

MODELLING AND SIMULATION OF LIQUID-VAPOR PHASE TRANSITION

A BOILING CRISIS STUDY CONTRIBUTION

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Orsay, 22nd October 2008



OUTLINE

- 1 **Context**
- 2 **Model**
- 3 **Numerical Approximation**
- 4 **Conclusion**



OUTLINE

1 Context

2 Model

- Equation of state
- Movement Equations

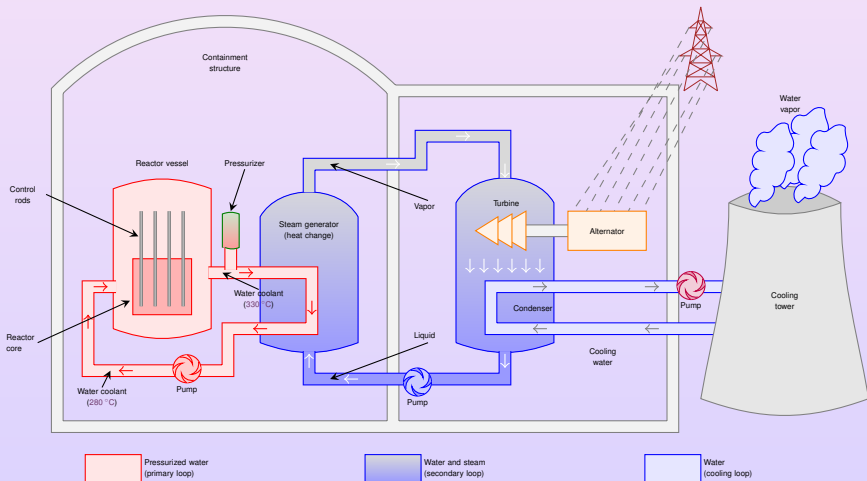
3 Numerical Approximation

- Numerical Method
- Numerical Tests

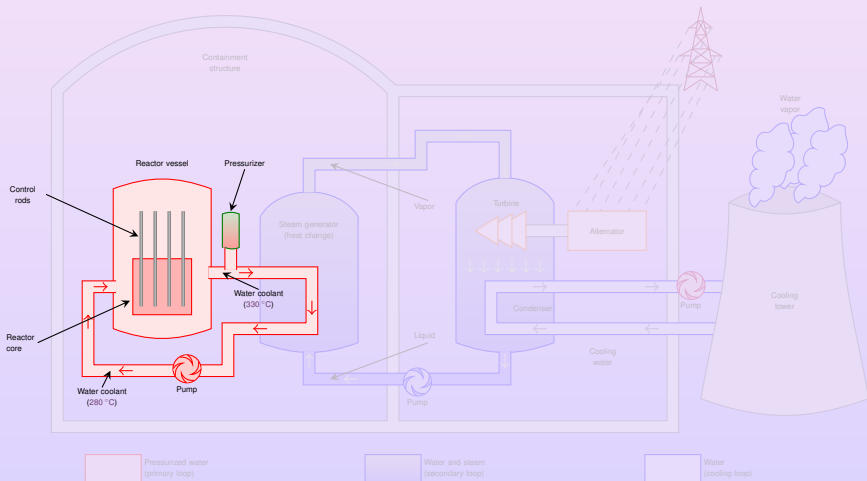
4 Conclusion



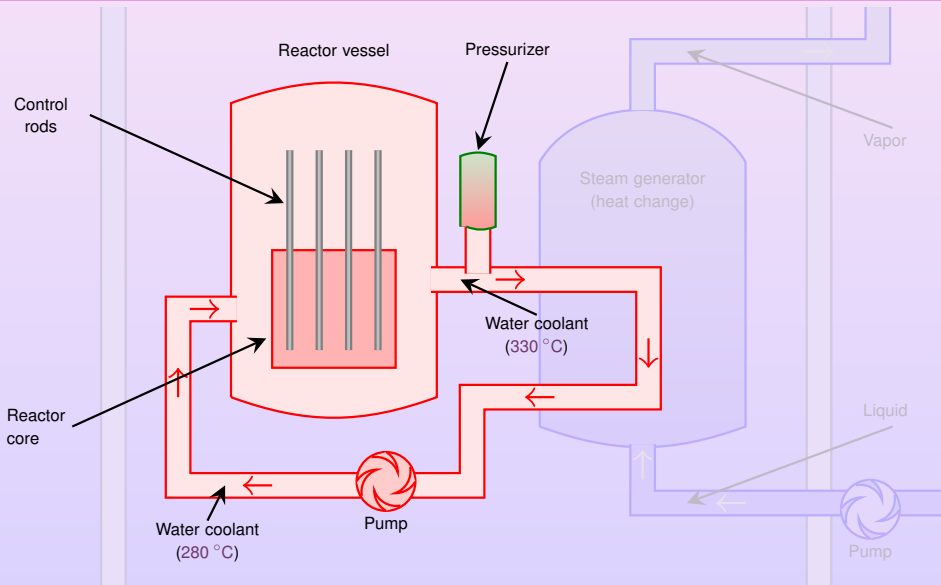
PRESSURIZED WATER REACTOR



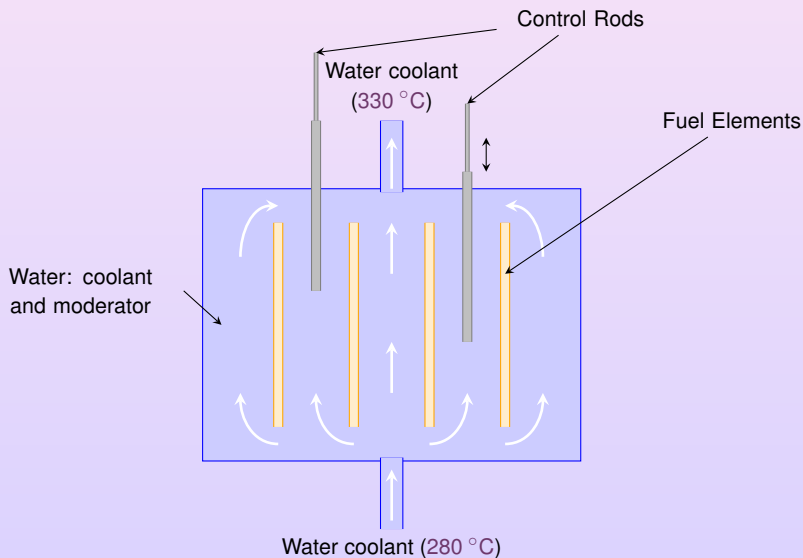
PRESSURIZED WATER REACTOR



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CORE OF A PRESSURIZED WATER REACTOR

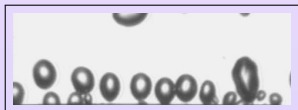


BOILING CRISIS

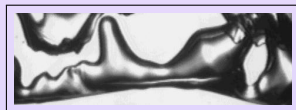
PHENOMENON

Liquid phase heated by a wall at a fixed temperature T^{wall} (pool boiling).
When T^{wall} increases, we switch from a **nucleate boiling** to a **film boiling**.

Nucleate Boiling



Film Boiling



source: http://www.spaceflight.esa.int/users/fluids/TT_boiling.htm

OMEGA - CEA GRENOBLE



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“INGREDIENTS” OF THE MODEL

- ✓ **System of PDEs for the mouvement of the fluid,**
 - Phase transition (pressure and/or temperature variations),
 - Heat Diffusion,
 - Surface Tension,
 - Gravity.

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EULER SYSTEM

$$\begin{cases} \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0, \\ \partial_t(\rho \mathbf{u}) + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = \mathfrak{V}_{\text{vf}} - \mathfrak{S}_{\text{sf}}, \\ \partial_t\left(\rho\left(\frac{|\mathbf{u}|^2}{2} + \varepsilon\right)\right) + \operatorname{div}\left(\rho\left(\frac{|\mathbf{u}|^2}{2} + \varepsilon\right)\mathbf{u} + P \mathbf{u}\right) = (\mathfrak{V}_{\text{vf}} - \mathfrak{S}_{\text{sf}}) \cdot \mathbf{u} - \operatorname{div}(q). \end{cases}$$

- $(\mathbf{x}, t) \mapsto \rho$ specific density,
- $(\mathbf{x}, t) \mapsto \varepsilon$ specific internal energy,
- $(\mathbf{x}, t) \mapsto \mathbf{u}$ velocity;
- $(\rho, \varepsilon) \mapsto \mathfrak{V}_{\text{vf}}$ volumic forces,
- $(\rho, \varepsilon) \mapsto \mathfrak{S}_{\text{sf}}$ surface forces,
- $(\rho, \varepsilon) \mapsto \operatorname{div}(q)$ heat transfert.

$(\rho, \varepsilon) \mapsto P$ pressure law.

