

# MODELLING AND SIMULATION OF LIQUID-VAPOR PHASE TRANSITION

A Boiling Crisis Study Contribution

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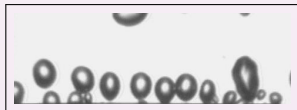


# BOILING CRISIS

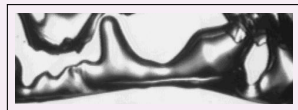
## PHENOMENON

Liquid phase heated by a wall at a fixed temperature  $T^{\text{wall}}$  (pool boiling).  
When  $T^{\text{wall}}$  increases, we switch from a **nucleate boiling** to a **film boiling**.

Nucleate Boiling



Film Boiling



source: [http://www.spaceflight.esa.int/users/fluids/TT\\_boiling.htm](http://www.spaceflight.esa.int/users/fluids/TT_boiling.htm)

# OUTLINE

- 1 Model
- 2 Numerical Method
- 3 Numerical Tests
- 4 Conclusion

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# EULER SYSTEM

$$\begin{cases} \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0, \\ \partial_t(\rho \mathbf{u}) + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = \mathfrak{V}_{\text{vf}} - \mathfrak{S}_{\text{sf}}, \\ \partial_t\left(\rho\left(\frac{|\mathbf{u}|^2}{2} + \varepsilon\right)\right) + \operatorname{div}\left(\rho\left(\frac{|\mathbf{u}|^2}{2} + \varepsilon\right)\mathbf{u} + P \mathbf{u}\right) = (\mathfrak{V}_{\text{vf}} - \mathfrak{S}_{\text{sf}}) \cdot \mathbf{u} - \operatorname{div}(\mathbf{q}). \end{cases}$$

- $(\mathbf{x}, t) \mapsto \rho$  specific density,
- $(\mathbf{x}, t) \mapsto \varepsilon$  specific internal energy,
- $(\mathbf{x}, t) \mapsto \mathbf{u}$  velocity;
- $(\rho, \varepsilon) \mapsto \mathfrak{V}_{\text{vf}}$  volumic forces,
- $(\rho, \varepsilon) \mapsto \mathfrak{S}_{\text{sf}}$  surface forces,
- $(\rho, \varepsilon) \mapsto \operatorname{div}(\mathbf{q})$  heat transfert.

$(\rho, \varepsilon) \mapsto P$  pressure law.

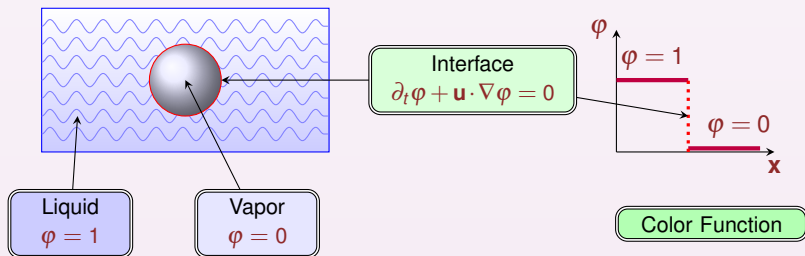
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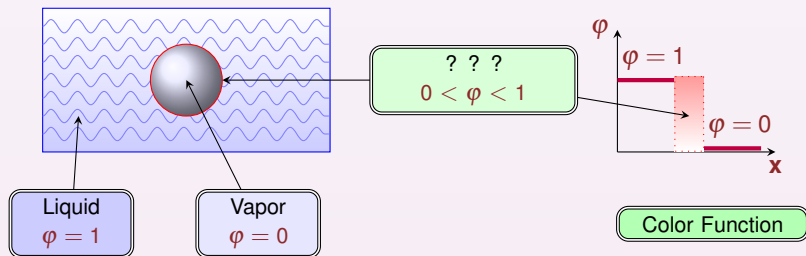
$(\rho, \varepsilon) \mapsto P$  pressure law.

# LIQUID-VAPOR INTERFACE



$$(\rho, \varepsilon) \mapsto P = \begin{cases} P^{\text{liq}} & \text{if } \varphi = 1; \\ P^{\text{vap}} & \text{if } \varphi = 0. \end{cases}$$

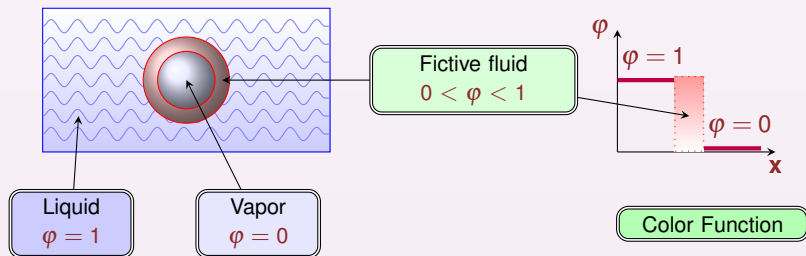
## LIQUID-VAPOR INTERFACE



$$(\rho, \varepsilon) \mapsto P = \begin{cases} P^{\text{liq}} & \text{if } \varphi = 1; \\ ??? & \text{if } 0 < \varphi < 1; \\ P^{\text{vap}} & \text{if } \varphi = 0. \end{cases}$$

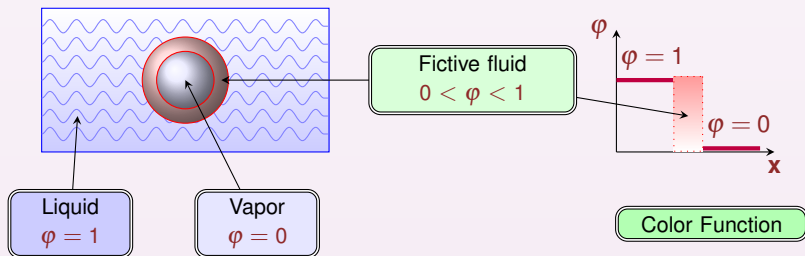


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# LIQUID-VAPOR INTERFACE



➡ Goal: define a global pressure law such that

- $(\rho, \varepsilon, \mathbf{u}, P)$  are continuous (3 zones)
- the interface position and the phase change are implicit ( $\leadsto$   ~~$\phi$~~ )
- coherence with classical thermodynamics [H. Callen]

## EOS OF EACH PHASE $\alpha = 1, 2$

$$\left. \begin{array}{l} \tau_\alpha \text{ specific volume} \\ \varepsilon_\alpha \text{ specific internal energy} \end{array} \right\} \Rightarrow \mathbf{w}_\alpha \stackrel{\text{def}}{=} (\tau_\alpha, \varepsilon_\alpha);$$

$\mathbf{w}_\alpha \mapsto s_\alpha$  specific entropy (Hessian matrix neg. def.);

$$\left. \begin{array}{l} \left. \begin{array}{l} T_\alpha \stackrel{\text{def}}{=} \left( \frac{\partial s_\alpha}{\partial \varepsilon_\alpha} \Big|_{\tau_\alpha} \right)^{-1} > 0 \\ P_\alpha \stackrel{\text{def}}{=} T_\alpha \frac{\partial s_\alpha}{\partial \tau_\alpha} \Big|_{\varepsilon_\alpha} > 0 \\ g_\alpha \stackrel{\text{def}}{=} \varepsilon_\alpha + P_\alpha \tau_\alpha - T_\alpha s_\alpha \end{array} \right\} \begin{array}{l} \text{temperature,} \\ \text{pressure,} \\ \text{free enthalpy (Gibbs potential).} \end{array} \end{array} \right\}$$

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# EOS WITHOUT PHASE CHANGE

- $\mathbf{w} \stackrel{\text{def}}{=} y\mathbf{w}_1 + (1 - y)\mathbf{w}_2;$
- $y$  mass fraction;
- $z$  volume fraction s.t.  $y\tau_1 = z\tau;$
- $\psi$  energy fraction s.t.  $y\varepsilon_1 = \psi\varepsilon.$

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## ENTROPY WITHOUT PHASE CHANGE

$$\sigma \stackrel{\text{def}}{=} ys_1(\mathbf{w}_1) + (1 - y)s_2(\mathbf{w}_2) = ys_1\left(\frac{z}{y}\tau, \frac{\psi}{y}\varepsilon\right) + (1 - y)s_2\left(\frac{1-z}{1-y}\tau, \frac{1-\psi}{1-y}\varepsilon\right)$$

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# EOS WITH PHASE CHANGE

## ENTROPY WITHOUT PH.CH.

$$(\mathbf{w}, z, y, \psi) \mapsto \sigma$$



## ENTROPY AT EQUILIBRIUM

$$\mathbf{w} \mapsto s^{\text{eq}}$$

### DEFINITION [H. CALLEN, PH. HELLUY ...]

Optimization Problem:

$$s^{\text{eq}}(\mathbf{w}) \stackrel{\text{def}}{=} \max_{z, y, \psi \in [0, 1]^3} \sigma(\mathbf{w}, z, y, \psi)$$

Optimality Condition: 
$$\begin{cases} T_1(z, y, \psi) = T_2(z, y, \psi) \\ P_1(z, y, \psi) = P_2(z, y, \psi) \\ g_1(z, y, \psi) = g_2(z, y, \psi) \\ z, y, \psi \in ]0, 1[^3 \end{cases}$$

Solution:  $(z^*, y^*, \psi^*)$

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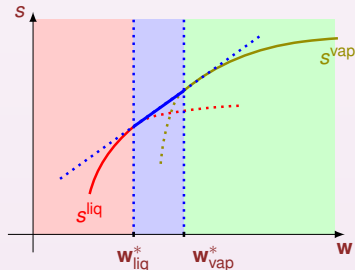
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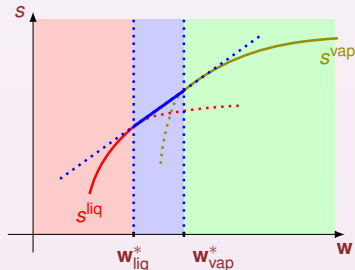
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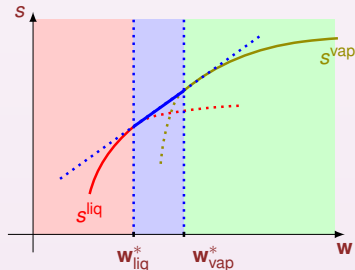
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# DYNAMIC LIQUID-VAPOR PHASE CHANGE

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## PROPERTIES [G. ALLAIRE, G. FACCANONI, S. KOKH]

If  $\tau_1^* \neq \tau_2^*$  and  $\varepsilon_1^* \neq \varepsilon_2^*$  (first order phase transition) then

$$\textcircled{1} c(w) > 0, \quad \textcircled{2} s_{\tau\varepsilon}^{\text{eq}}(w) > 0$$

- ① Euler system: strict hyperbolicity ( $\neq$  p-system),
- ② Riemann problem: multitude of entropic (Lax) solutions [R. Menikoff, B. J. Plohr], uniqueness of Liu solution.

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# HOW TO SIMULATE THE LIU SOLUTION

- Exact Riemann Solver [A. Voß]
- Viscuous Solver (the Liu solution is the only solution that has a viscuous profile) [S. Jaouen]
- Solver(s) based on **Relaxation Approach** [F. Coquel, B. Perthame], [Th. Barberon, Ph. Helluy], [Ph. Helluy, N. Seguin], [F. Coquel, F. Caro, D. Jamet, S. Kokh], ...

