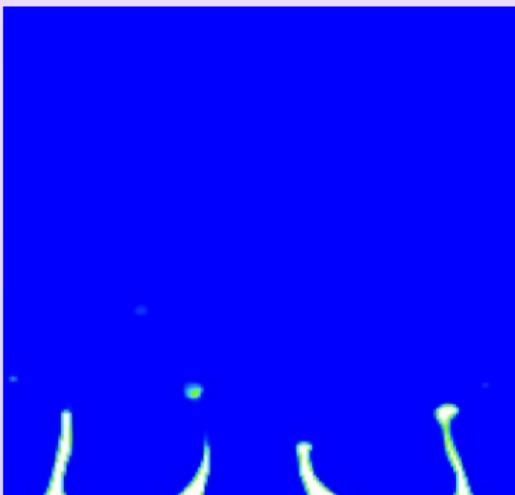
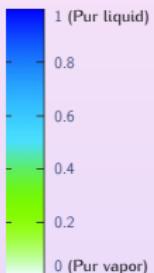
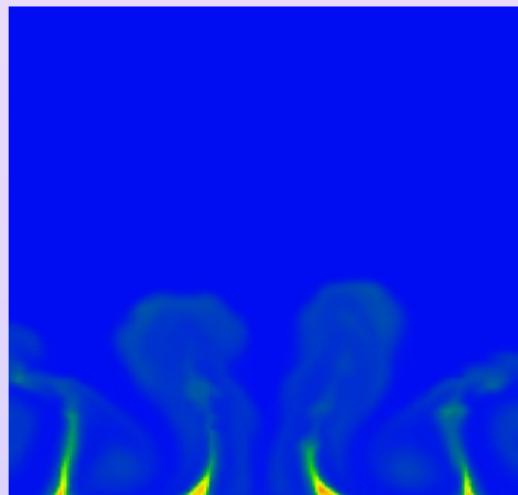
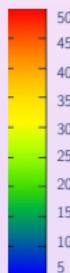


◀ Geometry

▶ Play

▶ Skip

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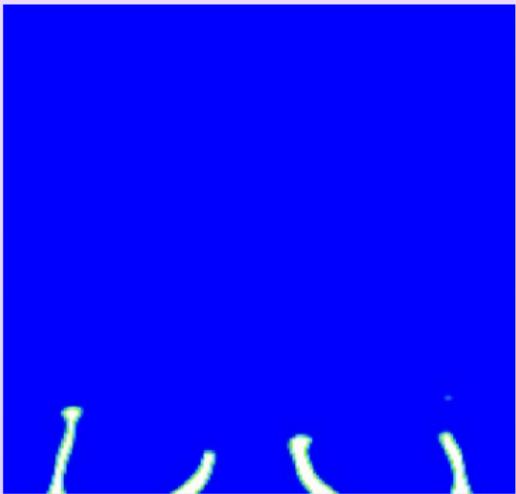
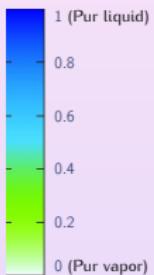
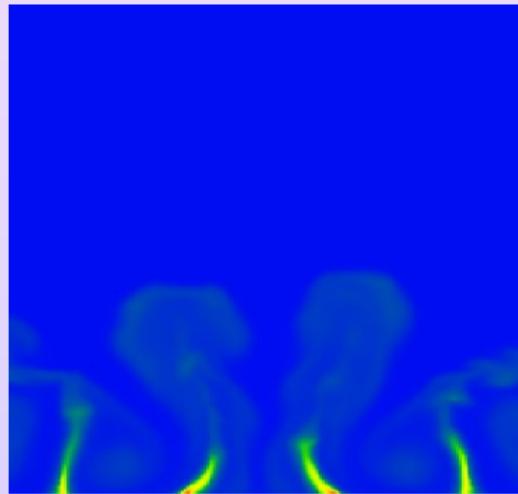
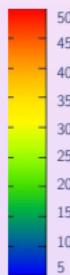
Massee fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

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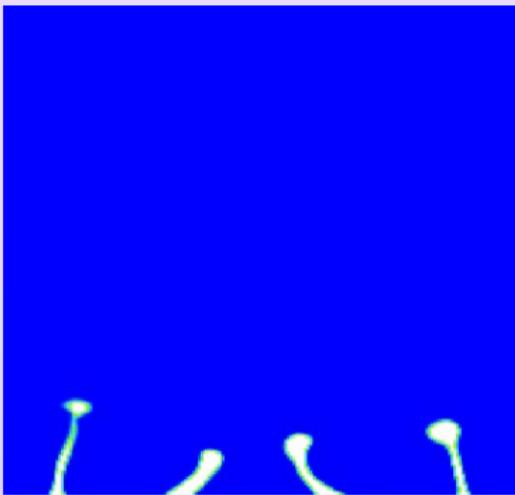
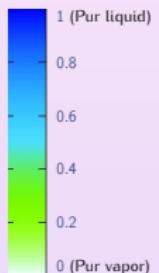
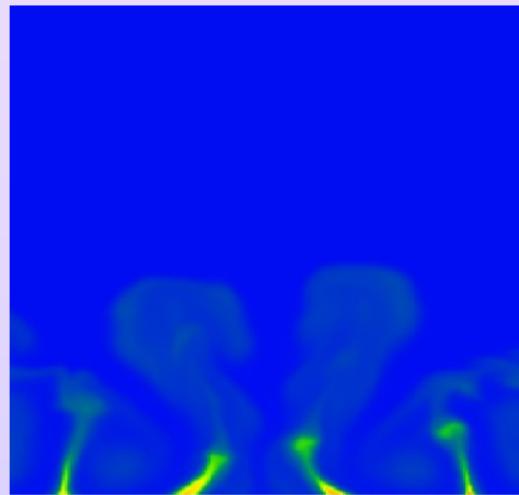
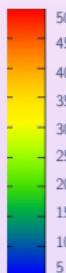
Massee fraction y Temperature T 