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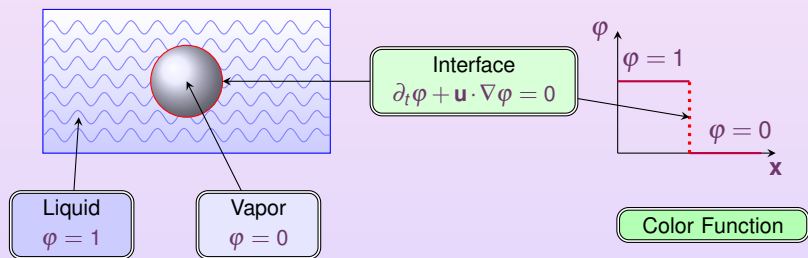
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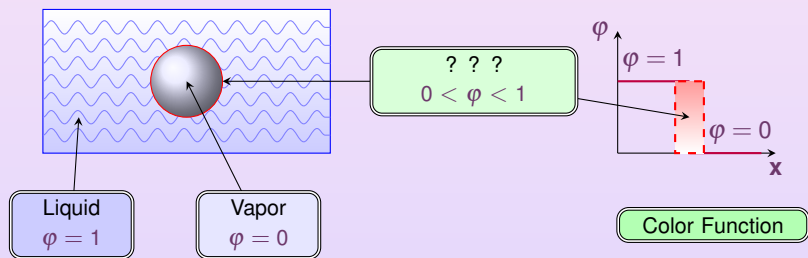
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LIQUID-VAPOR INTERFACE



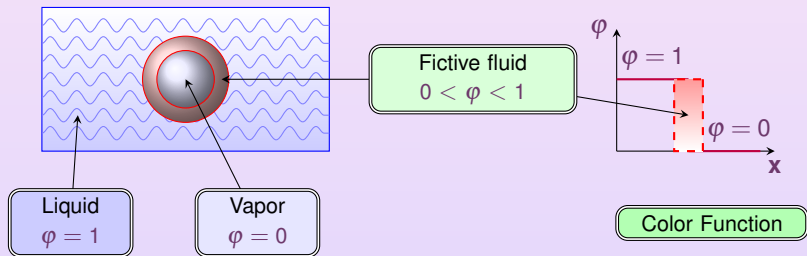
$$(\rho, \varepsilon) \mapsto P = \begin{cases} P^{\text{liq}} & \text{if } \varphi = 1; \\ P^{\text{vap}} & \text{if } \varphi = 0. \end{cases}$$

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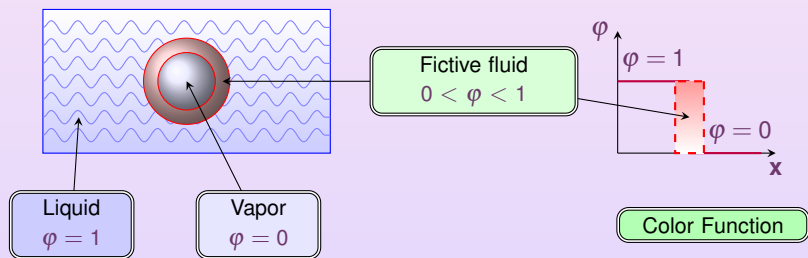
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LIQUID-VAPOR INTERFACE



➡ Goal: define a global pressure law such that

- $(\rho, \varepsilon, \mathbf{u}, P)$ are continuous (3 zones)
- the interface position and the phase change are implicit (\leadsto ~~\emptyset~~)
- coherence with classical thermodynamics [H. Callen]

EOS OF EACH PHASE $\alpha = 1, 2$

$$\left. \begin{array}{l} \tau_{\alpha} \text{ specific volume} \\ \varepsilon_{\alpha} \text{ specific internal energy} \end{array} \right\} \Rightarrow \mathbf{w}_{\alpha} \stackrel{\text{def}}{=} (\tau_{\alpha}, \varepsilon_{\alpha});$$

$\mathbf{w}_{\alpha} \mapsto s_{\alpha}$ specific entropy (Hessian matrix neg. def.);

$$\rightarrow \left\{ \begin{array}{l} T_{\alpha} \stackrel{\text{def}}{=} \left(\frac{\partial s_{\alpha}}{\partial \varepsilon_{\alpha}} \Big|_{\tau_{\alpha}} \right)^{-1} > 0 \quad \text{temperature,} \\ P_{\alpha} \stackrel{\text{def}}{=} T_{\alpha} \frac{\partial s_{\alpha}}{\partial \tau_{\alpha}} \Big|_{\varepsilon_{\alpha}} > 0 \quad \text{pressure,} \\ g_{\alpha} \stackrel{\text{def}}{=} \varepsilon_{\alpha} + P_{\alpha} \tau_{\alpha} - T_{\alpha} s_{\alpha} \quad \text{free enthalpy (Gibbs potential).} \end{array} \right.$$

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EOS WITHOUT PHASE CHANGE

- $\mathbf{w} \stackrel{\text{def}}{=} y\mathbf{w}_1 + (1 - y)\mathbf{w}_2$;
- y mass fraction;
- z volume fraction s.t. $y\tau_1 = z\tau$;
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ENTROPY WITHOUT PHASE CHANGE

$$\sigma \stackrel{\text{def}}{=} y s_1(\mathbf{w}_1) + (1-y) s_2(\mathbf{w}_2) = y s_1\left(\frac{z}{y}\tau, \frac{\psi}{y}\varepsilon\right) + (1-y) s_2\left(\frac{1-z}{1-y}\tau, \frac{1-\psi}{1-y}\varepsilon\right)$$

$$P = \left(\frac{\partial \sigma}{\partial \varepsilon} \Big|_{\tau; y, z, \psi} \right)^{-1} \frac{\partial \sigma}{\partial \tau} \Big|_{\varepsilon; y, z, \psi}$$

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EOS WITH PHASE CHANGE

ENTROPY WITHOUT PH.CH.

$$(\mathbf{w}, z, y, \psi) \mapsto \sigma$$



ENTROPY AT EQUILIBRIUM

$$\mathbf{w} \mapsto s^{\text{eq}}$$

DEFINITION [H. CALLEN, PH. HELLUY ...]

Optimization Problem:

$$s^{\text{eq}}(\mathbf{w}) \stackrel{\text{def}}{=} \max_{z, y, \psi \in [0, 1]^3} \sigma(\mathbf{w}, z, y, \psi)$$

Optimality Condition:
$$\begin{cases} T_1(z, y, \psi) = T_2(z, y, \psi) \\ P_1(z, y, \psi) = P_2(z, y, \psi) \\ g_1(z, y, \psi) = g_2(z, y, \psi) \\ z, y, \psi \in]0, 1[^3 \end{cases}$$

Solution: (z^*, y^*, ψ^*)

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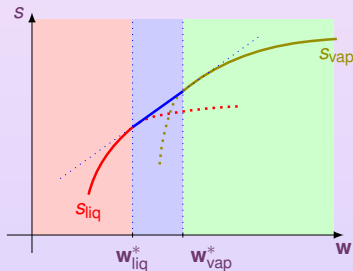
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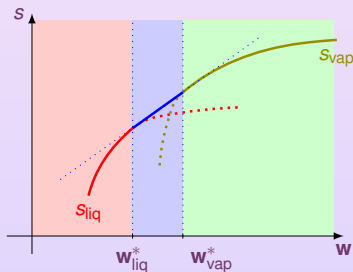
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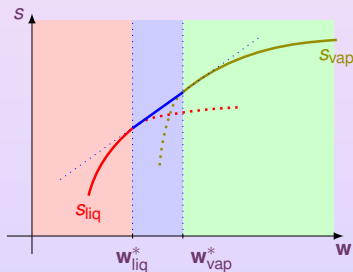
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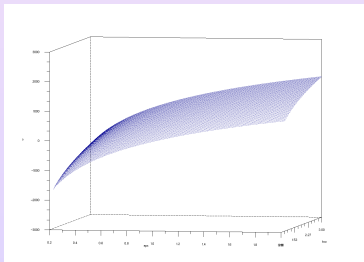
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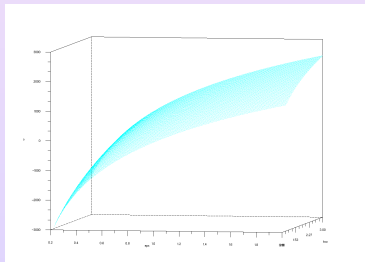
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CONCAVE HULL WITH TWO PERFECT GASES