# RELAXATION APPROACH

$$\partial_t \mathbf{U} + \operatorname{div} \mathbf{F}(\mathbf{U}) = \mathbf{0}$$

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$$\partial_t \mathbf{V} + \operatorname{div} \mathbf{G}(\mathbf{V}) = \frac{1}{\mu} \mathbf{R}(\mathbf{V}) \quad \xrightarrow[\mu \rightarrow 0]{\text{Formally}} \quad \partial_t \mathbf{U} + \operatorname{div} \mathbf{F}(\mathbf{U}) = \mathbf{0}$$

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$$P^{\text{eq}}(\rho, \varepsilon) = \frac{S_\tau^{\text{eq}}}{S_\varepsilon^{\text{eq}}}, \quad e \stackrel{\text{def}}{=} \frac{|\mathbf{u}|^2}{2} + \varepsilon$$

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$$P(\rho, \varepsilon, z, y, \psi) = \frac{\sigma_\tau}{\sigma_\varepsilon}$$

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In the interface

$$\begin{cases} \partial_t z + \mathbf{u} \cdot \operatorname{grad} z = \\ \partial_t y + \mathbf{u} \cdot \operatorname{grad} y = \\ \partial_t \psi + \mathbf{u} \cdot \operatorname{grad} \psi = \end{cases}$$

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$$\begin{cases} \partial_t z + \mathbf{u} \cdot \operatorname{grad} z = \frac{1}{\mu_z} \left( \frac{P_2}{T_2} - \frac{P_1}{T_1} \right) \\ \partial_t y + \mathbf{u} \cdot \operatorname{grad} y = \frac{1}{\mu_y} \left( \frac{g_1}{T_1} - \frac{g_2}{T_2} \right) \frac{1}{\rho} \\ \partial_t \psi + \mathbf{u} \cdot \operatorname{grad} \psi = \frac{1}{\mu_\psi} \left( \frac{1}{T_1} - \frac{1}{T_2} \right) \varepsilon \end{cases}$$

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$$\xrightarrow[\mu_j \rightarrow 0]{\text{Formally}}$$

## EQUILIBRIUM SYSTEM

$$\begin{cases} \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0 \\ \partial_t(\rho \mathbf{u}) + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t(\rho e) + \operatorname{div}((\rho e + P^{\text{eq}}) \mathbf{u}) = 0 \end{cases}$$

$$P^{\text{eq}}(\rho, \varepsilon) = \frac{\mathbf{S}_\tau^{\text{eq}}}{\mathbf{S}_\varepsilon^{\text{eq}}}, \quad e \stackrel{\text{def}}{=} \frac{|\mathbf{u}|^2}{2} + \varepsilon$$



# RELAXATION APPROACH

$$\partial_t \mathbf{V} + \operatorname{div} \mathbf{G}(\mathbf{V}) = \frac{1}{\mu} \mathbf{R}(\mathbf{V}) \quad \xrightarrow[\mu \rightarrow 0]{\text{Formally}} \quad \partial_t \mathbf{U} + \operatorname{div} \mathbf{F}(\mathbf{U}) = \mathbf{0}$$

## AUGMENTED SYSTEM

$$\begin{cases} \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0 \\ \partial_t(\rho \mathbf{u}) + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = 0 \\ \partial_t(\rho e) + \operatorname{div}((\rho e + P) \mathbf{u}) = 0 \end{cases}$$

In the interface

$$\begin{cases} \partial_t z + \mathbf{u} \cdot \operatorname{grad} z = \frac{1}{\mu_z} \left( \frac{P_2}{T_2} - \frac{P_1}{T_1} \right) \\ \partial_t y + \mathbf{u} \cdot \operatorname{grad} y = \frac{1}{\mu_y} \left( \frac{g_1}{T_1} - \frac{g_2}{T_2} \right) \frac{1}{\rho} \\ \partial_t \psi + \mathbf{u} \cdot \operatorname{grad} \psi = \frac{1}{\mu_\psi} \left( \frac{1}{T_1} - \frac{1}{T_2} \right) \varepsilon \end{cases}$$

$$P(\rho, \varepsilon, z, y, \psi) = \frac{\sigma_\tau}{\sigma_\varepsilon}$$

Formally  
 $\mu_j \rightarrow 0$

## EQUILIBRIUM SYSTEM

$$\begin{cases} \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0 \\ \partial_t(\rho \mathbf{u}) + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t(\rho e) + \operatorname{div}((\rho e + P^{\text{eq}}) \mathbf{u}) = 0 \end{cases}$$

$$P^{\text{eq}}(\rho, \varepsilon) = \frac{s_\tau^{\text{eq}}}{s_\varepsilon^{\text{eq}}}, \quad e \stackrel{\text{def}}{=} \frac{|\mathbf{u}|^2}{2} + \varepsilon$$

REMARK:  ~~$\partial_t \psi + \mathbf{u} \cdot \operatorname{grad} \psi = 0$~~   $\rightsquigarrow T_1 = T_2$ .

# NUMERICAL SCHEME

$$\partial_t \mathbf{V} + \text{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V}) + \frac{1}{\mu} \mathbf{R}(\mathbf{V})$$

 $\mathbf{V}_i^n$ 

$\ominus \mu_j = +\infty$



$\partial_t \mathbf{V} + \text{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V})$

Aug. System: 5-eq. iso-T  
 Num. Scheme: op. splitting  
 Conv.: [G. Allaire and all.]  
 Surf. Tens.: [J. U. Brackbill and all.]  
 Heat: 2D implicit

 $\mathbf{V}_i^{n+1}$ 

$\oplus \mu_j = 0$



$\mathbf{R}(\mathbf{V}) = \mathbf{0}$

update fractions  
 $(y, z, \psi)$  by  
 projecting  $\mathbf{V}_i^{n+1/2}$   
 onto the  
 $P, T, g$  equilibrium

# NUMERICAL SCHEME

$$\partial_t \mathbf{V} + \text{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V}) + \frac{1}{\mu} \mathbf{R}(\mathbf{V})$$

 $\mathbf{V}_i^n$ 

$$\textcircled{1} \mu_j = +\infty$$



$$\partial_t \mathbf{V} + \text{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V})$$

Aug. System: 5-eq. iso-T  
 Num. Scheme: op. splitting  
 Conv.: [G. Allaire and all.]  
 Surf. Tens.: [J. U. Brackbill and all.]  
 Heat: 2D implicit

$$\textcircled{2} \mu_j = 0$$



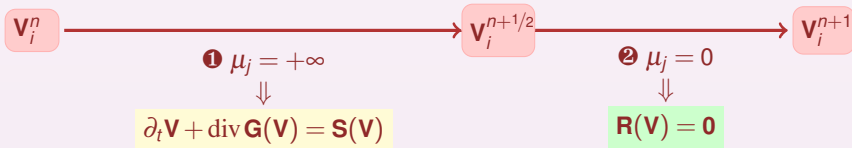
$$\mathbf{R}(\mathbf{V}) = \mathbf{0}$$

update fractions  
 ( $y, z, \psi$ ) by  
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 onto the  
 $P, T, g$  equilibrium

 $\mathbf{V}_i^{n+1}$

# NUMERICAL SCHEME

$$\partial_t \mathbf{V} + \text{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V}) + \frac{1}{\mu} \mathbf{R}(\mathbf{V})$$

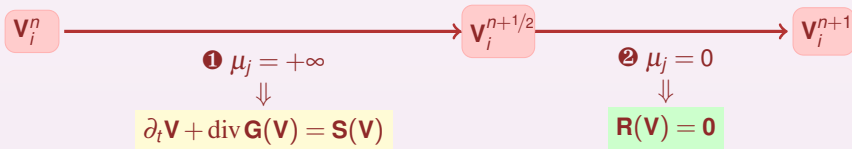


Aug. System: 5-eq. iso-T  
 Num. Scheme: op. splitting  
 Conv.: [G. Allaire and all.]  
 Surf. Tens.: [J. U. Brackbill and all.]  
 Heat: 2D implicit

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# NUMERICAL SCHEME

$$\partial_t \mathbf{V} + \text{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V}) + \frac{1}{\mu} \mathbf{R}(\mathbf{V})$$

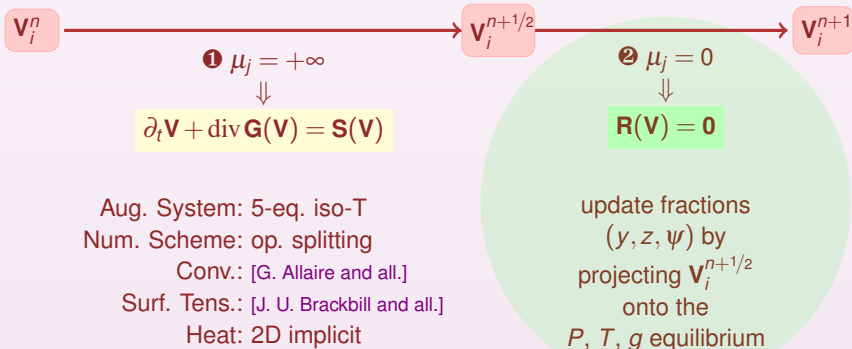


Aug. System: 5-eq. iso-T  
 Num. Scheme: op. splitting  
 Conv.: [G. Allaire and all.]  
 Surf. Tens.: [J. U. Brackbill and all.]  
 Heat: 2D implicit

update fractions  
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# NUMERICAL SCHEME

$$\partial_t \mathbf{V} + \text{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V}) + \frac{1}{\mu} \mathbf{R}(\mathbf{V})$$



## ANALYTICAL EOS

▶▶ Water Example

 $(\tau, \varepsilon)$  fixed $(\tau_1, \varepsilon_1, \tau_2, \varepsilon_2, y)$  SOLUTION OF

$$\begin{cases} g_1(\tau_1, \varepsilon_1) = g_2(\tau_2, \varepsilon_2) \\ P_1(\tau_1, \varepsilon_1) = P_2(\tau_2, \varepsilon_2) \\ T_1(\tau_1, \varepsilon_1) = T_2(\tau_2, \varepsilon_2) \\ \tau = y\tau_1 + (1-y)\tau_2 \\ \varepsilon = y\varepsilon_1 + (1-y)\varepsilon_2 \end{cases}$$

 $(P, T)$  SOLUTION OF

$$\begin{cases} g_1(P, T) = g_2(P, T) \\ \frac{\tau - \tau_2(P, T)}{\tau_1(P, T) - \tau_2(P, T)} = \frac{\varepsilon - \varepsilon_2(P, T)}{\varepsilon_1(P, T) - \varepsilon_2(P, T)} \end{cases}$$

$$T \mapsto P = P^{\text{sat}}(T) \approx P^{\text{sat}}(T)$$

 $T$  SOLUTION OF

$$\frac{\tau - \tau_2^{\text{sat}}(T)}{\tau_1^{\text{sat}}(T) - \tau_2^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_2^{\text{sat}}(T)}{\varepsilon_1^{\text{sat}}(T) - \varepsilon_2^{\text{sat}}(T)} \quad \text{where} \quad \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(T) \stackrel{\text{def}}{=} \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}(P^{\text{sat}}(T), T)$$

## ANALYTICAL EOS

▶▶ Water Example

 $(\tau, \varepsilon)$  fixed $(\tau_1, \varepsilon_1, \tau_2, \varepsilon_2, y)$  SOLUTION OF

$$\begin{cases} g_1(\tau_1, \varepsilon_1) = g_2(\tau_2, \varepsilon_2) \\ P_1(\tau_1, \varepsilon_1) = P_2(\tau_2, \varepsilon_2) \\ T_1(\tau_1, \varepsilon_1) = T_2(\tau_2, \varepsilon_2) \\ \tau = y\tau_1 + (1-y)\tau_2 \\ \varepsilon = y\varepsilon_1 + (1-y)\varepsilon_2 \end{cases}$$

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## ANALYTICAL EOS

▶▶ Water Example

 $(\tau, \varepsilon)$  fixed $(\tau_1, \varepsilon_1, \tau_2, \varepsilon_2, y)$  SOLUTION OF

$$\begin{cases} g_1(\tau_1, \varepsilon_1) = g_2(\tau_2, \varepsilon_2) \\ P_1(\tau_1, \varepsilon_1) = P_2(\tau_2, \varepsilon_2) \\ T_1(\tau_1, \varepsilon_1) = T_2(\tau_2, \varepsilon_2) \\ \tau = y\tau_1 + (1-y)\tau_2 \\ \varepsilon = y\varepsilon_1 + (1-y)\varepsilon_2 \end{cases}$$

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## ANALYTICAL EOS

▶▶ Water Example

 $(\tau, \varepsilon)$  fixed $(\tau_1, \varepsilon_1, \tau_2, \varepsilon_2, y)$  SOLUTION OF

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 $(P, T)$  SOLUTION OF

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$$\frac{\tau - \tau_2^{\text{sat}}(T)}{\tau_1^{\text{sat}}(T) - \tau_2^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_2^{\text{sat}}(T)}{\varepsilon_1^{\text{sat}}(T) - \varepsilon_2^{\text{sat}}(T)} \quad \text{where} \quad \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(T) \stackrel{\text{def}}{=} \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}(P^{\text{sat}}(T), T)$$

## ANALYTICAL EOS

▶ Water Example

 $(\tau, \varepsilon)$  fixed $(\tau_1, \varepsilon_1, \tau_2, \varepsilon_2, y)$  SOLUTION OF

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 $(P, T)$  SOLUTION OF

$$\begin{cases} g_1(P, T) = g_2(P, T) \\ \frac{\tau - \tau_2(P, T)}{\tau_1(P, T) - \tau_2(P, T)} = \frac{\varepsilon - \varepsilon_2(P, T)}{\varepsilon_1(P, T) - \varepsilon_2(P, T)} \end{cases}$$

least square approximation

$$T \mapsto P = \hat{P}^{\text{sat}}(T) \approx P^{\text{sat}}(T)$$

 $T$  SOLUTION OF

$$\frac{\tau - \tau_2^{\text{sat}}(T)}{\tau_1^{\text{sat}}(T) - \tau_2^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_2^{\text{sat}}(T)}{\varepsilon_1^{\text{sat}}(T) - \varepsilon_2^{\text{sat}}(T)} \quad \text{where} \quad \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(T) \stackrel{\text{def}}{=} \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}(\hat{P}^{\text{sat}}(T), T)$$