◀ Geometry

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▶ Skip

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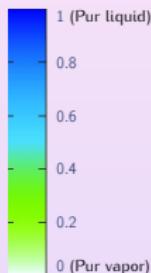
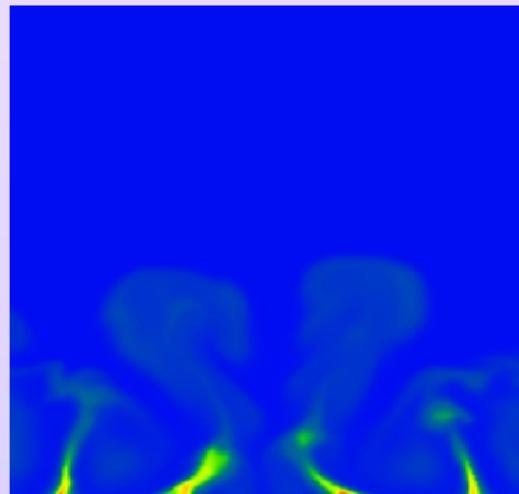
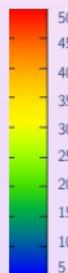
Massee fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

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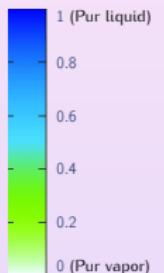
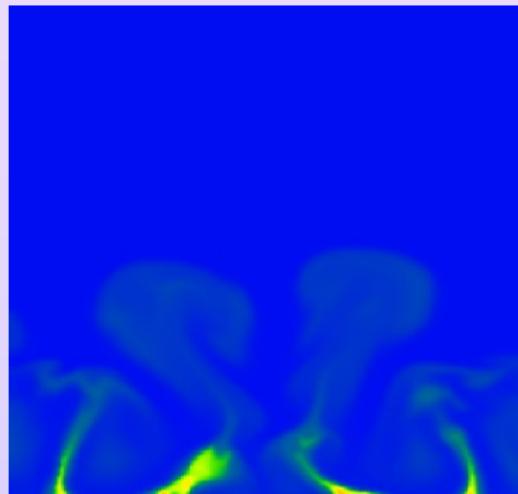
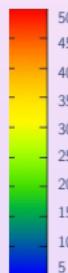
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◀ Geometry

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TRANSITION TO A FILM BOILING

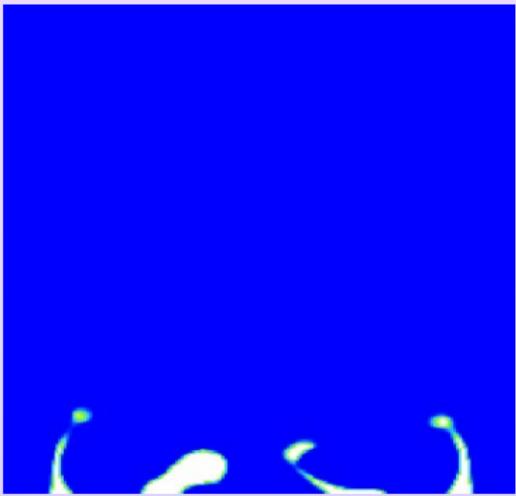
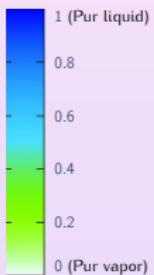
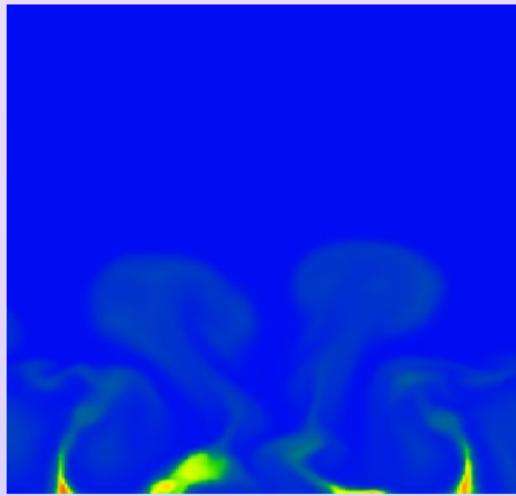
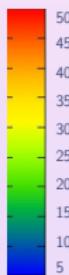
Massee fraction y Temperature T 