$$(\tau, \varepsilon) \mapsto s_{\text{liq}}$$

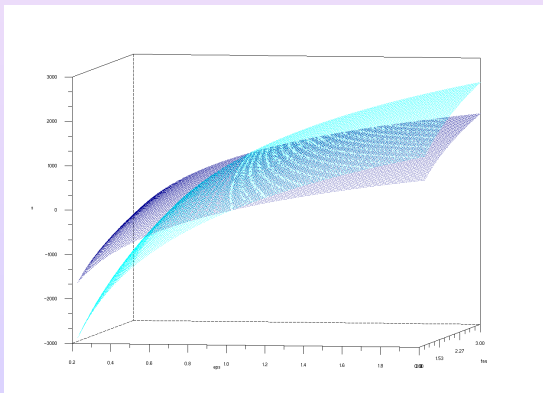


$$(\tau, \varepsilon) \mapsto s_{\text{vap}}$$



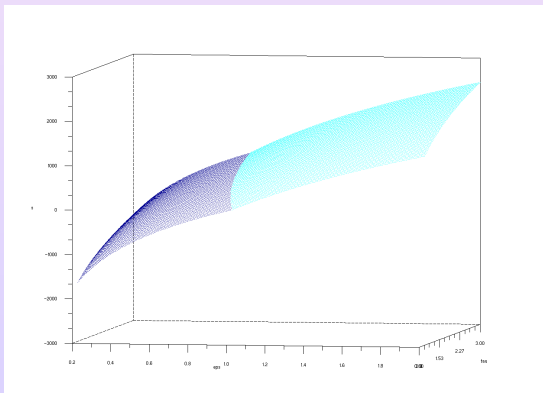
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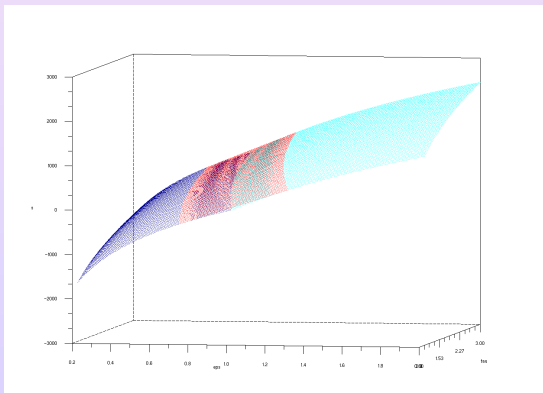
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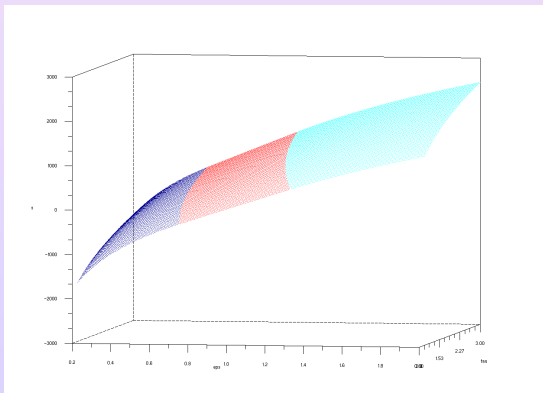
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FROM $\mathbf{w} \mapsto s^{\text{eq}}$ TO $\mathbf{w} \mapsto P^{\text{eq}}$

For all $\tilde{\mathbf{w}}$ fixed, we seek $(\mathbf{w}_{\text{liq}}^*, \mathbf{w}_{\text{vap}}^*, y^*)$ as the solution of the system

$$\begin{cases} P_{\text{liq}}(\mathbf{w}_{\text{liq}}) = P_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ T_{\text{liq}}(\mathbf{w}_{\text{liq}}) = T_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ g_{\text{liq}}(\mathbf{w}_{\text{liq}}) = g_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ \tilde{\mathbf{w}} = y\mathbf{w}_{\text{liq}} + (1-y)\mathbf{w}_{\text{vap}} \end{cases}$$

- if $y^* \in]0, 1[$ then $\tilde{\mathbf{w}}$ is an **equilibrium mixture state**

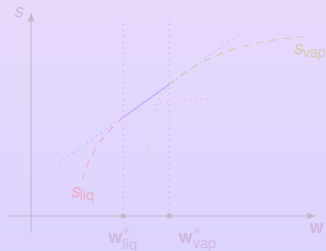
$$s^{\text{eq}}(\tilde{\mathbf{w}}) = y^* s_{\text{liq}}(\mathbf{w}_{\text{liq}}^*) + (1-y^*) s_{\text{vap}}(\mathbf{w}_{\text{vap}}^*),$$

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- if the system has no solution or $y^* \notin]0, 1[$ then $\tilde{\mathbf{w}}$ is a **monophasique pure state**

$$s^{\text{eq}}(\tilde{\mathbf{w}}) = \max\{s_{\text{liq}}(\tilde{\mathbf{w}}), s_{\text{vap}}(\tilde{\mathbf{w}})\},$$

$$P^{\text{eq}}(\tilde{\mathbf{w}}) = P_{\pm}(\tilde{\mathbf{w}})$$



FROM $\mathbf{w} \mapsto \mathbf{s}^{\text{eq}}$ TO $\mathbf{w} \mapsto P^{\text{eq}}$

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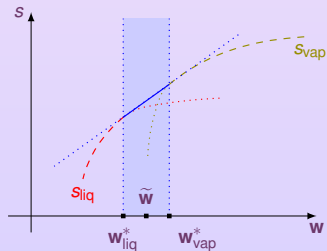
- if $y^* \in]0, 1[$ then $\tilde{\mathbf{w}}$ is an **equilibrium mixture state**

$$\begin{aligned} \mathbf{s}^{\text{eq}}(\tilde{\mathbf{w}}) &= y^* \mathbf{s}_{\text{liq}}(\mathbf{w}_{\text{liq}}^*) + (1-y^*) \mathbf{s}_{\text{vap}}(\mathbf{w}_{\text{vap}}^*), \\ P^{\text{eq}}(\tilde{\mathbf{w}}) &= P_{\text{liq}}(\mathbf{w}_{\text{liq}}^*) = P_{\text{vap}}(\mathbf{w}_{\text{vap}}^*); \end{aligned}$$

- if the system has no solution or $y^* \notin]0, 1[$ then $\tilde{\mathbf{w}}$ is a **monophasique pure state**

$$\mathbf{s}^{\text{eq}}(\tilde{\mathbf{w}}) = \max\{\mathbf{s}_{\text{liq}}(\tilde{\mathbf{w}}), \mathbf{s}_{\text{vap}}(\tilde{\mathbf{w}})\},$$

$$P^{\text{eq}}(\tilde{\mathbf{w}}) = P_{\text{liq}}(\tilde{\mathbf{w}})$$



FROM $\mathbf{w} \mapsto \mathbf{s}^{\text{eq}}$ TO $\mathbf{w} \mapsto P^{\text{eq}}$

For all $\tilde{\mathbf{w}}$ fixed, we seek $(\mathbf{w}_{\text{liq}}^*, \mathbf{w}_{\text{vap}}^*, y^*)$ as the solution of the system

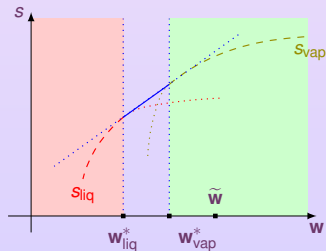
$$\begin{cases} P_{\text{liq}}(\mathbf{w}_{\text{liq}}) = P_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ T_{\text{liq}}(\mathbf{w}_{\text{liq}}) = T_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ g_{\text{liq}}(\mathbf{w}_{\text{liq}}) = g_{\text{vap}}(\mathbf{w}_{\text{vap}}) \\ \tilde{\mathbf{w}} = y\mathbf{w}_{\text{liq}} + (1-y)\mathbf{w}_{\text{vap}} \end{cases}$$

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FROM $\mathbf{w} \mapsto s^{\text{eq}}$ TO $\mathbf{w} \mapsto P^{\text{eq}}$

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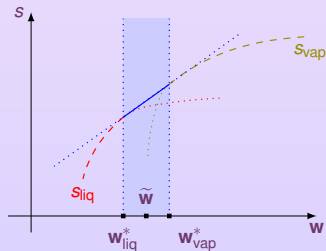
$$s^{\text{eq}}(\tilde{\mathbf{w}}) = y^* s_{\text{liq}}(\mathbf{w}_{\text{liq}}^*) + (1-y^*) s_{\text{vap}}(\mathbf{w}_{\text{vap}}^*),$$

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FROM $\mathbf{w} \mapsto s^{\text{eq}}$ TO $\mathbf{w} \mapsto P^{\text{eq}}$

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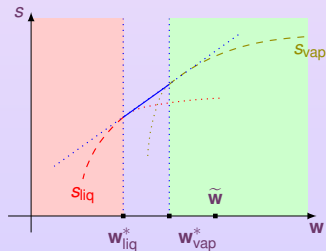
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ANALYTICAL EOS

 (τ, ε) fixed $(\tau_1, \varepsilon_1, \tau_2, \varepsilon_2, y)$ SOLUTION OF

$$\begin{cases} g_1(\tau_1, \varepsilon_1) = g_2(\tau_2, \varepsilon_2) \\ P_1(\tau_1, \varepsilon_1) = P_2(\tau_2, \varepsilon_2) \\ T_1(\tau_1, \varepsilon_1) = T_2(\tau_2, \varepsilon_2) \\ \tau = y\tau_1 + (1-y)\tau_2 \\ \varepsilon = y\varepsilon_1 + (1-y)\varepsilon_2 \end{cases}$$