## TABULATED EOS

» Water Examples

 $(\tau, \varepsilon)$  fixed**T SOLUTION OF**

$$\frac{\tau - \tau_2^{\text{sat}}(T)}{\tau_1^{\text{sat}}(T) - \tau_2^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_2^{\text{sat}}(T)}{\varepsilon_1^{\text{sat}}(T) - \varepsilon_2^{\text{sat}}(T)} \quad \text{with} \quad \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(T) \quad \text{tabulated}$$

}}

$$\frac{\tau - \widehat{\tau}_2^{\text{sat}}(T)}{\widehat{\tau}_1^{\text{sat}}(T) - \widehat{\tau}_2^{\text{sat}}(T)} = \frac{\varepsilon - \widehat{\varepsilon}_2^{\text{sat}}(T)}{\widehat{\varepsilon}_1^{\text{sat}}(T) - \widehat{\varepsilon}_2^{\text{sat}}(T)} \quad \text{with} \quad \begin{pmatrix} \widehat{\tau} \\ \widehat{\varepsilon} \end{pmatrix}_{\alpha}^{\text{sat}}(T)$$

# TABULATED EOS

» Water Examples

$(\tau, \varepsilon)$  fixed

**T SOLUTION OF**

$$\frac{\tau - \tau_2^{\text{sat}}(T)}{\tau_1^{\text{sat}}(T) - \tau_2^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_2^{\text{sat}}(T)}{\varepsilon_1^{\text{sat}}(T) - \varepsilon_2^{\text{sat}}(T)}$$

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$$\frac{\tau - \widehat{\tau}_2^{\text{sat}}(T)}{\widehat{\tau}_1^{\text{sat}}(T) - \widehat{\tau}_2^{\text{sat}}(T)} = \frac{\varepsilon - \widehat{\varepsilon}_2^{\text{sat}}(T)}{\widehat{\varepsilon}_1^{\text{sat}}(T) - \widehat{\varepsilon}_2^{\text{sat}}(T)}$$

with  $\begin{pmatrix} \widehat{\tau} \\ \widehat{\varepsilon} \end{pmatrix}_{\alpha}^{\text{sat}}(T)$

}}

least square approximations

## TABULATED EOS

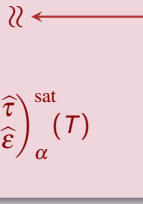
» Water Examples

 $(\tau, \varepsilon)$  fixed**T SOLUTION OF**

$$\frac{\tau - \tau_2^{\text{sat}}(T)}{\tau_1^{\text{sat}}(T) - \tau_2^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_2^{\text{sat}}(T)}{\varepsilon_1^{\text{sat}}(T) - \varepsilon_2^{\text{sat}}(T)}$$

with  $\begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(T)$  tabulated

$$\frac{\tau - \widehat{\tau}_2^{\text{sat}}(T)}{\widehat{\tau}_1^{\text{sat}}(T) - \widehat{\tau}_2^{\text{sat}}(T)} = \frac{\varepsilon - \widehat{\varepsilon}_2^{\text{sat}}(T)}{\widehat{\varepsilon}_1^{\text{sat}}(T) - \widehat{\varepsilon}_2^{\text{sat}}(T)}$$

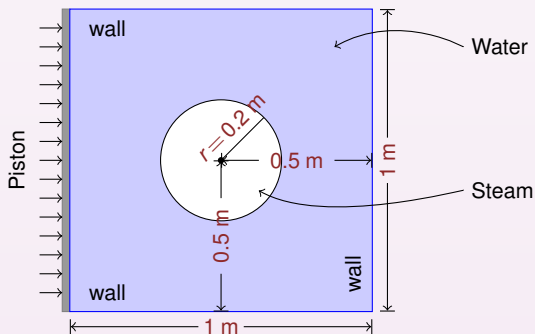
with  $\begin{pmatrix} \widehat{\tau} \\ \widehat{\varepsilon} \end{pmatrix}_{\alpha}^{\text{sat}}(T)$ 

least square approximations

# OUTLINE

- 1 Model
- 2 Numerical Method
- 3 Numerical Tests**
- 4 Conclusion

# COMPRESSION OF A VAPOR BUBBLE

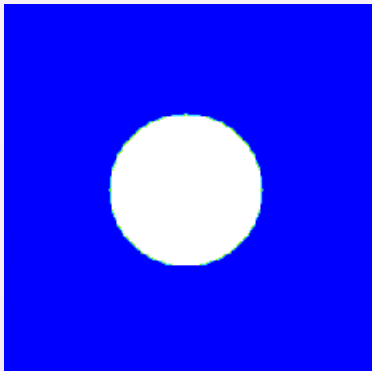
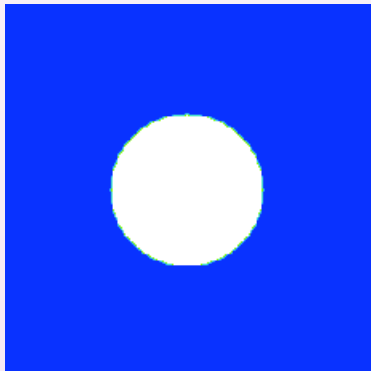


Compression of a 2D Vapor Bubble involving two Stiffened Gases for water and steam.

The piston moves towards right at constant speed  $u_p = 30$  m/s.



## COMPRESSION OF A VAPOR BUBBLE

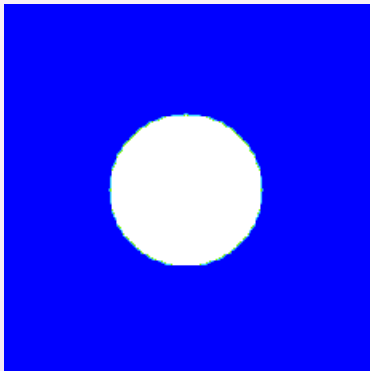
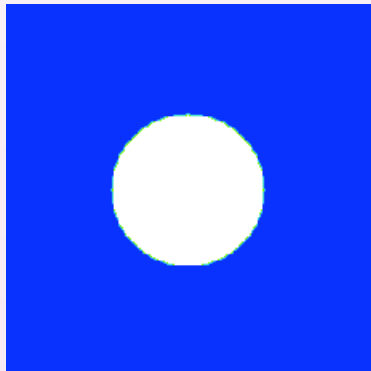
Mass Fraction  $y$ Density  $\rho$  $t = 0.00$  ms

◀ Geometry

▶ Play

▶▶ Skip

## COMPRESSION OF A VAPOR BUBBLE

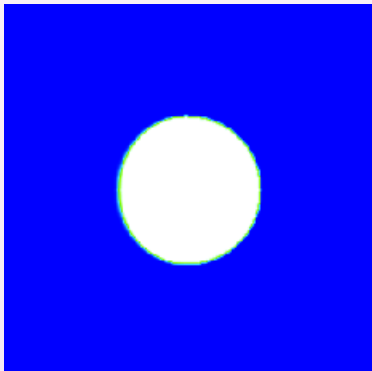
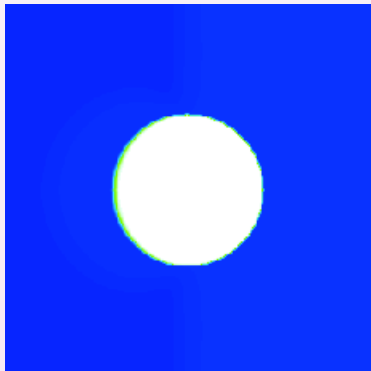
Mass Fraction  $y$ Density  $\rho$  $t = 0.00$  ms

◀ Geometry

▶ Play

▶▶ Skip

## COMPRESSION OF A VAPOR BUBBLE

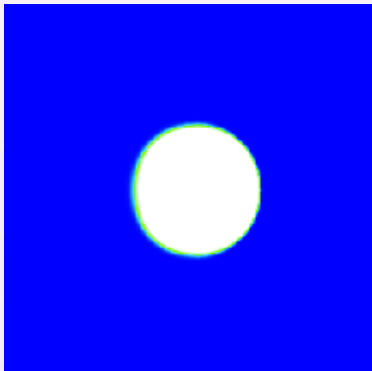
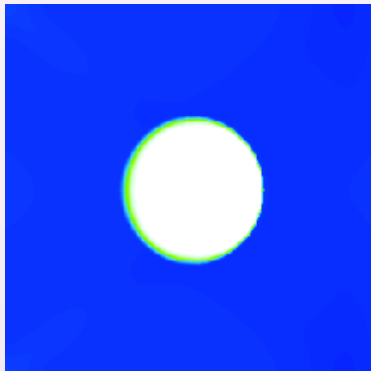
Mass Fraction  $y$ Density  $\rho$  $t = 0.89$  ms