◀ Geometry

▶ Play

▶ Skip

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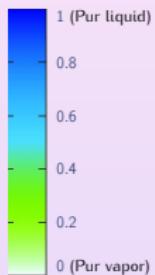
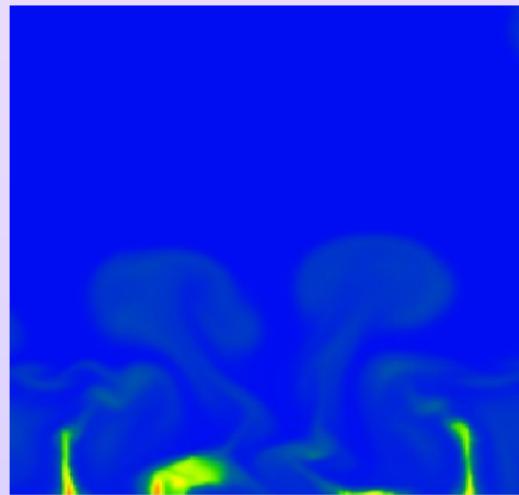
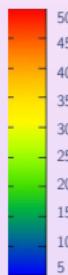
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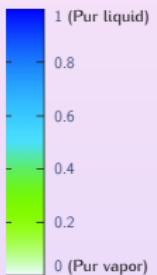
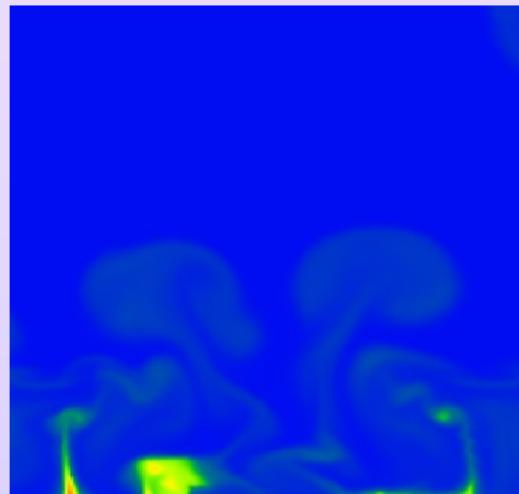
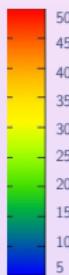
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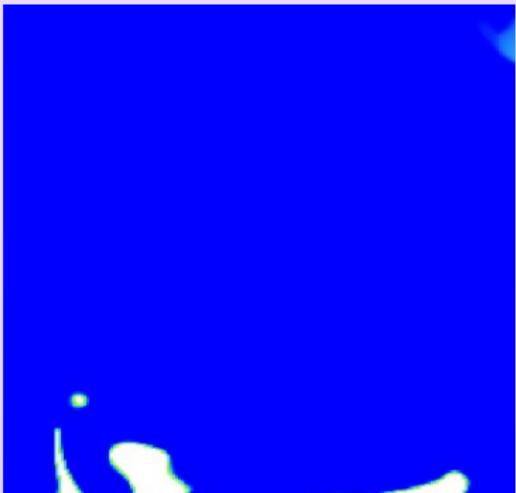
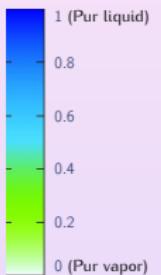
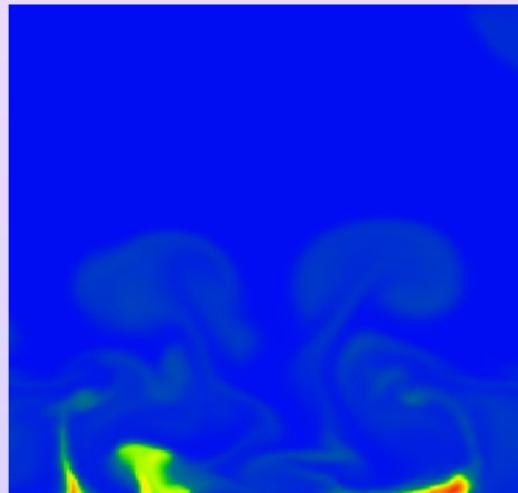
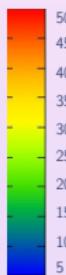
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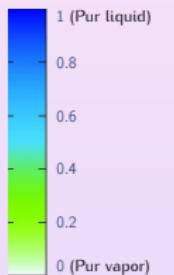
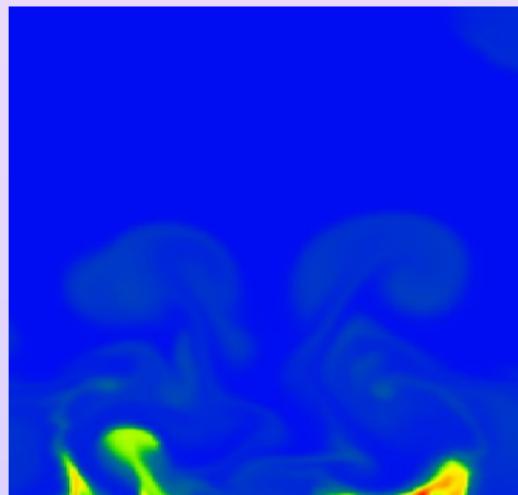
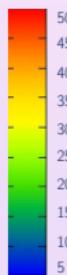
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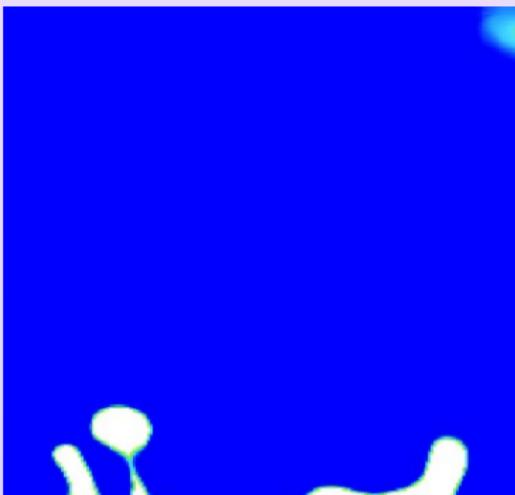
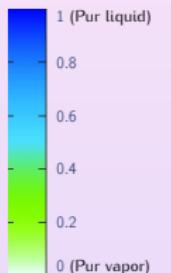