 (P, T) SOLUTION OF

$$\begin{cases} g_1(P, T) = g_2(P, T) \\ \frac{\tau - \tau_2(P, T)}{\tau_1(P, T) - \tau_2(P, T)} = \frac{\varepsilon - \varepsilon_2(P, T)}{\varepsilon_1(P, T) - \varepsilon_2(P, T)} \end{cases}$$

$$T \mapsto P = P^{\text{sat}}(T) \approx P^{\text{sat}}(T)$$

 T SOLUTION OF

$$\frac{\tau - \tau_2^{\text{sat}}(T)}{\tau_1^{\text{sat}}(T) - \tau_2^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_2^{\text{sat}}(T)}{\varepsilon_1^{\text{sat}}(T) - \varepsilon_2^{\text{sat}}(T)} \quad \text{where} \quad \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha^{\text{sat}}(T) \stackrel{\text{def}}{=} \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_\alpha(P^{\text{sat}}(T), T)$$

→ [Numerical Solution](#)

ANALYTICAL EOS

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* Numerical solution

ANALYTICAL EOS

(τ, ε) fixed

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least square approximation

$$T \mapsto P = \hat{P}^{\text{sat}}(T) \approx P^{\text{sat}}(T)$$

T SOLUTION OF

$$\frac{\tau - \tau_2^{\text{sat}}(T)}{\tau_1^{\text{sat}}(T) - \tau_2^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_2^{\text{sat}}(T)}{\varepsilon_1^{\text{sat}}(T) - \varepsilon_2^{\text{sat}}(T)} \quad \text{where} \quad \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(T) \stackrel{\text{def}}{=} \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}(\hat{P}^{\text{sat}}(T), T)$$

► Water Example

TABULATED EOS

(τ, ε) fixed

T SOLUTION OF

$$\frac{\tau - \tau_2^{\text{sat}}(T)}{\tau_1^{\text{sat}}(T) - \tau_2^{\text{sat}}(T)} = \frac{\varepsilon - \varepsilon_2^{\text{sat}}(T)}{\varepsilon_1^{\text{sat}}(T) - \varepsilon_2^{\text{sat}}(T)} \quad \text{with} \quad \begin{pmatrix} \tau \\ \varepsilon \end{pmatrix}_{\alpha}^{\text{sat}}(T) \quad \text{tabulated}$$

\rightsquigarrow

$$\frac{\tau - \widehat{\tau}_2^{\text{sat}}(T)}{\widehat{\tau}_1^{\text{sat}}(T) - \widehat{\tau}_2^{\text{sat}}(T)} = \frac{\varepsilon - \widehat{\varepsilon}_2^{\text{sat}}(T)}{\widehat{\varepsilon}_1^{\text{sat}}(T) - \widehat{\varepsilon}_2^{\text{sat}}(T)} \quad \text{with} \quad \begin{pmatrix} \widehat{\tau} \\ \widehat{\varepsilon} \end{pmatrix}_{\alpha}^{\text{sat}}(T)$$

★ Water Example

TABULATED EOS

(τ, ε) fixed

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least square approximations

★ Water Example

TABULATED EOS

(τ, ε) fixed

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▶▶ Water Examples

OUTLINE

1 Context

2 Model

- Equation of state
- **Movement Equations**

3 Numerical Approximation

- Numerical Method
- Numerical Tests

4 Conclusion

DYNAMIC LIQUID-VAPOR PHASE CHANGE

EULER SYSTEM

$$\begin{cases} \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0, \\ \partial_t(\rho \mathbf{u}) + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t \left(\rho \left(\frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \right) + \operatorname{div} \left(\rho \left(\frac{|\mathbf{u}|^2}{2} + \varepsilon \right) \mathbf{u} + P^{\text{eq}} \mathbf{u} \right) = 0 \end{cases} \quad \text{with} \quad P^{\text{eq}} \stackrel{\text{def}}{=} \frac{S_\tau^{\text{eq}}}{S_\varepsilon^{\text{eq}}}.$$

PROPERTIES [G. ALLAIRE, G. FACCANONI, S. KOKH]

If $\tau_1^* \neq \tau_2^*$ and $\varepsilon_1^* \neq \varepsilon_2^*$ (first order phase transition) then

$$\textcircled{1} c(w) > 0, \quad \textcircled{2} s_{cc}^{\text{eq}}(w) > 0$$

- ① Euler system: strict hyperbolicity (\neq p-system),
- ② Riemann problem: multitude of entropy (Lax) solutions [R. Menikoff, B. J. Plohr], uniqueness of Liu solution.

DYNAMIC LIQUID-VAPOR PHASE CHANGE



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HOW TO SIMULATE THE LIU SOLUTION

- Exact Riemann Solver (cf. [A. Voß] for Van der Waals EOS)
- Viscous Solver (the Liu solution is the only solution that has a viscous profile) (cf. [S. Jaouen] for Perfect Gas EOS with $c_{V_{liq}} = c_{V_{vap}}$)
- Solver(s) based on **Relaxation Approach** [F. Coquel, B. Perthame], [Th. Barberon, Ph. Helluy], [Ph. Helluy, N. Seguin], [F. Coquel, F. Caro, D. Jamet, S. Kokh], . . .

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RELAXATION APPROACH

$$\partial_t \mathbf{U} + \operatorname{div} \mathbf{F}(\mathbf{U}) = \mathbf{0}$$

RELAXATION APPROACH

$$\partial_t \mathbf{V} + \operatorname{div} \mathbf{G}(\mathbf{V}) = \frac{1}{\mu} \mathbf{R}(\mathbf{V}) \quad \xrightarrow[\mu \rightarrow 0]{\text{Formally}} \quad \partial_t \mathbf{U} + \operatorname{div} \mathbf{F}(\mathbf{U}) = \mathbf{0}$$

RELAXATION APPROACH

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EQUILIBRIUM SYSTEM

$$\begin{cases} \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0 \\ \partial_t(\rho \mathbf{u}) + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t(\rho e) + \operatorname{div}((\rho e + P^{\text{eq}}) \mathbf{u}) = 0 \end{cases}$$

$$P^{\text{eq}}(\rho, \varepsilon) = \frac{s_\tau^{\text{eq}}}{s_\varepsilon^{\text{eq}}}, \quad e \stackrel{\text{def}}{=} \frac{|\mathbf{u}|^2}{2} + \varepsilon$$

RELAXATION APPROACH

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AUGMENTED SYSTEM

$$\begin{cases} \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0 \\ \partial_t(\rho \mathbf{u}) + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = 0 \\ \partial_t(\rho e) + \operatorname{div}((\rho e + P) \mathbf{u}) = 0 \end{cases}$$

$$P(\rho, \varepsilon, z, y, \psi) = \frac{\sigma_\tau}{\sigma_\varepsilon}$$

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$$\partial_t \mathbf{V} + \operatorname{div} \mathbf{G}(\mathbf{V}) = \frac{1}{\mu} \mathbf{R}(\mathbf{V}) \quad \xrightarrow[\mu \rightarrow 0]{\text{Formally}} \quad \partial_t \mathbf{U} + \operatorname{div} \mathbf{F}(\mathbf{U}) = \mathbf{0}$$

AUGMENTED SYSTEM

$$\begin{cases} \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0 \\ \partial_t(\rho \mathbf{u}) + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = 0 \\ \partial_t(\rho e) + \operatorname{div}((\rho e + P)\mathbf{u}) = 0 \end{cases}$$

In the interface

$$\begin{cases} \partial_t z + \mathbf{u} \cdot \operatorname{grad} z = \\ \partial_t y + \mathbf{u} \cdot \operatorname{grad} y = \\ \partial_t \psi + \mathbf{u} \cdot \operatorname{grad} \psi = \end{cases}$$

$$P(\rho, \varepsilon, z, y, \psi) = \frac{\sigma_\tau}{\sigma_\varepsilon}$$

EQUILIBRIUM SYSTEM

$$\begin{cases} \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0 \\ \partial_t(\rho \mathbf{u}) + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t(\rho e) + \operatorname{div}((\rho e + P^{\text{eq}})\mathbf{u}) = 0 \end{cases}$$

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$$\partial_t \mathbf{V} + \operatorname{div} \mathbf{G}(\mathbf{V}) = \frac{1}{\mu} \mathbf{R}(\mathbf{V}) \quad \xrightarrow[\mu \rightarrow 0]{\text{Formally}} \quad \partial_t \mathbf{U} + \operatorname{div} \mathbf{F}(\mathbf{U}) = \mathbf{0}$$

AUGMENTED SYSTEM

$$\begin{cases} \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0 \\ \partial_t(\rho \mathbf{u}) + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = 0 \\ \partial_t(\rho e) + \operatorname{div}((\rho e + P) \mathbf{u}) = 0 \end{cases}$$

In the interface

$$\begin{cases} \partial_t z + \mathbf{u} \cdot \operatorname{grad} z = \frac{1}{\mu_z} \left(\frac{P_2}{T_2} - \frac{P_1}{T_1} \right) \\ \partial_t y + \mathbf{u} \cdot \operatorname{grad} y = \frac{1}{\mu_y} \left(\frac{g_1}{T_1} - \frac{g_2}{T_2} \right) \frac{1}{\rho} \\ \partial_t \psi + \mathbf{u} \cdot \operatorname{grad} \psi = \frac{1}{\mu_\psi} \left(\frac{1}{T_1} - \frac{1}{T_2} \right) \varepsilon \end{cases}$$

$$P(\rho, \varepsilon, z, y, \psi) = \frac{\sigma_\tau}{\sigma_\varepsilon}$$

Formally
 $\mu_j \rightarrow 0$

EQUILIBRIUM SYSTEM

$$\begin{cases} \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0 \\ \partial_t(\rho \mathbf{u}) + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t(\rho e) + \operatorname{div}((\rho e + P^{\text{eq}}) \mathbf{u}) = 0 \end{cases}$$

$$P^{\text{eq}}(\rho, \varepsilon) = \frac{\sigma_\tau^{\text{eq}}}{\sigma_\varepsilon^{\text{eq}}}, \quad e \stackrel{\text{def}}{=} \frac{|\mathbf{u}|^2}{2} + \varepsilon$$