◀ Geometry

▶ Play

▶▶ Skip

## COMPRESSION OF A VAPOR BUBBLE

Mass Fraction  $y$ Density  $\rho$  $t = 1.49 \text{ ms}$ 

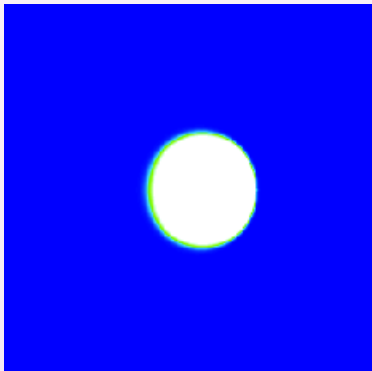
◀ Geometry

▶ Play

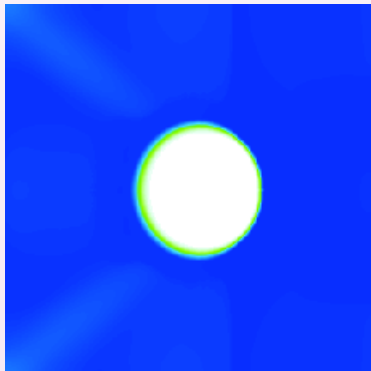
▶▶ Skip

# COMPRESSION OF A VAPOR BUBBLE

Mass Fraction  $y$



Density  $\rho$



$t = 2.09$  ms

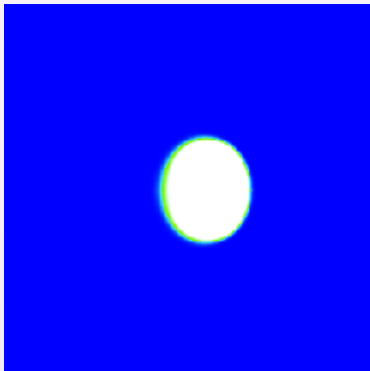
◀ Geometry

▶ Play

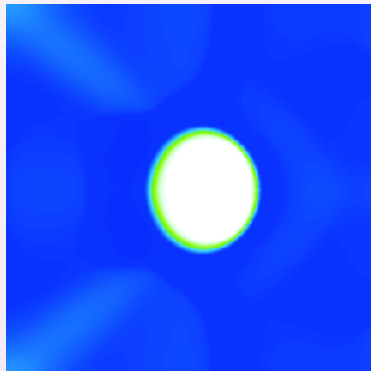
▶▶ Skip

# COMPRESSION OF A VAPOR BUBBLE

Mass Fraction  $y$



Density  $\rho$



$t = 2.69$  ms

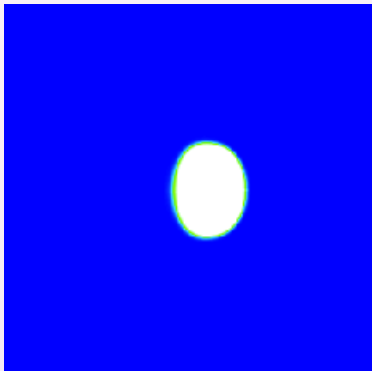
◀ Geometry

▶ Play

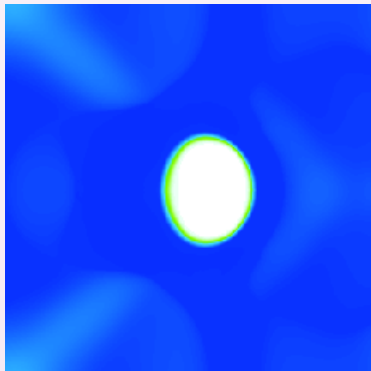
▶▶ Skip

# COMPRESSION OF A VAPOR BUBBLE

Mass Fraction  $y$



Density  $\rho$



$t = 3.30$  ms

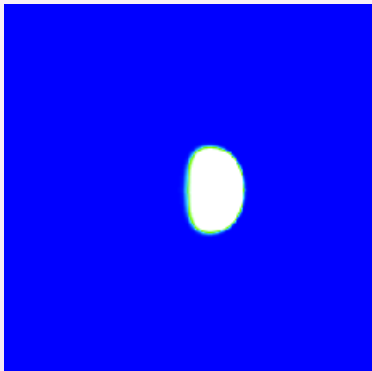
◀ Geometry

▶ Play

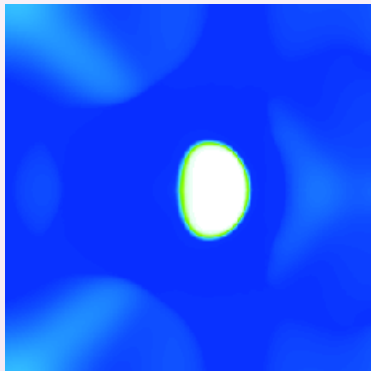
▶▶ Skip

# COMPRESSION OF A VAPOR BUBBLE

Mass Fraction  $y$



Density  $\rho$



$t = 3.60$  ms

◀ Geometry

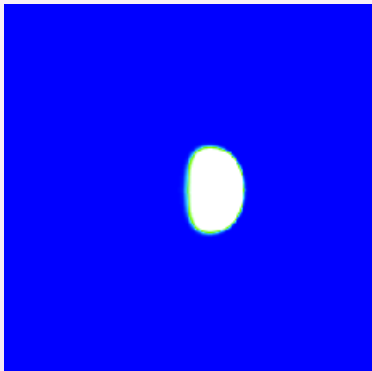
▶ Play

▶▶ Skip

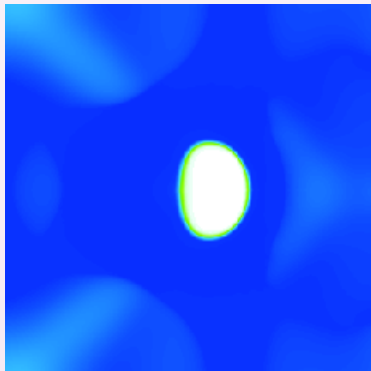


# COMPRESSION OF A VAPOR BUBBLE

Mass Fraction  $y$



Density  $\rho$



$t = 3.60$  ms

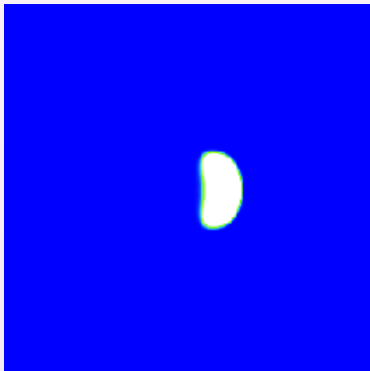
◀ Geometry

▶ Play

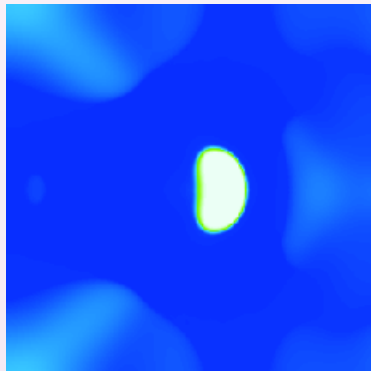
▶▶ Skip

# COMPRESSION OF A VAPOR BUBBLE

Mass Fraction  $y$



Density  $\rho$



$t = ?$  ms

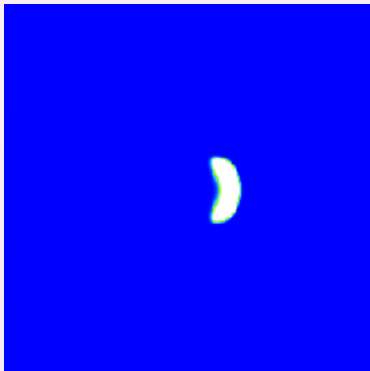
◀ Geometry

▶ Play

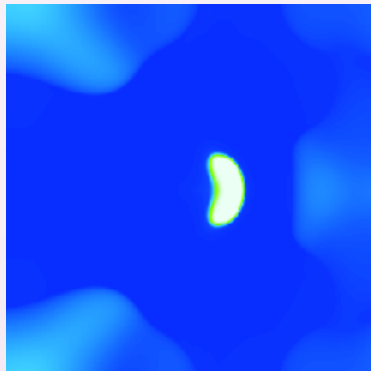
▶▶ Skip

# COMPRESSION OF A VAPOR BUBBLE

Mass Fraction  $y$



Density  $\rho$



$t = ?$  ms

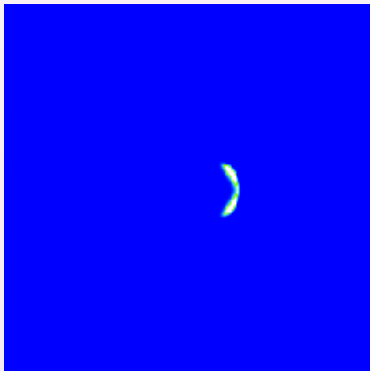
◀ Geometry

▶ Play

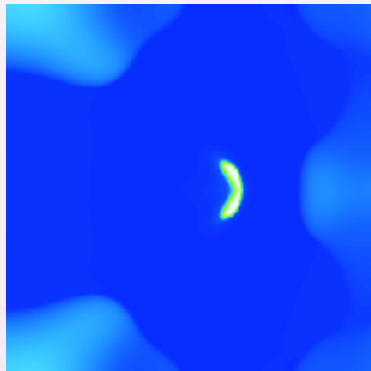
▶▶ Skip

# COMPRESSION OF A VAPOR BUBBLE

Mass Fraction  $y$



Density  $\rho$



$t = ?$  ms

◀ Geometry

▶ Play

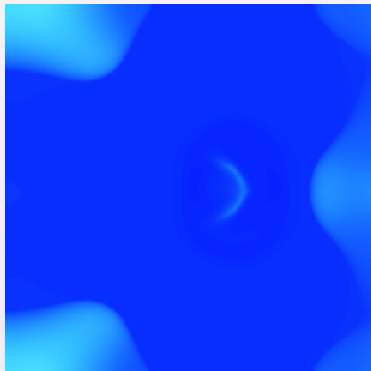
▶▶ Skip

# COMPRESSION OF A VAPOR BUBBLE

Mass Fraction  $y$



Density  $\rho$



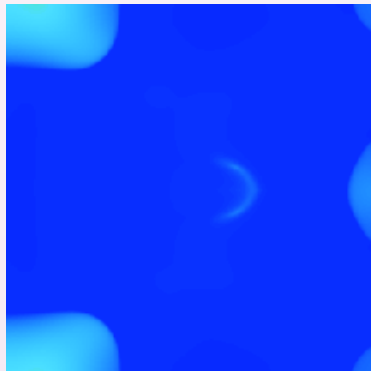
$t = ?$  ms

◀ Geometry

▶ Play

▶▶ Skip

## COMPRESSION OF A VAPOR BUBBLE

Mass Fraction  $y$ Density  $\rho$  $t = ?$  ms

◀ Geometry

▶ Play

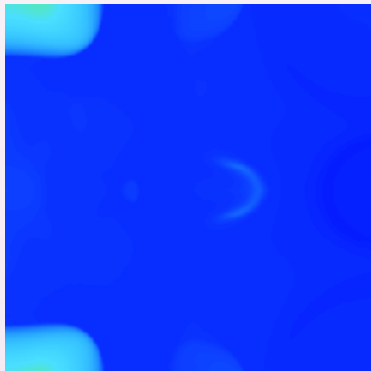
▶▶ Skip

# COMPRESSION OF A VAPOR BUBBLE

Mass Fraction  $y$



Density  $\rho$



$t = ?$  ms

◀ Geometry

▶ Play

▶▶ Skip

# COMPRESSION OF A VAPOR BUBBLE

Mass Fraction  $y$



Density  $\rho$



$t = ?$  ms

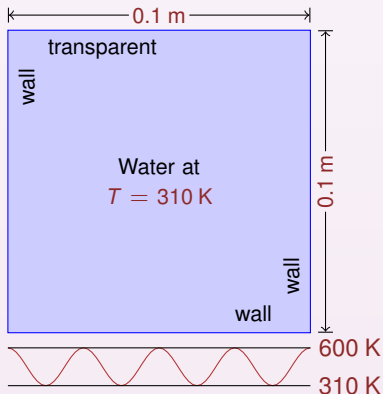
◀ Geometry

▶ Play

▶▶ Skip



# NUCLEATING BUBBLES

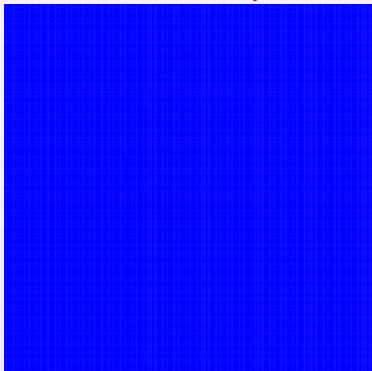


Nucleation of a 2D Vapor Bubbles involving two Stiffened Gases for water and steam. The temperature of the south wall is fixed at

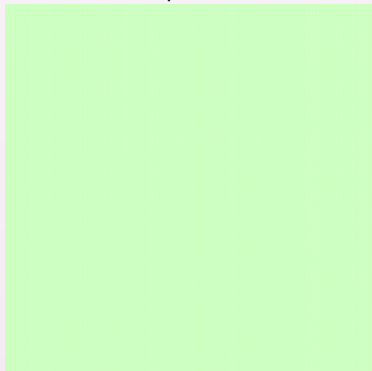
$$T^{\text{wall}} = 310 + (600 - 310)(1 + \cos(6\pi x))/2.$$

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



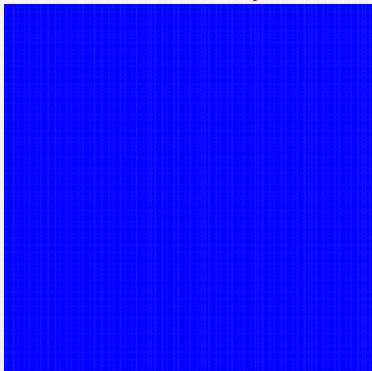
◀ Geometry

▶ Play

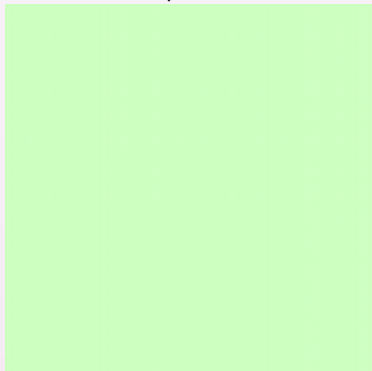
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



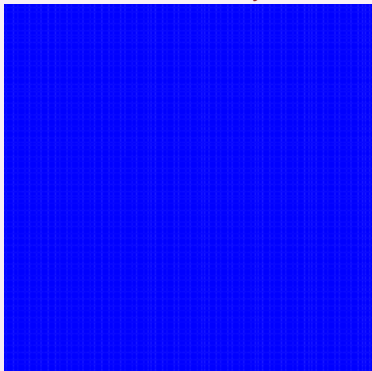
◀ Geometry

▶ Play

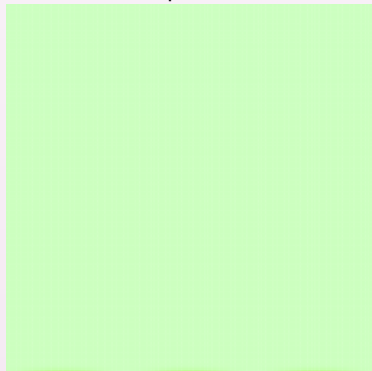
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



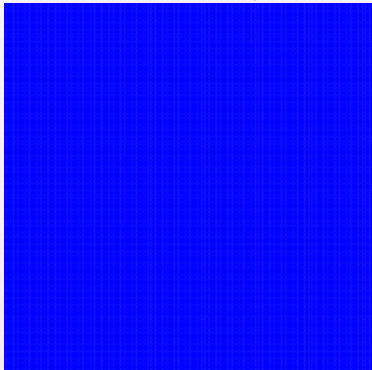
◀ Geometry

▶ Play

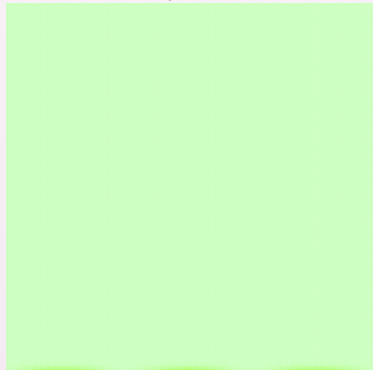
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