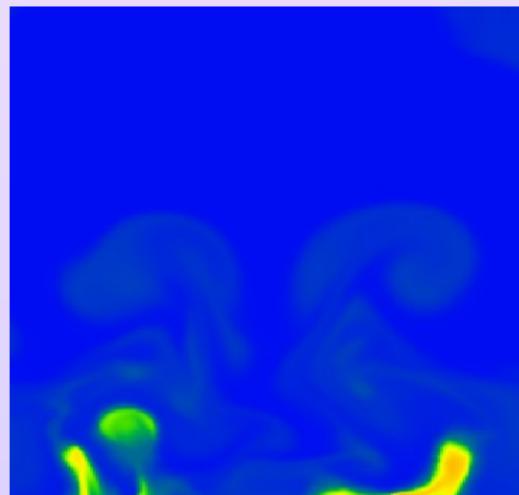
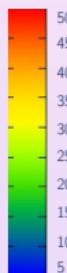
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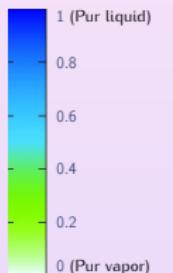
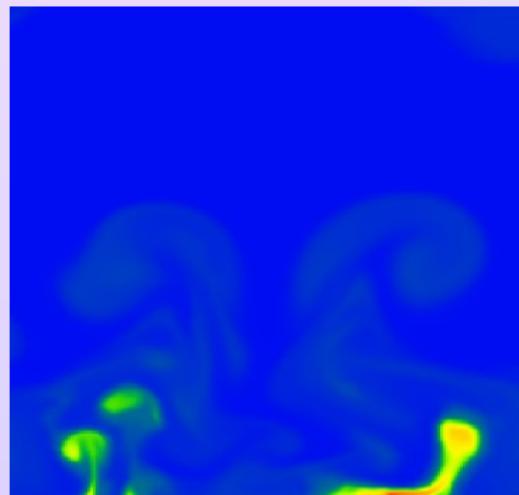
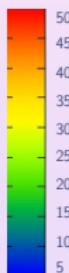
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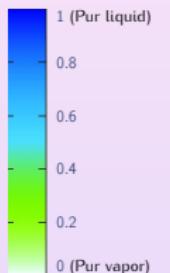
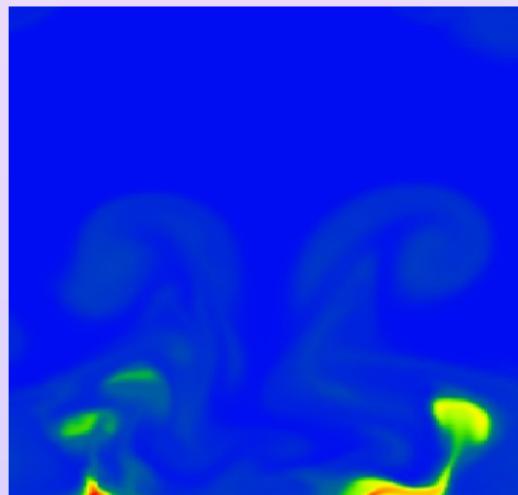
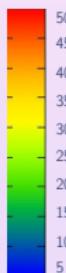
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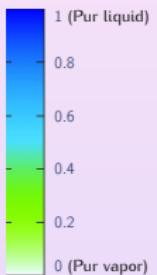
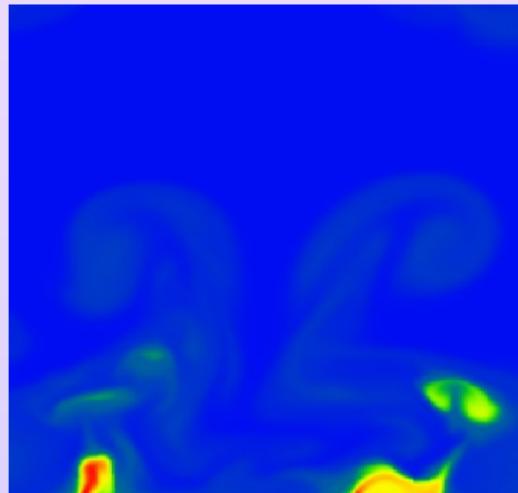
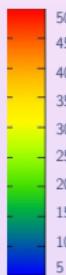
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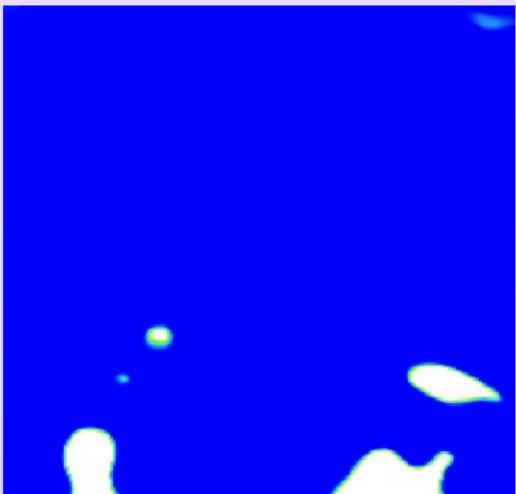
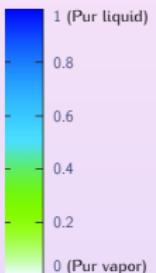
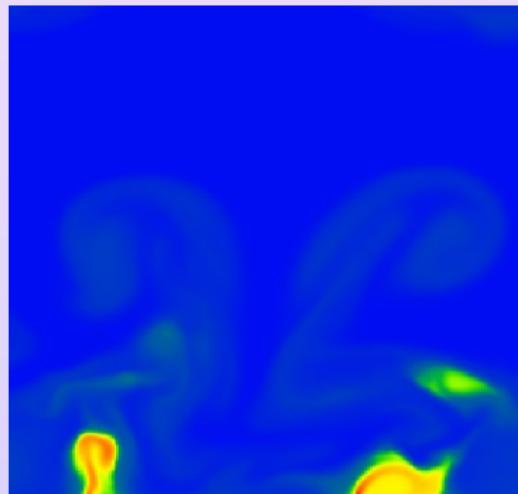
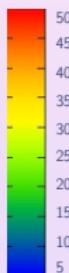
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◀ Geometry