RELAXATION APPROACH

$$\partial_t \mathbf{V} + \operatorname{div} \mathbf{G}(\mathbf{V}) = \frac{1}{\mu} \mathbf{R}(\mathbf{V}) \quad \xrightarrow[\mu \rightarrow 0]{\text{Formally}} \quad \partial_t \mathbf{U} + \operatorname{div} \mathbf{F}(\mathbf{U}) = \mathbf{0}$$

AUGMENTED SYSTEM

$$\begin{cases} \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0 \\ \partial_t(\rho \mathbf{u}) + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u} + P \mathbb{I}) = 0 \\ \partial_t(\rho e) + \operatorname{div}((\rho e + P) \mathbf{u}) = 0 \end{cases}$$

In the interface

$$\begin{cases} \partial_t z + \mathbf{u} \cdot \operatorname{grad} z = \frac{1}{\mu_z} \left(\frac{P_2}{T_2} - \frac{P_1}{T_1} \right) \\ \partial_t y + \mathbf{u} \cdot \operatorname{grad} y = \frac{1}{\mu_y} \left(\frac{g_1}{T_1} - \frac{g_2}{T_2} \right) \frac{1}{\rho} \\ \partial_t \psi + \mathbf{u} \cdot \operatorname{grad} \psi = \frac{1}{\mu_\psi} \left(\frac{1}{T_1} - \frac{1}{T_2} \right) \varepsilon \end{cases}$$

$$P(\rho, \varepsilon, z, y, \psi) = \frac{\sigma_\tau}{\sigma_e}$$

Formally
 $\mu_j \rightarrow 0$

EQUILIBRIUM SYSTEM

$$\begin{cases} \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0 \\ \partial_t(\rho \mathbf{u}) + \operatorname{div}(\rho \mathbf{u} \otimes \mathbf{u} + P^{\text{eq}} \mathbb{I}) = 0 \\ \partial_t(\rho e) + \operatorname{div}((\rho e + P^{\text{eq}}) \mathbf{u}) = 0 \end{cases}$$

$$P^{\text{eq}}(\rho, \varepsilon) = \frac{s_\tau^{\text{eq}}}{s_e^{\text{eq}}}, \quad e \stackrel{\text{def}}{=} \frac{|\mathbf{u}|^2}{2} + \varepsilon$$

REMARK: ~~$\partial_t \psi + \mathbf{u} \cdot \operatorname{grad} \psi = 0 \rightsquigarrow T_1 = T_2$~~

NUMERICAL SCHEME

$$\partial_t \mathbf{V} + \operatorname{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V}) + \frac{1}{\mu} \mathbf{R}(\mathbf{V})$$

 \mathbf{V}_i^n

$\textcircled{1} \mu_j = +\infty$



$$\partial_t \mathbf{V} + \operatorname{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V})$$

Aug. System: 5-eq. iso-T
 Num. Scheme: op. splitting
 Conv.: [G. Allaire and all.]
 Surf. Tens.: [J. U. Brackbill and all.]
 Heat: 2D implicit

 \mathbf{V}_i^{n+1}

$\textcircled{2} \mu_j = 0$



$$\mathbf{R}(\mathbf{V}) = 0$$

update fractions
 (y, z, ψ) by
 projecting $\mathbf{V}_i^{n+1/2}$
 onto the
 P, T, g equilibrium

NUMERICAL SCHEME

$$\partial_t \mathbf{V} + \text{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V}) + \frac{1}{\mu} \mathbf{R}(\mathbf{V})$$

 \mathbf{V}_i^n

$$\textcircled{1} \mu_j = +\infty$$



$$\partial_t \mathbf{V} + \text{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V})$$

Aug. System: 5-eq. iso-T
 Num. Scheme: op. splitting
 Conv.: [G. Allaire and all.]
 Surf. Tens.: [J. U. Brackbill and all.]
 Heat: 2D implicit

 \mathbf{V}_i^{n+1}

$$\textcircled{2} \mu_j = 0$$

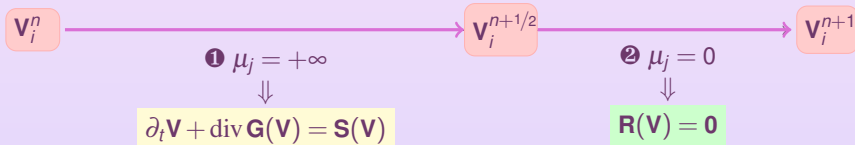


$$\mathbf{R}(\mathbf{V}) = 0$$

update fractions
 (y, z, ψ) by
 projecting $\mathbf{V}_i^{n+1/2}$
 onto the
 P, T, g equilibrium

NUMERICAL SCHEME

$$\partial_t \mathbf{V} + \text{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V}) + \frac{1}{\mu} \mathbf{R}(\mathbf{V})$$

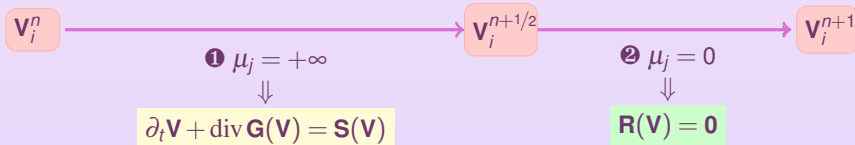


Aug. System: 5-eq. iso-T
 Num. Scheme: op. splitting
 Conv.: [G. Allaire and all.]
 Surf. Tens.: [J. U. Brackbill and all.]
 Heat: 2D implicit

update fractions
 (y, z, ψ) by
 projecting $\mathbf{V}_i^{n+1/2}$
 onto the
 P, T, g equilibrium

NUMERICAL SCHEME

$$\partial_t \mathbf{V} + \text{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V}) + \frac{1}{\mu} \mathbf{R}(\mathbf{V})$$



Aug. System: 5-eq. iso-T
 Num. Scheme: op. splitting
 Conv.: [G. Allaire and all.]
 Surf. Tens.: [J. U. Brackbill and all.]
 Heat: 2D implicit

update fractions
 (y, z, ψ) by
 projecting $\mathbf{V}_i^{n+1/2}$
 onto the
 P, T, g equilibrium

NUMERICAL SCHEME

$$\partial_t \mathbf{V} + \text{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V}) + \frac{1}{\mu} \mathbf{R}(\mathbf{V})$$

$$\mathbf{V}_i^n$$

$$\textcircled{1} \mu_j = +\infty$$



$$\partial_t \mathbf{V} + \text{div} \mathbf{G}(\mathbf{V}) = \mathbf{S}(\mathbf{V})$$

Aug. System: 5-eq. iso-T
 Num. Scheme: op. splitting
 Conv.: [G. Allaire and all.]
 Surf. Tens.: [J. U. Brackbill and all.]
 Heat: 2D implicit

$$\mathbf{V}_i^{n+1/2}$$

$$\textcircled{2} \mu_j = 0$$



$$\mathbf{R}(\mathbf{V}) = 0$$

update fractions
 (y, z, ψ) by
 projecting $\mathbf{V}_i^{n+1/2}$
 onto the
 P, T, g equilibrium

$$\mathbf{V}_i^{n+1}$$

OUTLINE

1 Context

2 Model

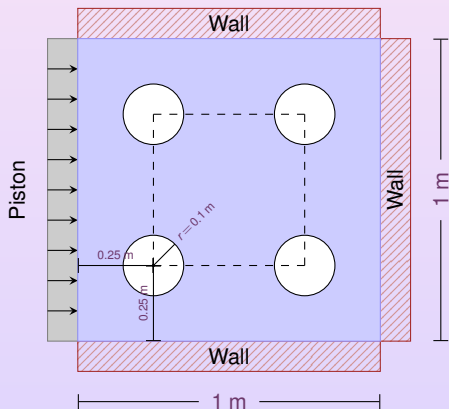
- Equation of state
- Movement Equations

3 Numerical Approximation

- Numerical Method
- Numerical Tests

4 Conclusion

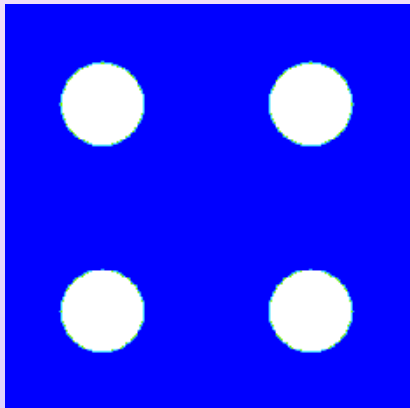
COMPRESSION OF VAPOR BUBBLES



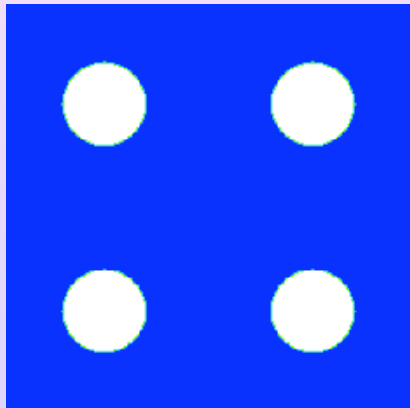
Compression of 4 Vapor Bubbles involving two Stiffened Gases for water and steam. The piston moves towards right at constant speed $u_p = 30 \text{ m/s}$.

COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



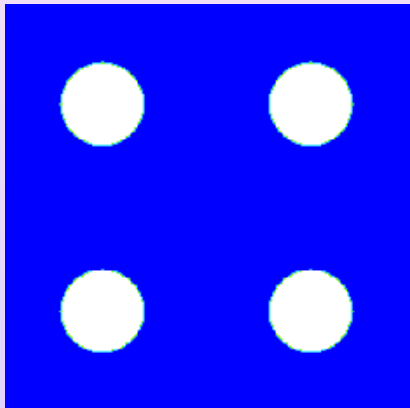
◀ Geometry

▶ Play

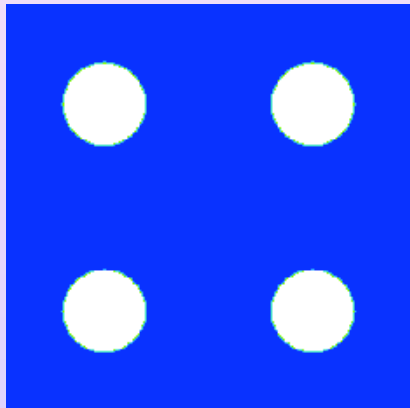
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



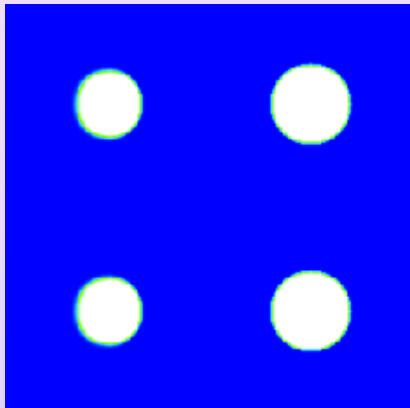
◀ Geometry

▶ Play

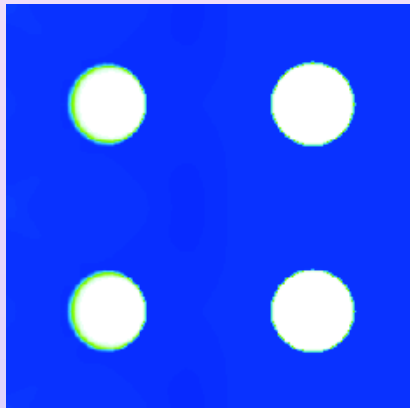
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



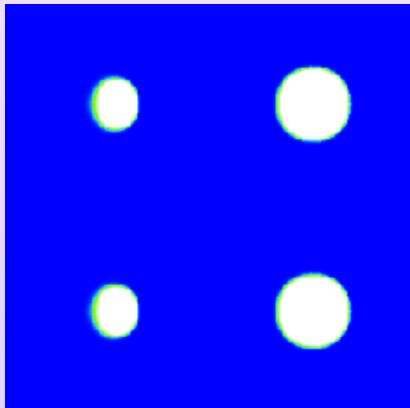
◀ Geometry

▶ Play

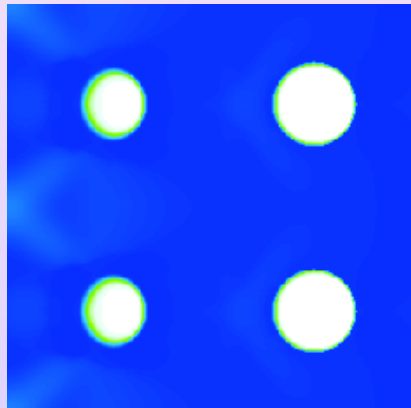
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



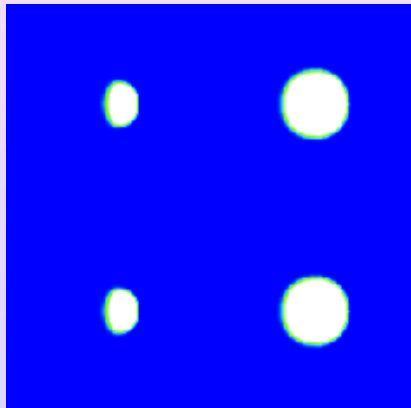
◀ Geometry

▶ Play

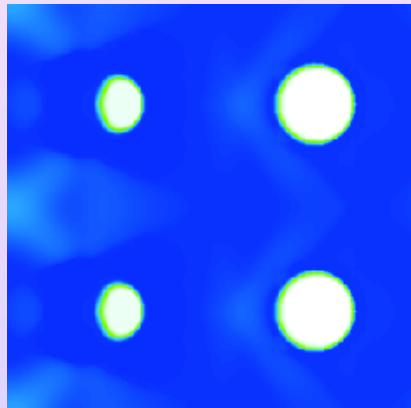
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



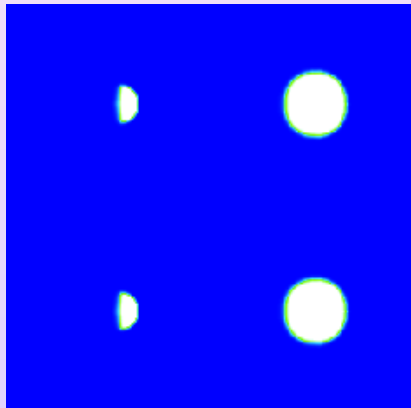
◀ Geometry

▶ Play

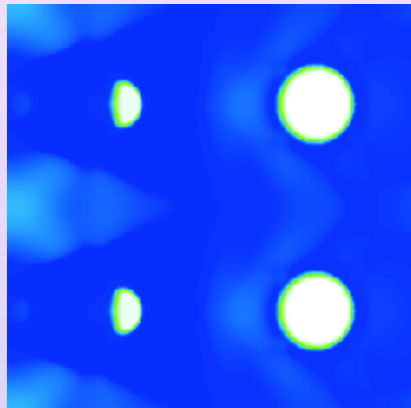
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



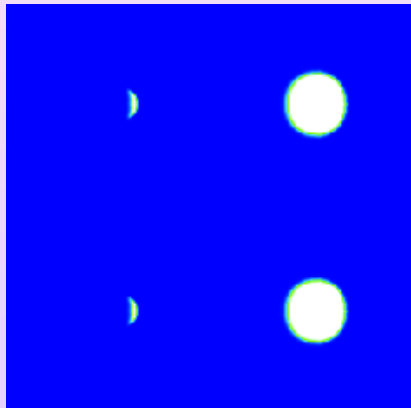
◀ Geometry

▶ Play

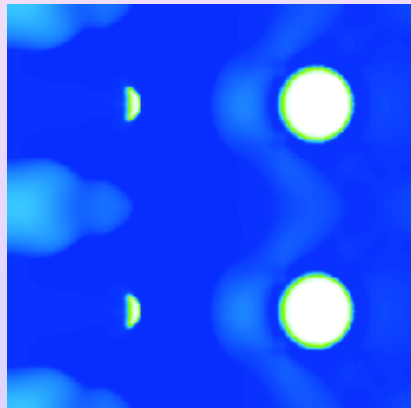
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



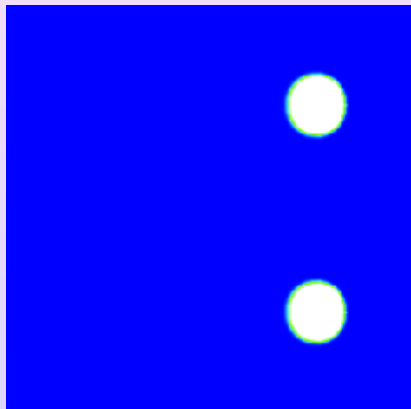
◀ Geometry

▶ Play

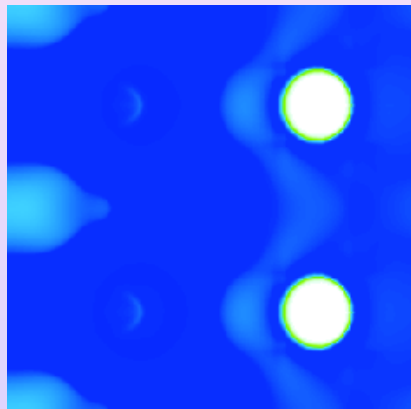
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