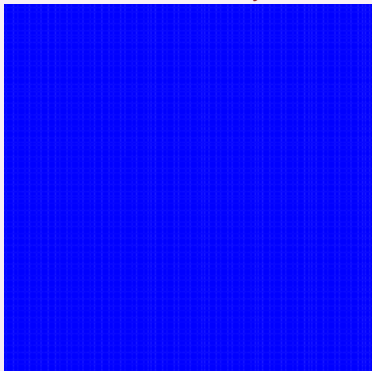
◀ Geometry

▶ Play

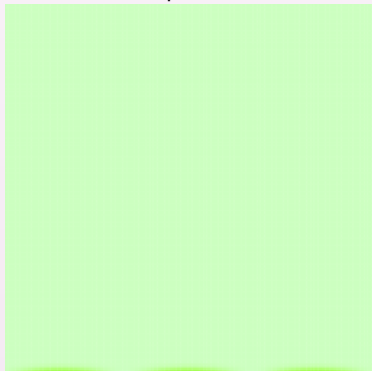
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



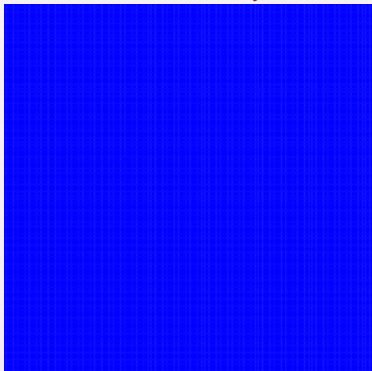
◀ Geometry

▶ Play

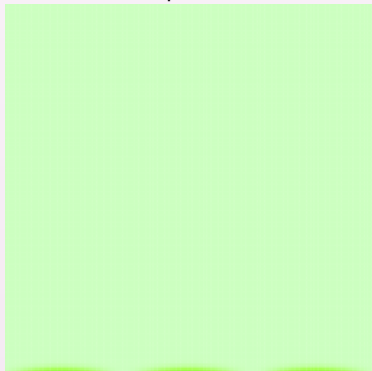
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



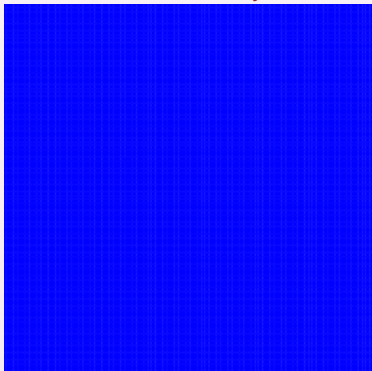
◀ Geometry

▶ Play

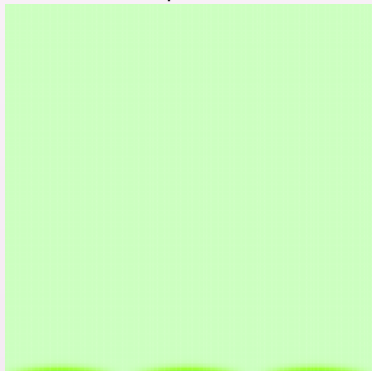
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



◀ Geometry

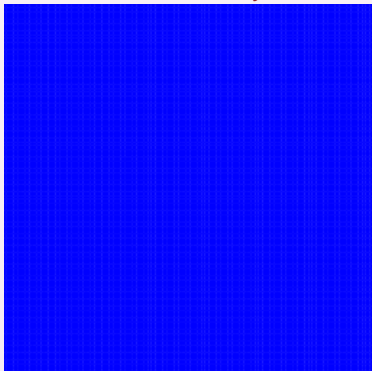
▶ Play

▶▶ Skip

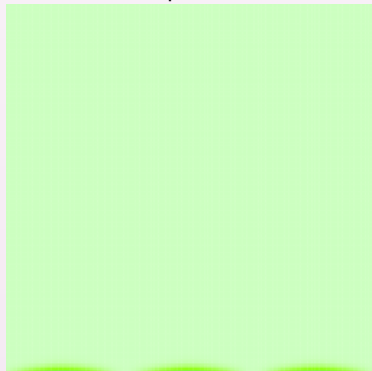


# NUCLEATING BUBBLES

Mass Fraction  $y$



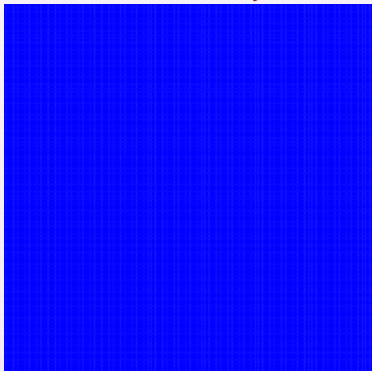
Temperature  $T$



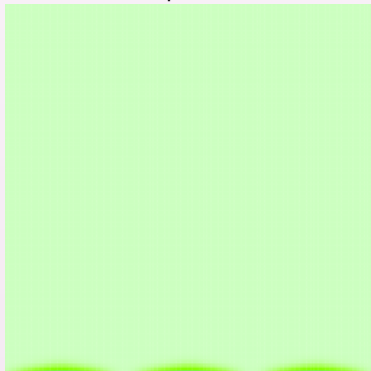
◀ Geometry ▶ Play ▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



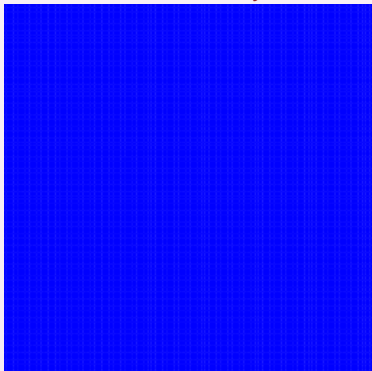
◀ Geometry

▶ Play

▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



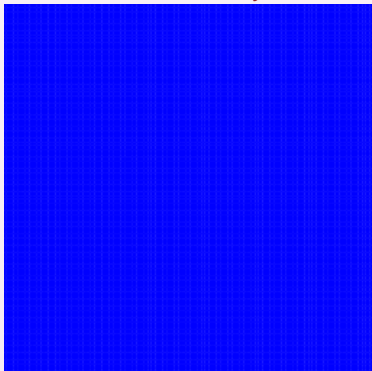
◀ Geometry

▶ Play

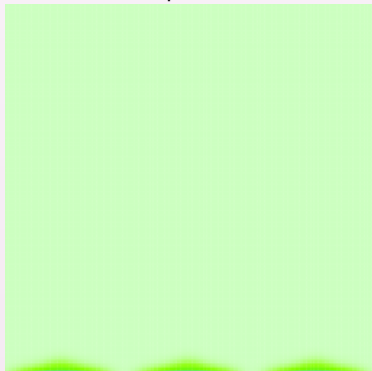
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



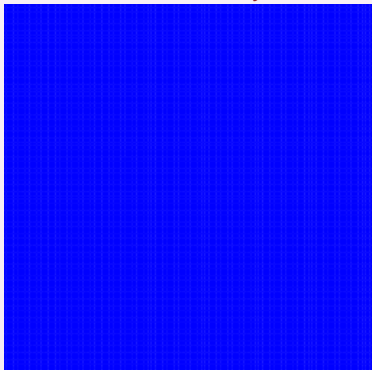
◀ Geometry

▶ Play

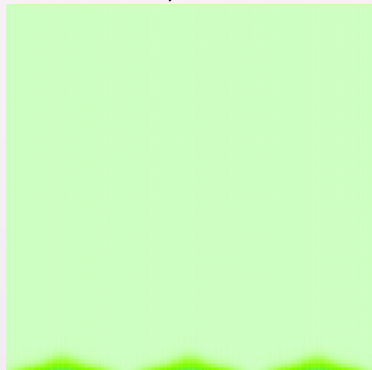
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



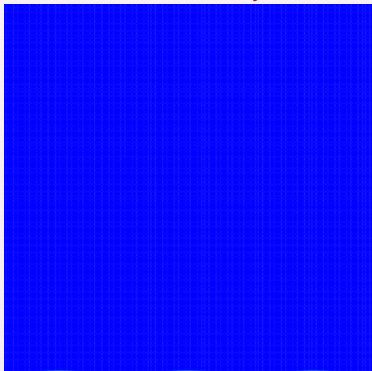
◀ Geometry

▶ Play

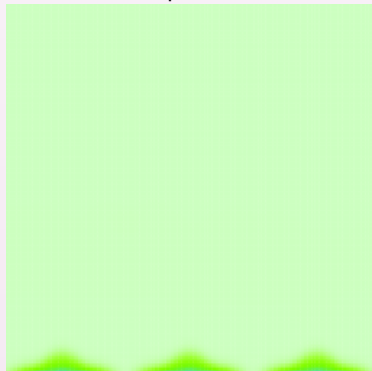
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



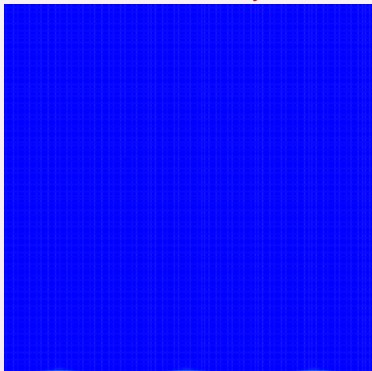
◀ Geometry

▶ Play

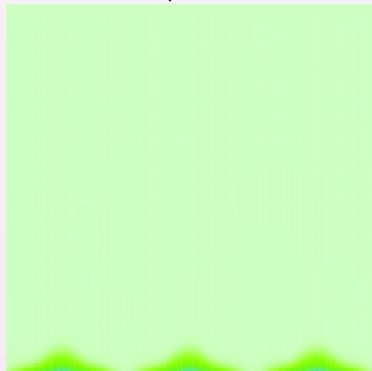
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



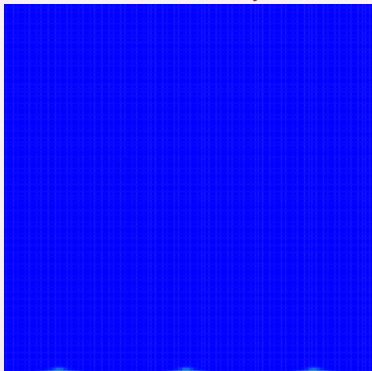
◀ Geometry

▶ Play

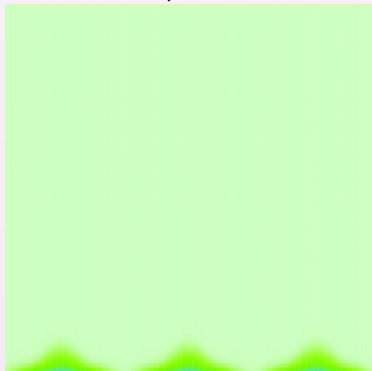
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



◀ Geometry

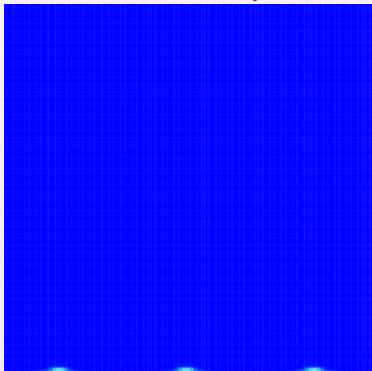
▶ Play

▶▶ Skip

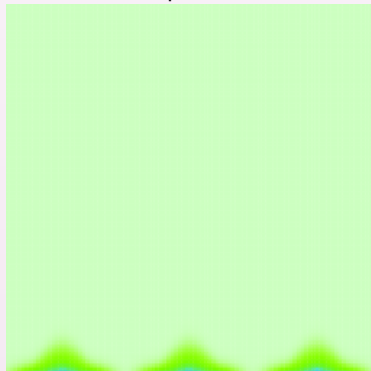


# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



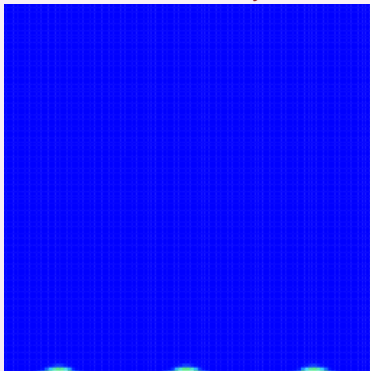
◀ Geometry

▶ Play

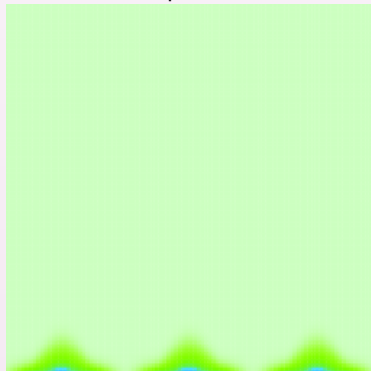
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