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▶ Skip

TRANSITION TO A FILM BOILING

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◀ Geometry

▶ Play

▶ Skip

OUTLINE

1 Context

2 Model

- Equation of State
- Conservation Laws

3 Numerical Approximation and Example

- The Phase Change Equation
- Numerical Scheme and Example

4 Conclusion

SUMMARY & PERSPECTIVES

• Model

- ✓ based on a general construction of the Equilibrium EOS (also for tabulated data),
- Numerical Method based on the relaxation approach: off-equilibrium system with relaxation terms
 - ✓ preliminary results: dynamic generation of a phase in a 2D-flow in a pure phase with surface tension, gravity and heat diffusion,
 - ✓ transition: liquid phase → nucleating boiling → film boiling

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- ✗ quantitative simulations: tabulated EOS for pure phases, implicit transport step (Low Mach) and 3D (parallelization).



APPENDIX

- ▶ Stiffened Gas for Water
- ▶ Tabulated EOS for Water
- ▶ Speed of Sound
- ▶ Isentropic Curves
- ▶ Surface Tension
- ▶ Metastability
- ▶ Critical Point
- ▶ Summary & To Do

STIFFENED GAS FOR WATER

Phase	c_v [J/(kg · K)]	γ	π [Pa]	q [J/kg]	m [J/(kg · K)]
Water	1816.2	2.35	10^9	-1167.056×10^3	-32765.55596
Steam	1040.14	1.43	0	2030.255×10^3	-33265.65947

Table: Parameters proposed by [O. LE METAYER] for water.

$$(\tau_\alpha, \varepsilon_\alpha) \mapsto s_\alpha = c_{v_\alpha} \ln(\varepsilon_\alpha - q_\alpha - \pi_\alpha \tau_\alpha) + c_{v_\alpha} (\gamma_\alpha - 1) \ln \tau_\alpha + m_\alpha$$

$$(P, T) \mapsto \varepsilon_\alpha = c_{v_\alpha} T \frac{P + \pi_\alpha \gamma_\alpha}{P + \pi_\alpha} + q_\alpha, \quad (P, T) \mapsto \tau_\alpha = c_{v_\alpha} (\gamma_\alpha - 1) \frac{T}{P + \pi_\alpha}.$$

$$\left. \begin{array}{l} T^i = 278\text{K} \dots 610\text{K}, \\ g_1(P, T^i) = g_2(P, T^i) \Rightarrow P^{\text{sat}}(T^i) \end{array} \right\} \Rightarrow \mathfrak{A} = \{(T^i, P^{\text{sat}}(T^i))\}_{i=0}^{83}$$

\hat{P}^{sat} defined by using a least square approximation of \mathfrak{A} :

$$T \mapsto P^{\text{sat}}(T) \approx \hat{P}^{\text{sat}}(T) \stackrel{\text{def}}{=} \exp \left(\sum_{k=-8}^{k=8} a_k T^k \right)$$

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WATER TABULATED EOS

$$T^i = 278\text{K} \dots 610\text{K}, \quad \varepsilon_{\alpha}^{\text{sat}}(T^i), \tau_{\alpha}^{\text{sat}}(T^i) \text{ found in the tables} \quad \left. \right\} \Rightarrow \begin{cases} \mathfrak{A} = \left\{ \left(T_i, \frac{1}{\varepsilon_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{B} = \left\{ \left(T_i, \frac{\varepsilon_{\text{liq}}^{\text{sat}}(T_i)}{\varepsilon_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{C} = \left\{ \left(T_i, \frac{1}{\tau_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{D} = \left\{ \left(T_i, \frac{\tau_{\text{liq}}^{\text{sat}}(T_i)}{\tau_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \end{cases}$$

$\hat{\varepsilon}_{\alpha}^{\text{sat}}$ and $\hat{\tau}_{\alpha}^{\text{sat}}$ defined by using a least square approximation of \mathfrak{A} , \mathfrak{B} , \mathfrak{C} and \mathfrak{D} :

$$T \mapsto \varepsilon_{\text{vap}}^{\text{sat}} \approx \hat{\varepsilon}_{\text{vap}}^{\text{sat}} \stackrel{\text{def}}{=} \frac{1}{\sum_{k=0}^6 a_k T^k}$$

$$T \mapsto \tau_{\text{vap}}^{\text{sat}} \approx \hat{\tau}_{\text{vap}}^{\text{sat}} \stackrel{\text{def}}{=} \frac{1}{\sum_{k=0}^8 c_k T^k}$$

$$T \mapsto \varepsilon_{\text{liq}}^{\text{sat}} \approx \hat{\varepsilon}_{\text{liq}}^{\text{sat}} \stackrel{\text{def}}{=} \hat{\varepsilon}_{\text{vap}}^{\text{sat}}(T) \sum_{k=0}^6 b_k T^k$$

$$T \mapsto \tau_{\text{liq}}^{\text{sat}} \approx \hat{\tau}_{\text{liq}}^{\text{sat}} \stackrel{\text{def}}{=} \hat{\tau}_{\text{vap}}^{\text{sat}}(T) \sum_{k=0}^9 d_k T^k$$