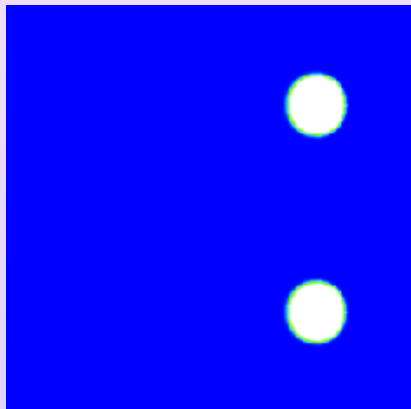
◀ Geometry

▶ Play

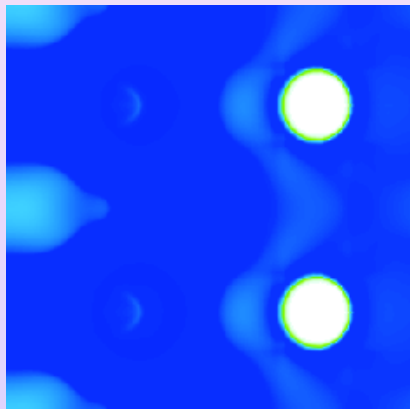
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



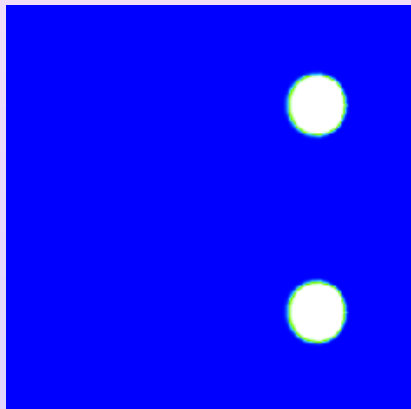
◀ Geometry

▶ Play

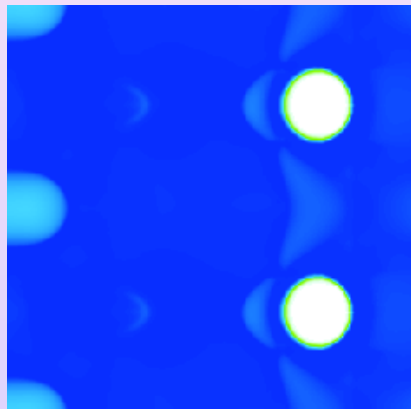
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



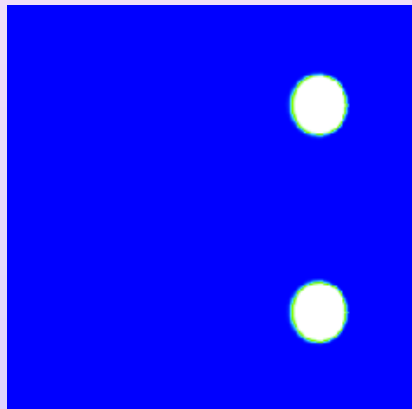
◀ Geometry

▶ Play

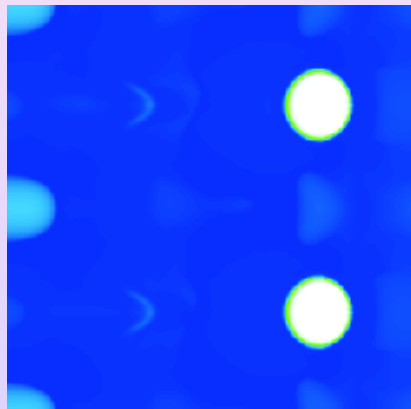
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



◀ Geometry

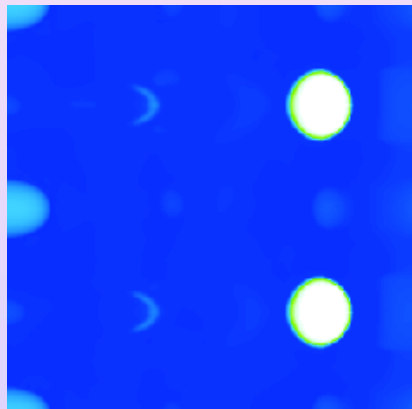
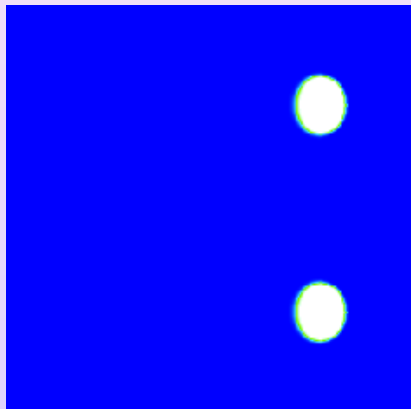
▶ Play

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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y

Density ρ



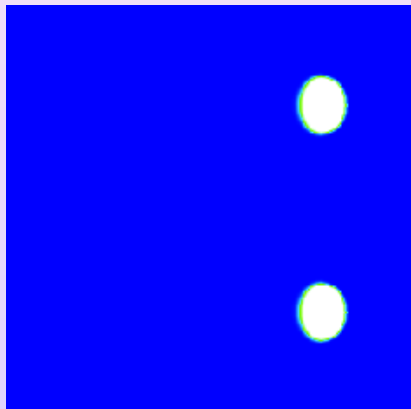
◀ Geometry

▶ Play

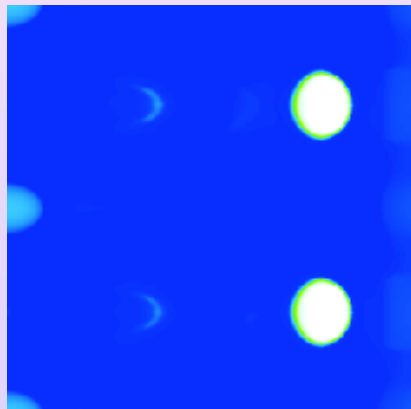
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



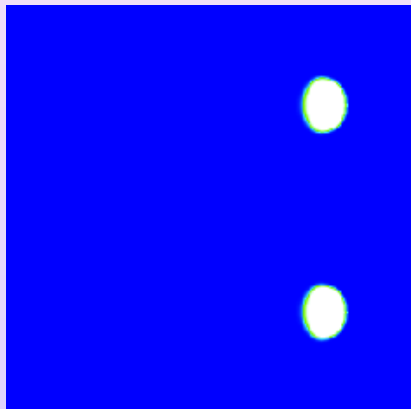
◀ Geometry

▶ Play

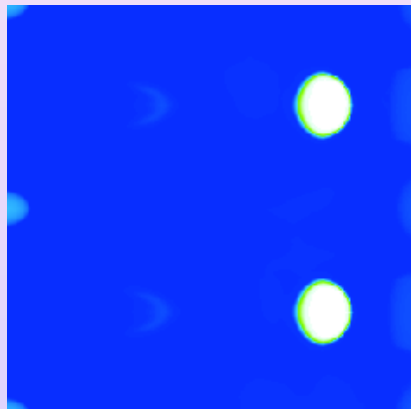
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



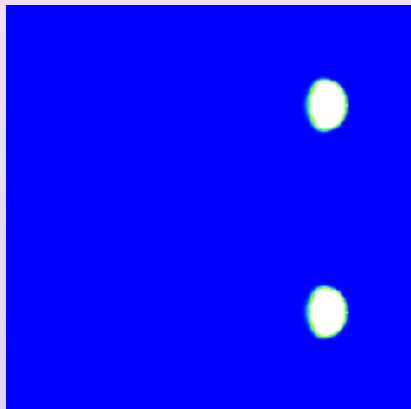
◀ Geometry

▶ Play

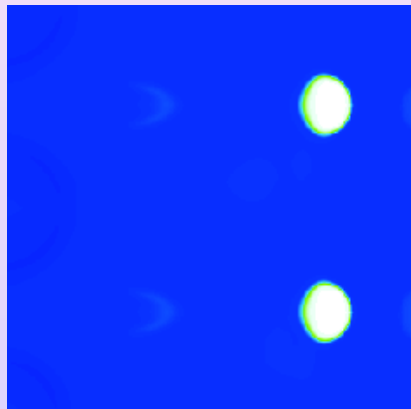
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



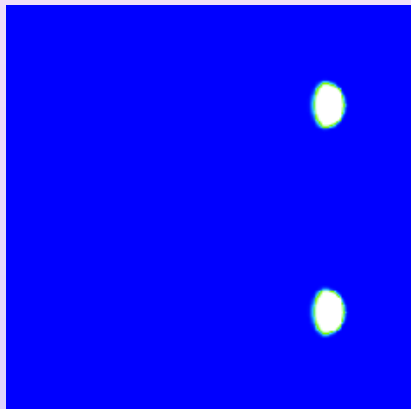
◀ Geometry

▶ Play

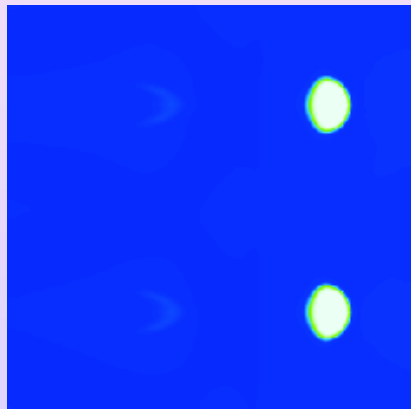
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