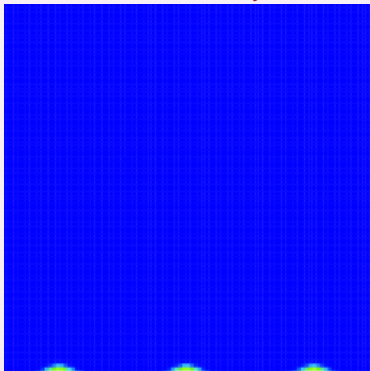
◀ Geometry

▶ Play

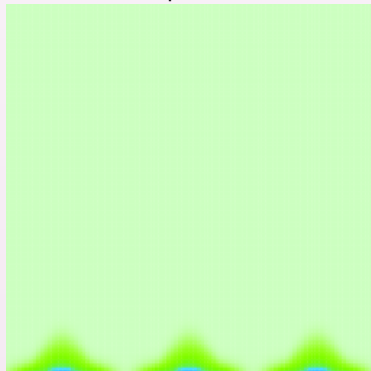
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



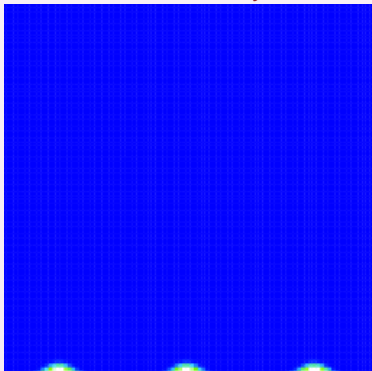
◀ Geometry

▶ Play

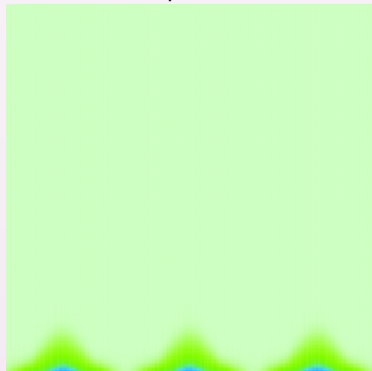
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



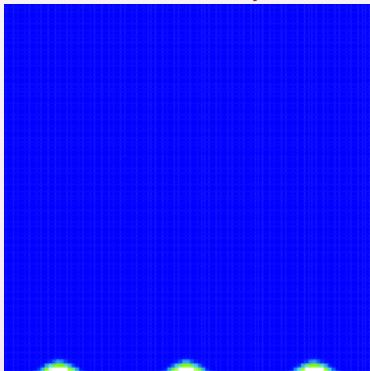
◀ Geometry

▶ Play

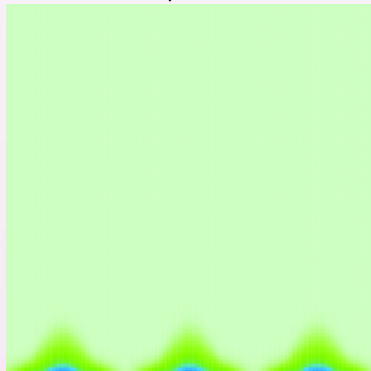
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# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



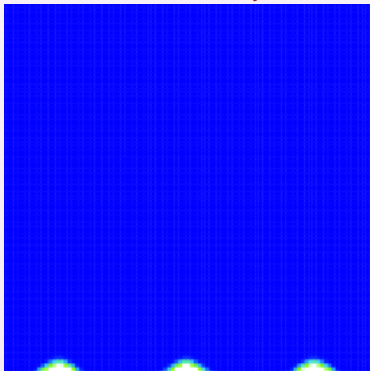
◀ Geometry

▶ Play

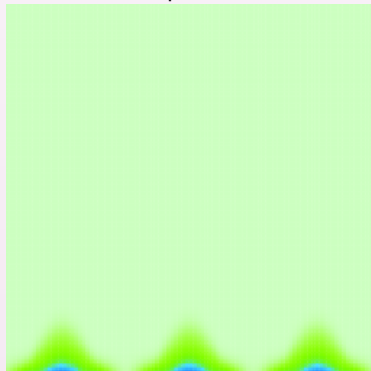
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



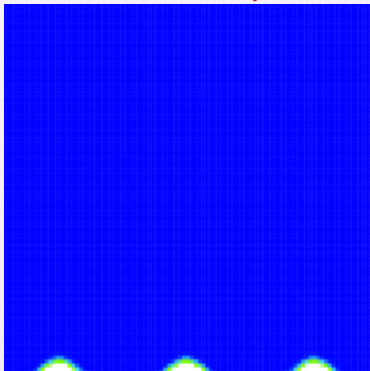
◀ Geometry

▶ Play

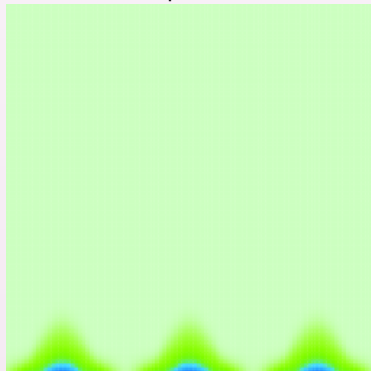
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# NUCLEATING BUBBLES

Mass Fraction  $y$



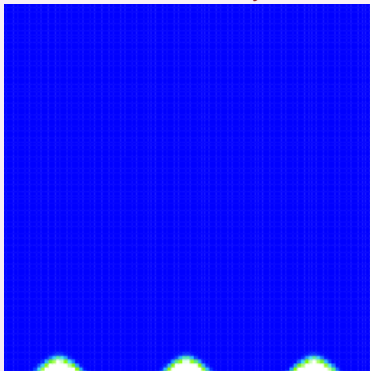
Temperature  $T$



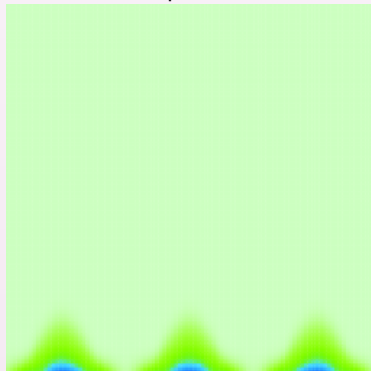
◀ Geometry ▶ Play ▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



◀ Geometry

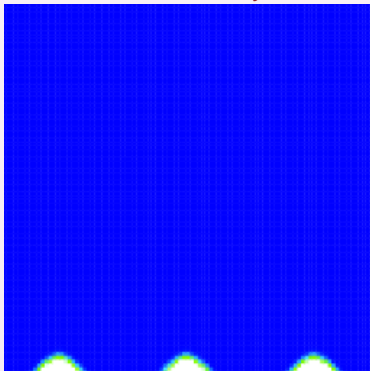
▶ Play

▶▶ Skip

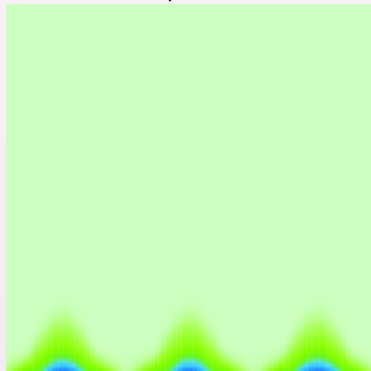


# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



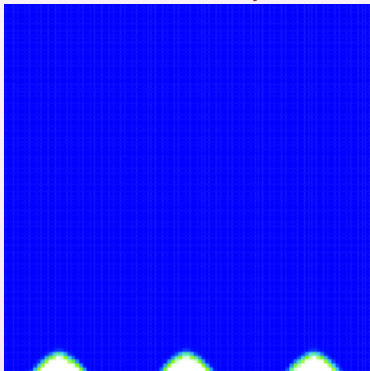
◀ Geometry

▶ Play

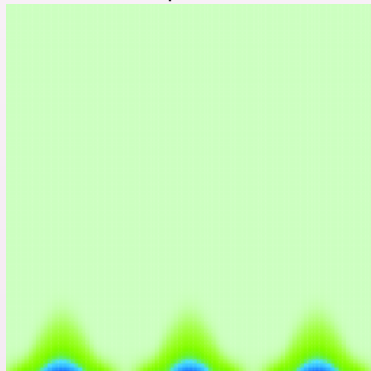
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



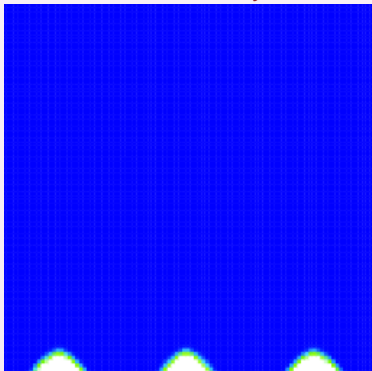
◀ Geometry

▶ Play

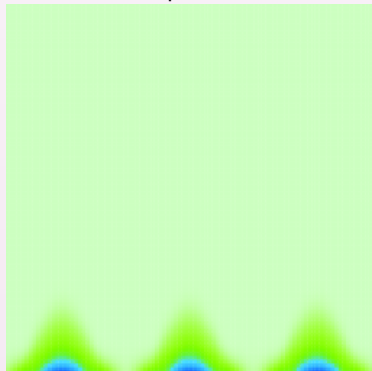
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



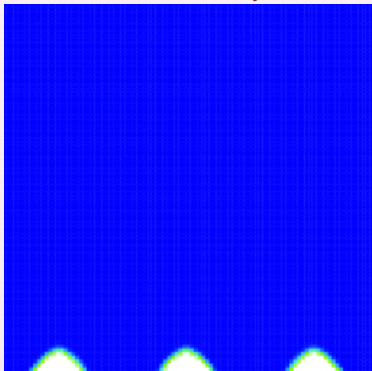
◀ Geometry

▶ Play

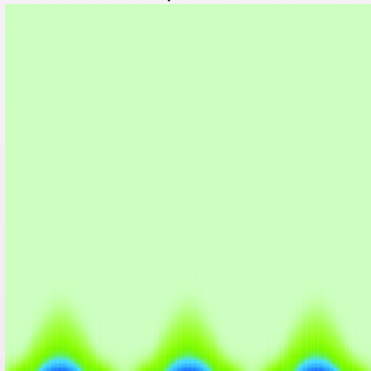
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



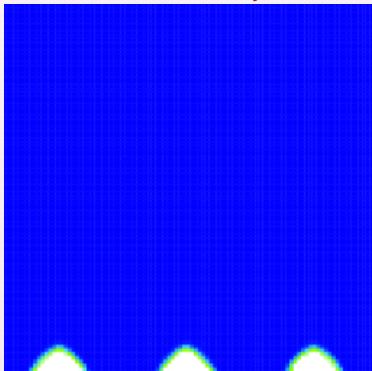
Temperature  $T$



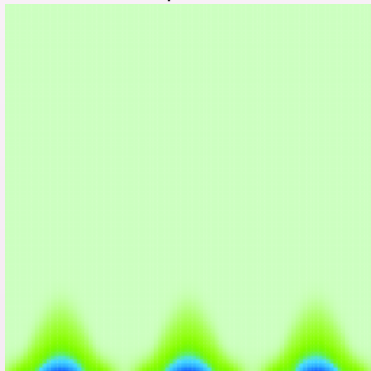
◀ Geometry ▶ Play ▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



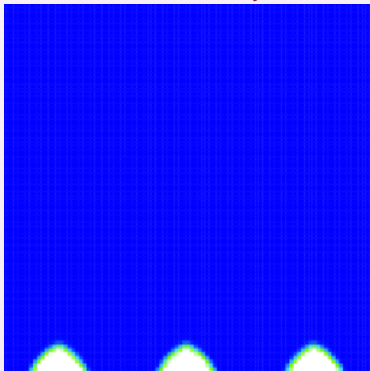
◀ Geometry

▶ Play

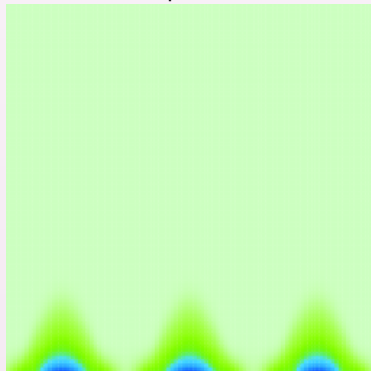
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