SPEED OF SOUND

$$c^2 \stackrel{\text{def}}{=} \tau^2 \left(P^{\text{eq}} \frac{\partial P^{\text{eq}}}{\partial \varepsilon} \Big|_{\tau} - \frac{\partial P^{\text{eq}}}{\partial \tau} \Big|_{\varepsilon} \right) = \begin{array}{c} \text{---} \\ \text{---} \\ \text{---} \end{array} \boxed{-\tau^2 T^{\text{eq}}} \quad \boxed{[P^{\text{eq}}, \quad -1]} \begin{bmatrix} S_{\varepsilon\varepsilon}^{\text{eq}} & S_{\tau\varepsilon}^{\text{eq}} \\ S_{\tau\varepsilon}^{\text{eq}} & S_{\tau\tau}^{\text{eq}} \end{bmatrix} \begin{bmatrix} P^{\text{eq}} \\ -1 \end{bmatrix}$$

HESSIAN MATRIX OF $w \mapsto s^{\text{eq}}$

- for all w pure phase state

$$\mathbf{v}^T d^2 s^{\text{eq}}(\mathbf{w}) \mathbf{v} < 0 \quad \forall \mathbf{v} \neq 0,$$

- for all w equilibrium mixture state

$$\exists \mathbf{v}(\mathbf{w}) \neq 0 \text{ s.t. } (\mathbf{v}(\mathbf{w}))^T d^2 s^{\text{eq}}(\mathbf{w}) \mathbf{v}(\mathbf{w}) = 0.$$

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HESSIAN MATRIX OF $w \mapsto s^{\text{eq}}$

- for all w pure phase state

$$v^T d^2 s^{\text{eq}}(w) v < 0 \quad \forall v \neq 0,$$

- for all w equilibrium mixture state

$$\exists v(w) \neq 0 \text{ s.t. } (v(w))^T d^2 s^{\text{eq}}(w) v(w) = 0.$$

SPEED OF SOUND

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$\forall \mathbf{w}$ equilibrium mixture state, $\mathbf{v}(\mathbf{w}) \stackrel{?}{\equiv} [P^{\text{eq}}(\mathbf{w}), -1]$

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HESSIAN MATRIX OF $\mathbf{w} \mapsto s^{\text{eq}}$

- for all \mathbf{w} pure phase state

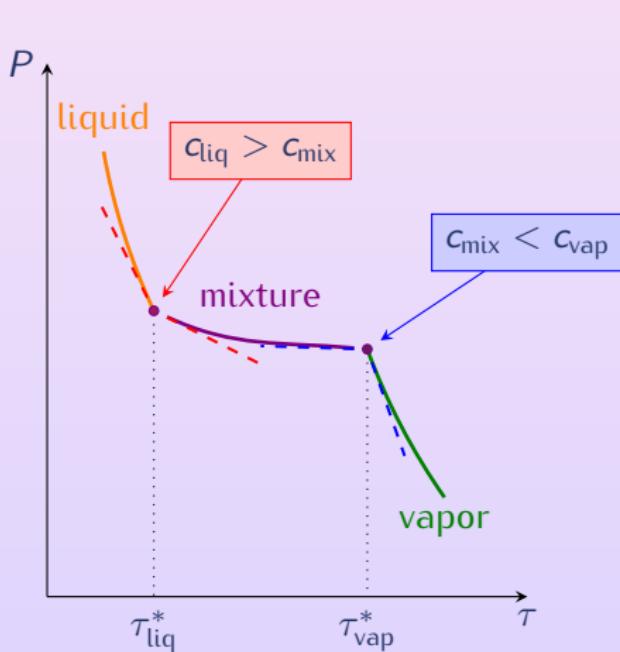
$$\mathbf{v}^T d^2 s^{\text{eq}}(\mathbf{w}) \mathbf{v} < 0 \quad \forall \mathbf{v} \neq 0,$$

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$$\exists \mathbf{v}(\mathbf{w}) \neq 0 \text{ s.t. } (\mathbf{v}(\mathbf{w}))^T d^2 s^{\text{eq}}(\mathbf{w}) \mathbf{v}(\mathbf{w}) = 0.$$

$\forall \mathbf{w}$ equilibrium mixture state, $\mathbf{v}(\mathbf{w}) \not\propto [P^{\text{eq}}(\mathbf{w}), -1]$

ISENTROPIC CURVES



$$\gamma \stackrel{\text{def}}{=} -\frac{\tau}{P} \left. \frac{\partial P}{\partial \tau} \right|_s$$

$$\Gamma \stackrel{\text{def}}{=} \tau \left. \frac{\partial P}{\partial \varepsilon} \right|_\tau$$

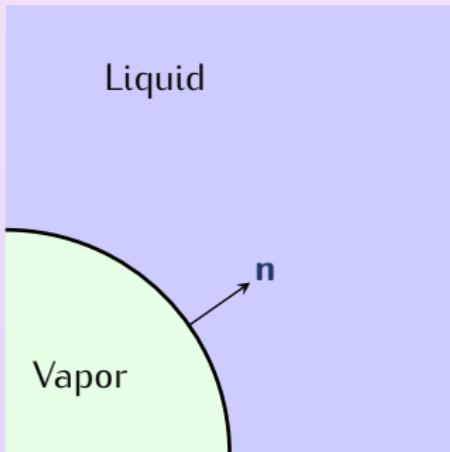
$$\mathfrak{G} \stackrel{\text{def}}{=} \frac{\tau^2}{2\gamma P} \left. \frac{\partial^2 P}{\partial \tau^2} \right|_s$$

- Regularity: [J. CORREIA, P.G. LEFLOCH, M.D. THANH]
- Loss of convexity: [A. Voss]

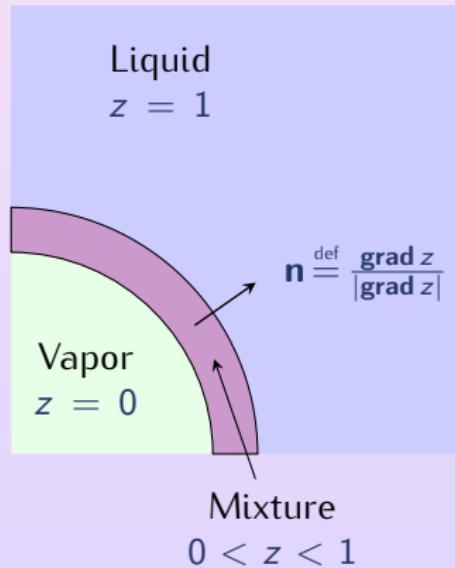
- Pure Phases
 - (H) $\gamma > 0$
 - (H) $\Gamma > 0$
 - (H) $\mathfrak{G} > 0$
- Mixture
 - (P) $\gamma > 0$
 - (P) $\Gamma > 0$
 - (H) $\mathfrak{G} > 0$

CONTINUUM SURFACE FORCE (CSF) APPROACH

Physical Interface



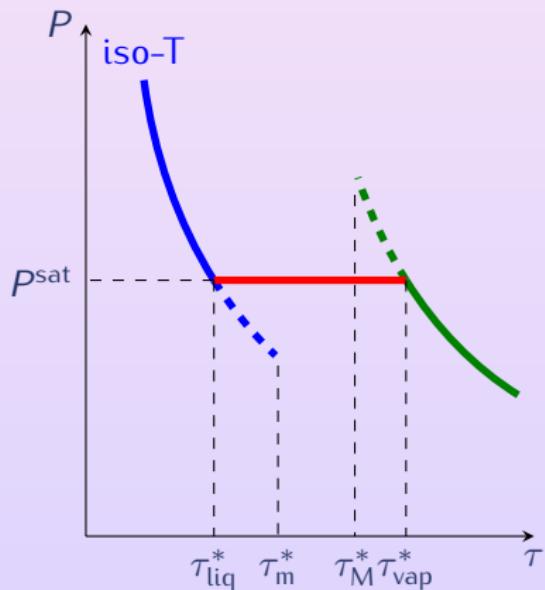
Diffuse Interface



$$\Pi_{\text{tension}} = -\sigma \operatorname{div}(\mathbf{n})\mathbf{n}$$

[J.U. BRACKBILL, D.B. KOTHE, C. ZEMACH]

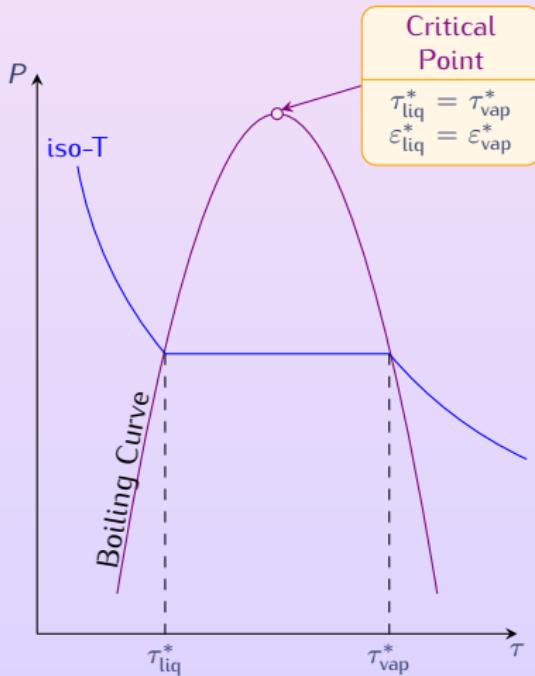
METASTABILITY



$$P^{\text{eq}} = \begin{cases} P_{\text{liq}}, & \text{if } \tau < \tau_{\text{liq}}^*, \\ P^{\text{sat}}, & \text{if } \tau_{\text{liq}}^* < \tau < \tau_{\text{vap}}^*, \\ P_{\text{vap}}, & \text{if } \tau_{\text{vap}}^* < \tau. \end{cases}$$

$$P^{\text{met}} = \begin{cases} P_{\text{liq}}, & \text{if } \tau < \tau_{\text{liq}}^*, \\ [P^{\text{sat}} \text{ or } P_{\text{liq}}], & \text{if } \tau_{\text{liq}}^* < \tau < \tau_m^*, \\ P^{\text{sat}}, & \text{if } \tau_m^* < \tau < \tau_M^*, \\ [P^{\text{sat}} \text{ or } P_{\text{vap}}], & \text{if } \tau_M^* < \tau < \tau_{\text{vap}}^*, \\ P_{\text{vap}}, & \text{if } \tau_{\text{vap}}^* < \tau, \end{cases}$$

CRITICAL POINT



Prinic

- 2 Pure Phases EOS $(\tau, \varepsilon) \mapsto P_\alpha$
- 1 Saturation EOS $\tau \mapsto P^{\text{sat}}$

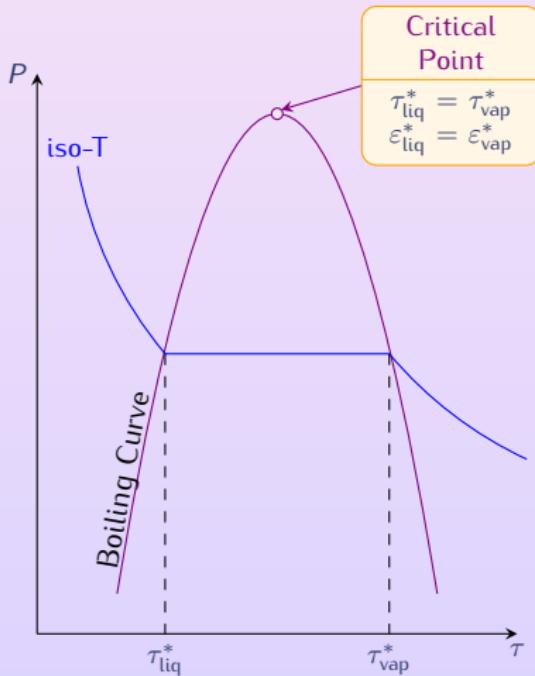
EOS

PG $\varepsilon_{liq}^* = \varepsilon_{vap}^* \Leftrightarrow c_{V_{liq}} = c_{V_{vap}}$ (indip. of T)