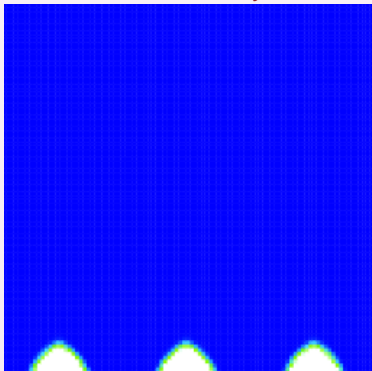
◀ Geometry

▶ Play

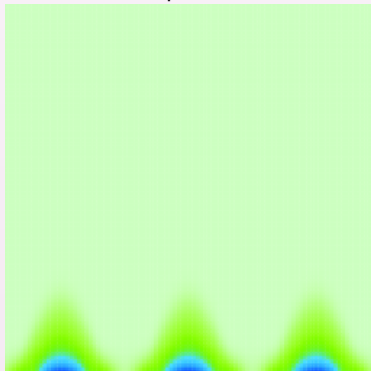
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# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



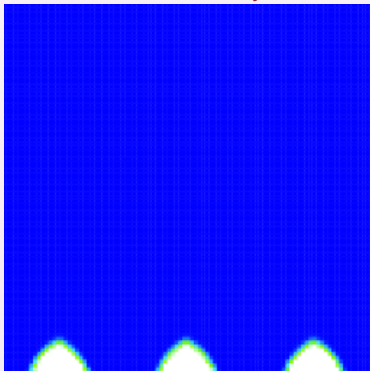
◀ Geometry

▶ Play

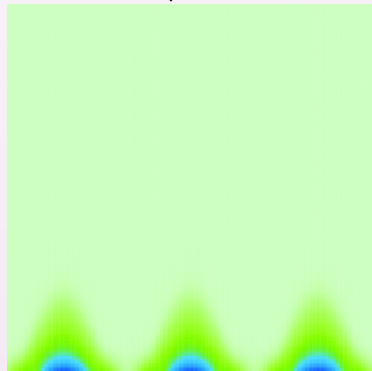
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



◀ Geometry

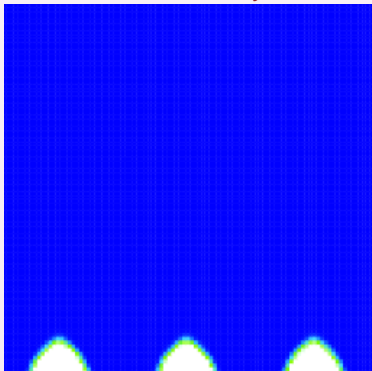
▶ Play

▶▶ Skip

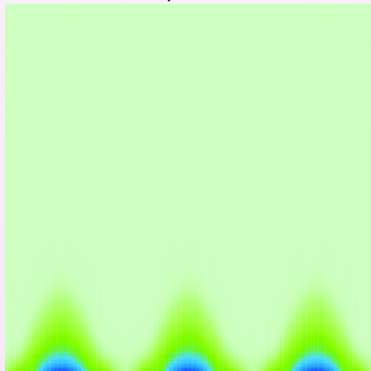


# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



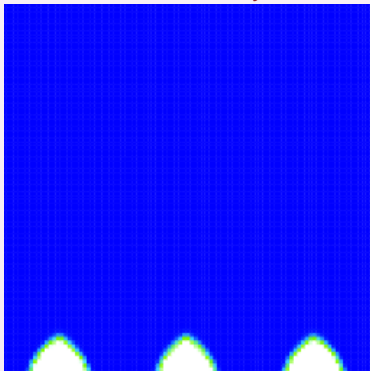
◀ Geometry

▶ Play

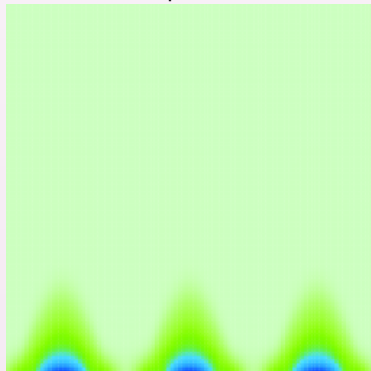
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



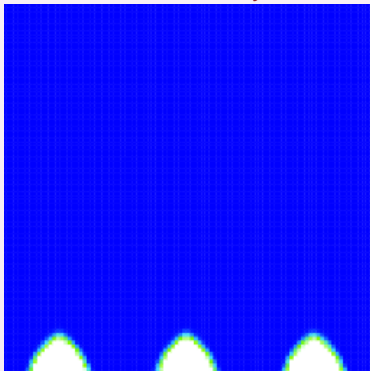
◀ Geometry

▶ Play

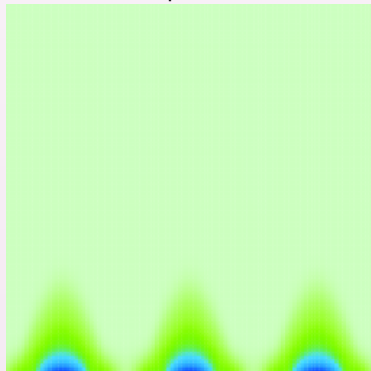
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



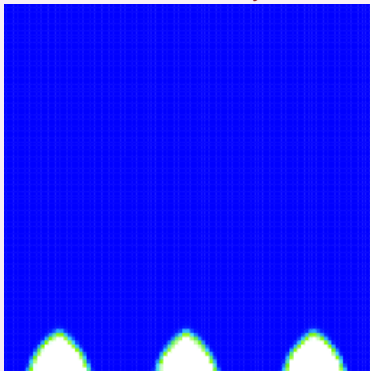
◀ Geometry

▶ Play

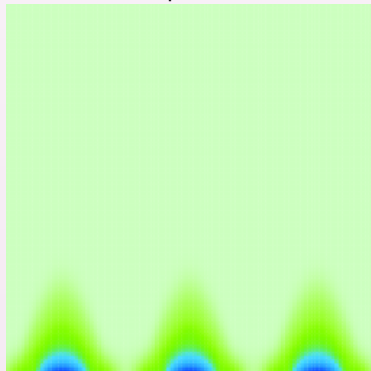
▶▶ Skip

# NUCLEATING BUBBLES

Mass Fraction  $y$



Temperature  $T$



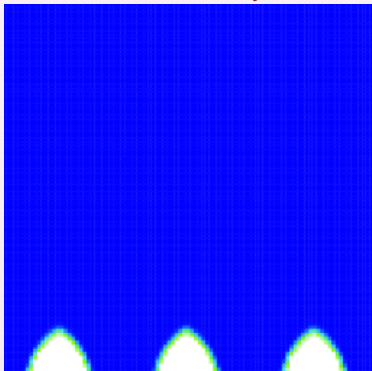
◀ Geometry

▶ Play

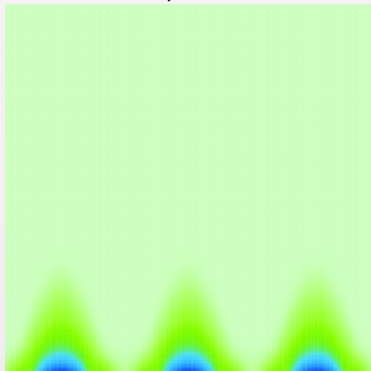
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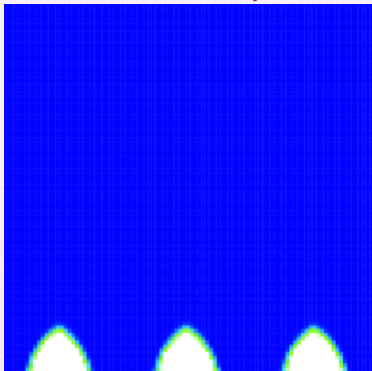
◀ Geometry

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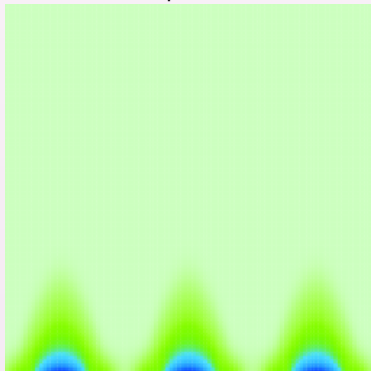
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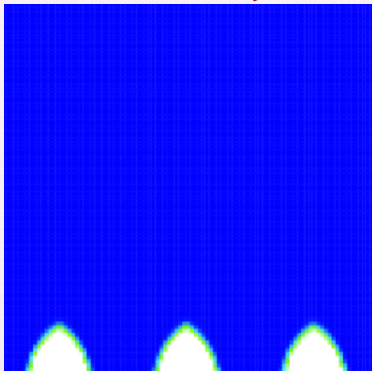
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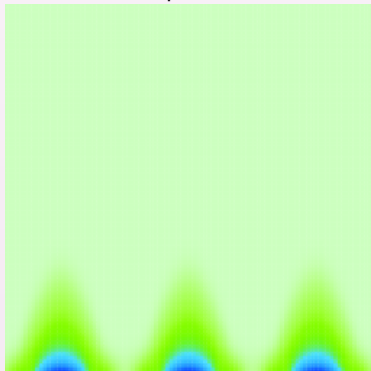
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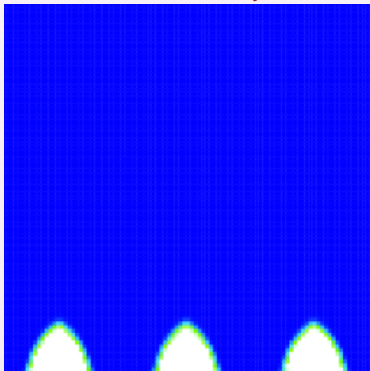
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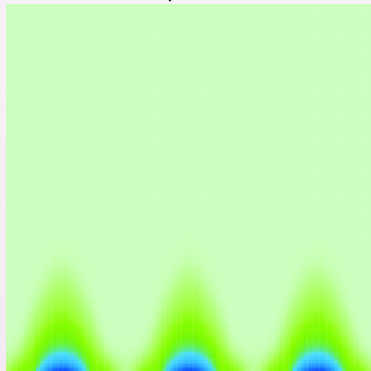
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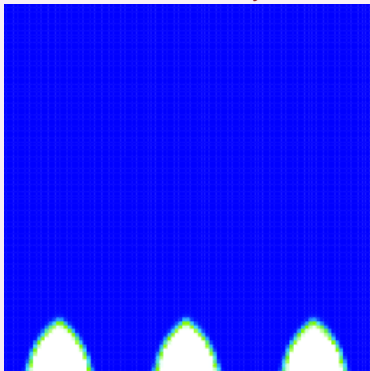
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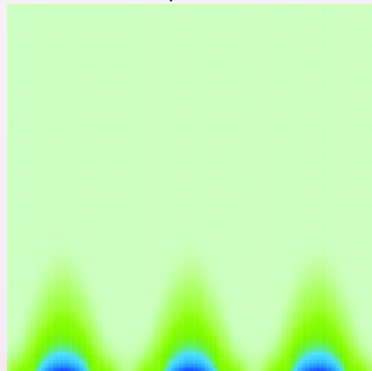


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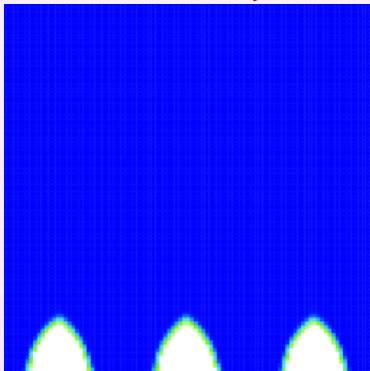
◀ Geometry

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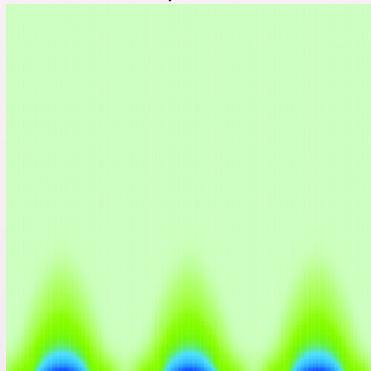
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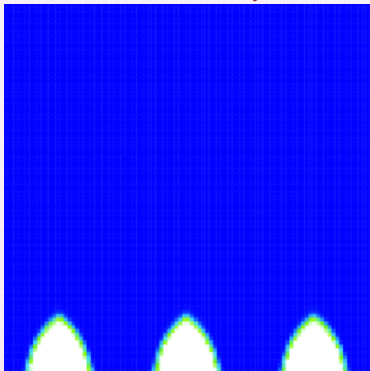
◀ Geometry