SG $\left\{ \tau_i, P_i^{\text{sat},e} \right\}_i \rightsquigarrow (\tau, \varepsilon) \mapsto P_\alpha \rightsquigarrow \tau \mapsto P^{\text{sat}}$

$\tau_{liq}^* = \tau_{vap}^*$ but $\varepsilon_{liq}^* \neq \varepsilon_{vap}^*$

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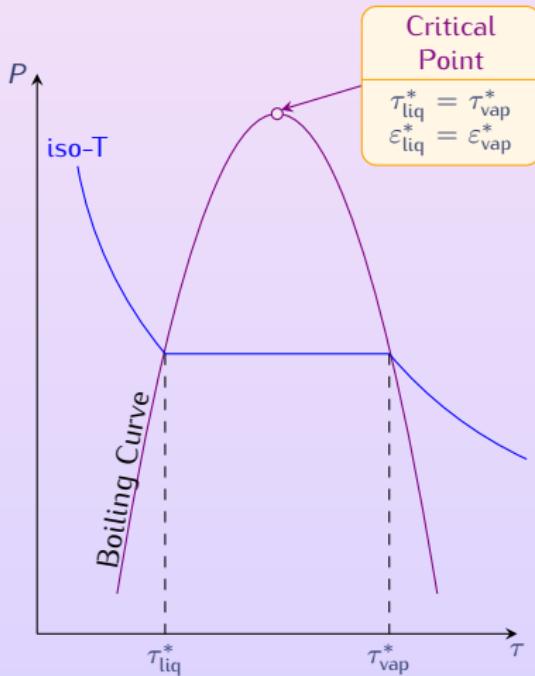
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EOS

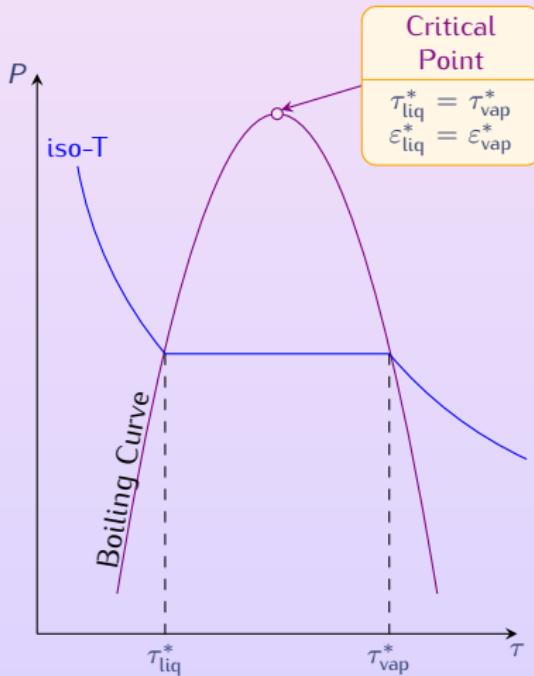
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SUMMARY

PHASE CHANGE EQUATION

$$\frac{\tau - \tau_{\text{vap}}^{\text{sat}}}{\tau_{\text{liq}}^{\text{sat}} - \tau_{\text{vap}}^{\text{sat}}} = \frac{\varepsilon - \varepsilon_{\text{vap}}^{\text{sat}}}{\varepsilon_{\text{liq}}^{\text{sat}} - \varepsilon_{\text{vap}}^{\text{sat}}}$$

with

$$T \mapsto \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(T) = \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}(T, P^{\text{sat}}(T))$$

or

$$P \mapsto \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(P) = \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}(T^{\text{sat}}(P), P)$$

SUMMARY

How to compute saturation functions τ_α^{sat} and $\varepsilon_\alpha^{\text{sat}}$

- **Analytical EOS:** we compute the saturation functions τ_α^{sat} and $\varepsilon_\alpha^{\text{sat}}$ by the **Coexistence Curve**:

- Exact: $T \mapsto P^{\text{sat}}(T)$ or $P \mapsto T^{\text{sat}}(P)$

$$\begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha^{\text{sat}}(P) = \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha(T^{\text{sat}}(P), P) \quad \text{e.g. Simplified Stiffened Gases}$$

- Approximated: $T \mapsto \hat{P}^{\text{sat}}(T) \approx P^{\text{sat}}(T)$

$$\begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha^{\text{sat}}(T) \approx \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha(T, \hat{P}^{\text{sat}}(T)) \quad \text{e.g. General Stiffened Gases}$$

- **Tabulated EOS:** the saturation functions τ_α^{sat} and $\varepsilon_\alpha^{\text{sat}}$ are given by experiments and we set

$$\begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha^{\text{sat}}(T \text{ or } P) \approx \begin{pmatrix} \hat{\tau} \\ \hat{\varepsilon} \end{pmatrix}_\alpha^{\text{sat}}(T \text{ or } P)$$

To Do

	EOS		Simulation		
	Pure Phases	Equilibrium	Cavitation	Boiling	Film
Virtual Fluid (SG)	✓	✓	✓	✓	①
Real Fluid (SG)	✓	✓	✓	②	③
Tabulated	④	✓	⑤	⑥	⑦