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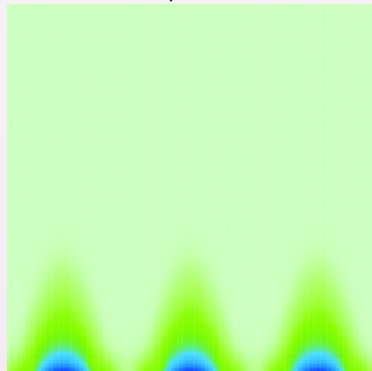
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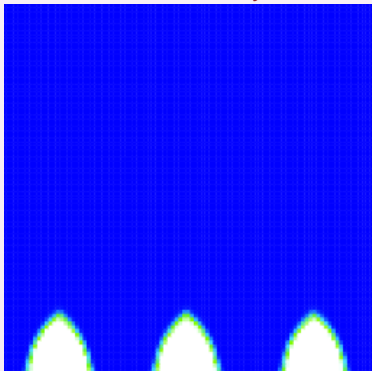
◀ Geometry

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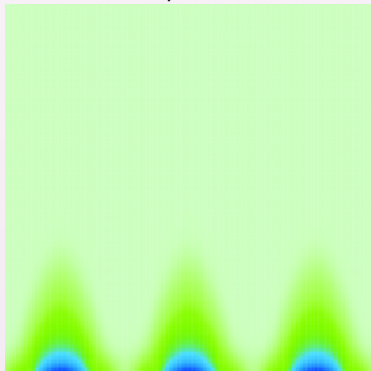
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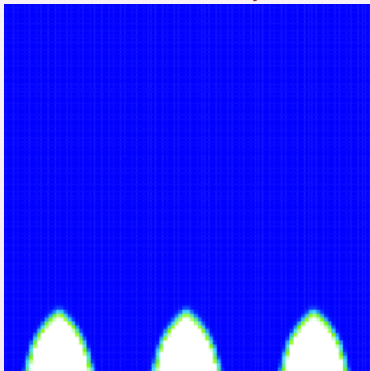
◀ Geometry

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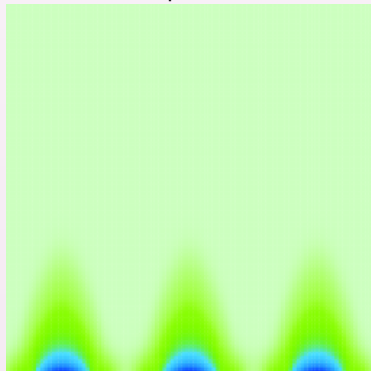
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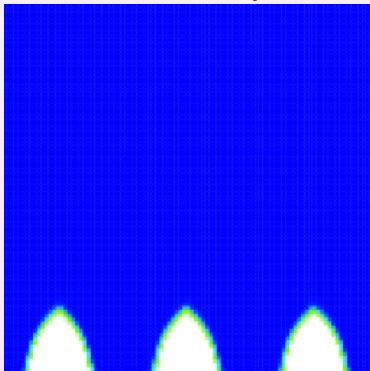
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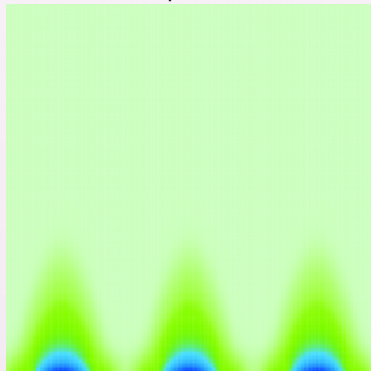
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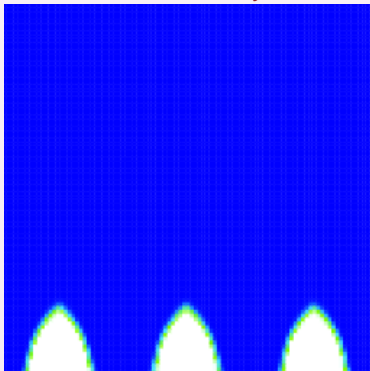
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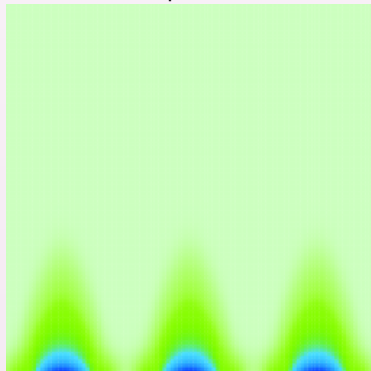
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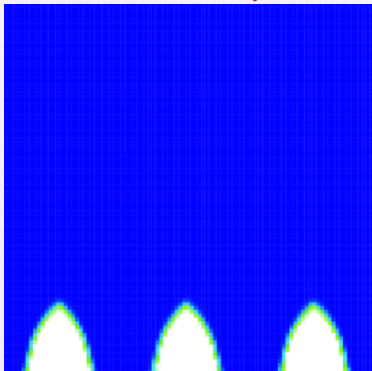
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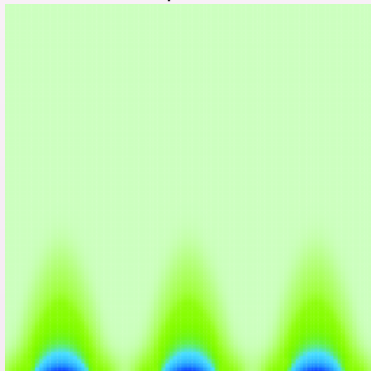
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◀ Geometry

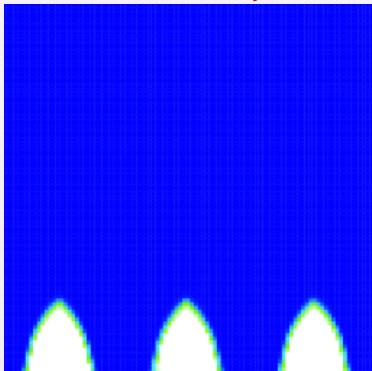
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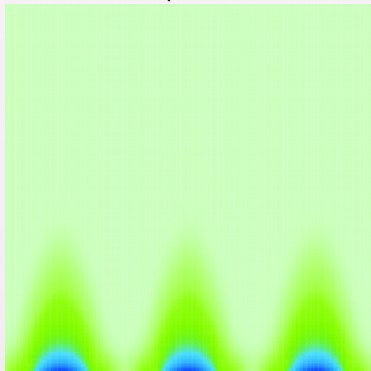


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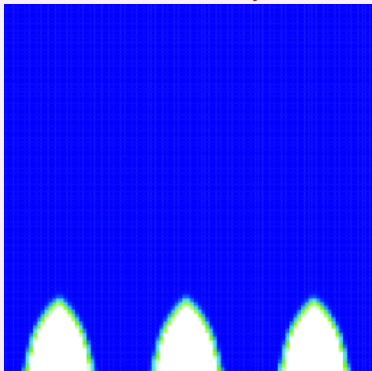
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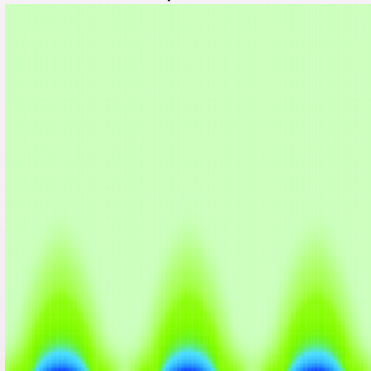
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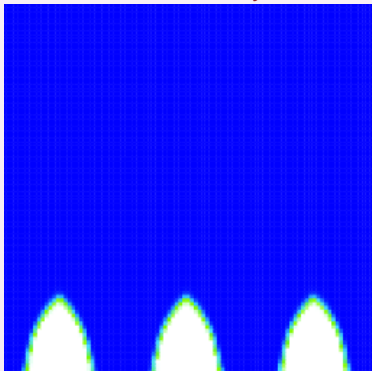
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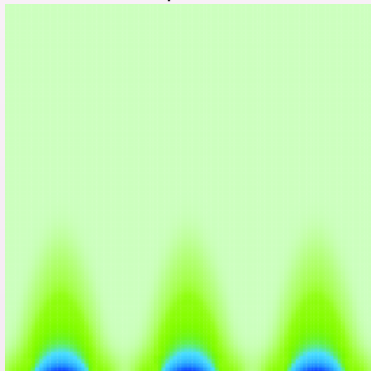
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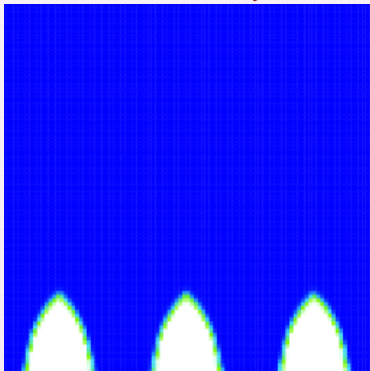
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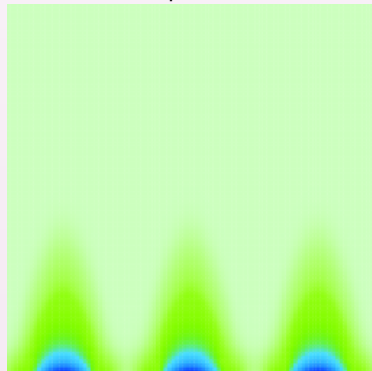
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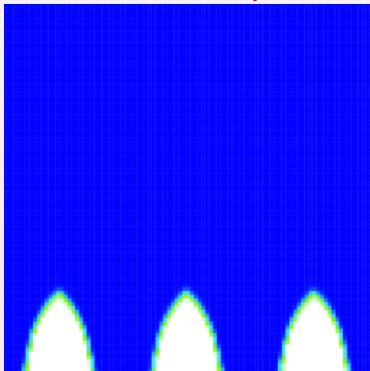
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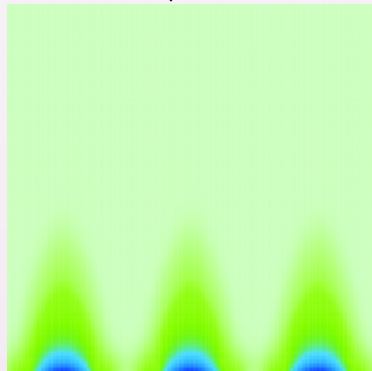
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◀ Geometry

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# OUTLINE

- 1 Model
- 2 Numerical Method
- 3 Numerical Tests
- 4 Conclusion**

# LIQUID-VAPOR PHASE TRANSITION

- Diffuse Interface Model
  - global EOS always at equilibrium (entropy maximization),
  - strict hyperbolicity of the Euler system,
  - uniqueness of Liu solution for the Riemann problem;
- Relaxation Approach
  - 6 (or 5) equation system with relaxation terms;
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  - operator splitting,
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# STIFFENED GAS FOR WATER

$$(\tau_\alpha, \varepsilon_\alpha) \mapsto s_\alpha = c_{v\alpha} \ln(\varepsilon_\alpha - q_\alpha - \pi_\alpha \tau_\alpha) + c_{v\alpha} (\gamma_\alpha - 1) \ln \tau_\alpha + m_\alpha$$

Phase	$c_v$ [J/(kg·K)]	$\gamma$	$\pi$ [Pa]	$q$ [J/kg]	$m$ [J/(kg·K)]
Water	1816.2	2.35	$10^9$	$-1167.056 \times 10^3$	-32765.55596
Steam	1040.14	1.43	0	$2030.255 \times 10^3$	-33265.65947

TABLE: Parameters proposed by [Le Metayer] for water.

$$(P, T) \mapsto \varepsilon_\alpha = c_{v\alpha} T \frac{P + \pi_\alpha \gamma_\alpha}{P + \pi_\alpha} + q_\alpha, \quad (P, T) \mapsto \tau_\alpha = c_{v\alpha} (\gamma_\alpha - 1) \frac{T}{P + \pi_\alpha}.$$

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# WATER TABULATED EOS

$$\left. \begin{array}{l} T^i = 278\text{K} \dots 610\text{K}, \\ \varepsilon_{\alpha}^{\text{sat}}(T^i), \tau_{\alpha}^{\text{sat}}(T^i) \text{ found in the tables} \end{array} \right\} \Rightarrow \left\{ \begin{array}{l} \mathfrak{A} = \left\{ \left( T_i, \frac{1}{\varepsilon_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{B} = \left\{ \left( T_i, \frac{\varepsilon_{\text{liq}}^{\text{sat}}(T_i)}{\varepsilon_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{C} = \left\{ \left( T_i, \frac{1}{\tau_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{D} = \left\{ \left( T_i, \frac{\tau_{\text{liq}}^{\text{sat}}(T_i)}{\tau_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \end{array} \right.$$

$\widehat{\varepsilon}_{\alpha}^{\text{sat}}$  and  $\widehat{\tau}_{\alpha}^{\text{sat}}$  defined by using a least square approximation of  $\mathfrak{A}$ ,  $\mathfrak{B}$ ,  $\mathfrak{C}$  and  $\mathfrak{D}$ :

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