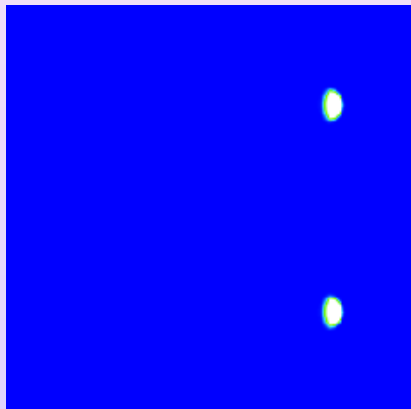
◀ Geometry

▶ Play

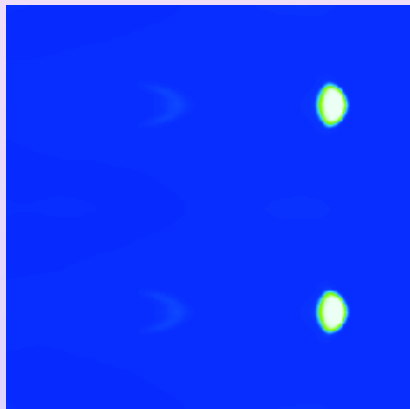
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



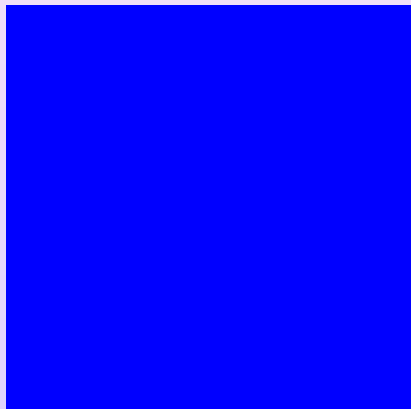
◀ Geometry

▶ Play

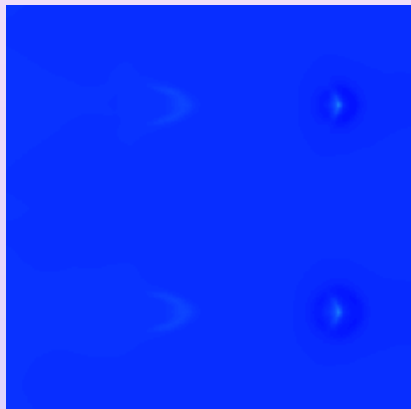
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COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



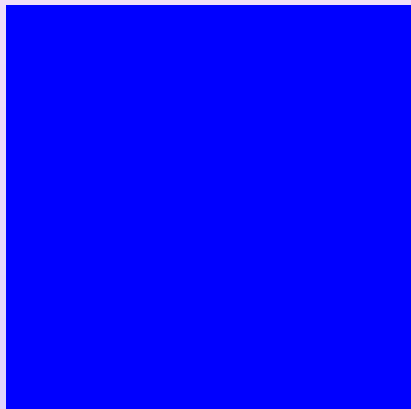
◀ Geometry

▶ Play

▶▶ Skip

COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



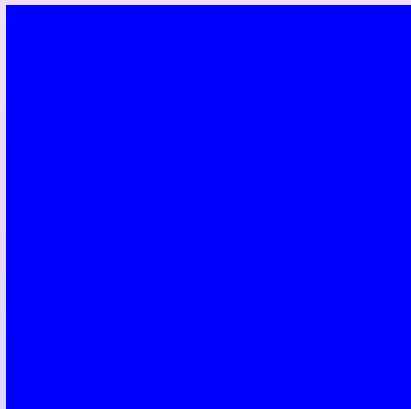
◀ Geometry

▶ Play

▶▶ Skip

COMPRESSION OF VAPOR BUBBLES

Mass Fraction y



Density ρ



◀ Geometry

▶ Play

▶▶ Skip

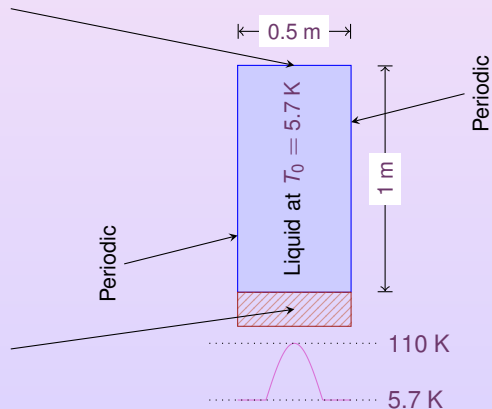
NUCLEATING BUBBLE

Pressure and
temperature
imposed

$$P = P^{\text{ref}} > P^{\text{sat}}(T_0),$$

$$T = T_0$$

Wall,
temperature imposed

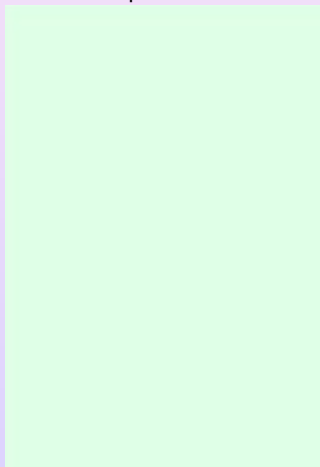


NUCLEATING BUBBLE

Mass Fraction y



Temperature T



◀ Geometry

▶ Play

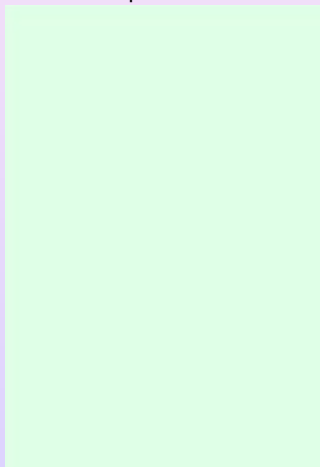
▶▶ Skip

NUCLEATING BUBBLE

Mass Fraction y



Temperature T



◀ Geometry

▶ Play

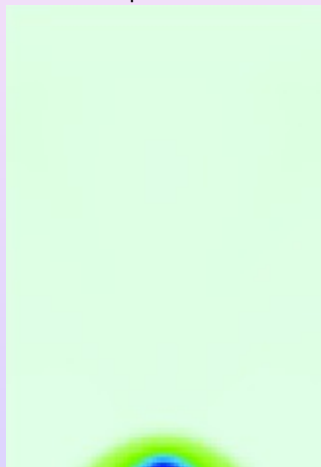
▶▶ Skip

NUCLEATING BUBBLE

Mass Fraction y



Temperature T



◀ Geometry

▶ Play

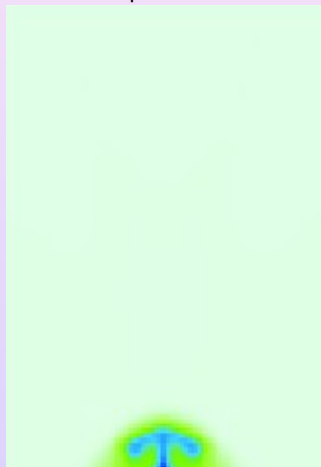
▶▶ Skip

NUCLEATING BUBBLE

Mass Fraction y



Temperature T



◀ Geometry

▶ Play

▶▶ Skip

NUCLEATING BUBBLE

Mass Fraction y



Temperature T



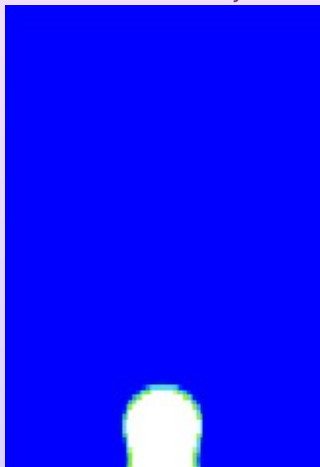
◀ Geometry

▶ Play

▶▶ Skip

NUCLEATING BUBBLE

Mass Fraction y



Temperature T



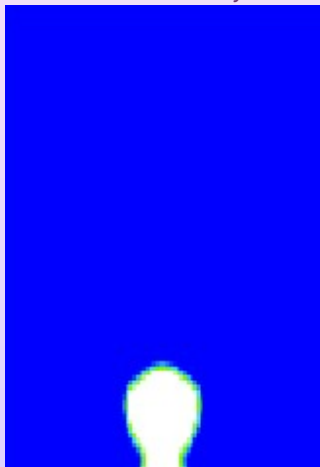
◀ Geometry

▶ Play

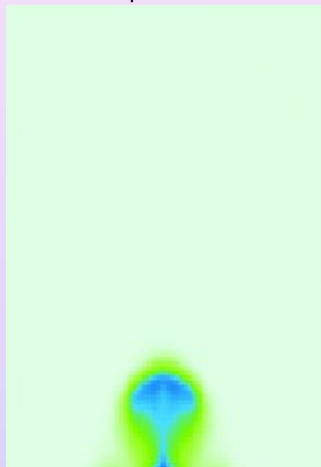
▶▶ Skip

NUCLEATING BUBBLE

Mass Fraction y



Temperature T



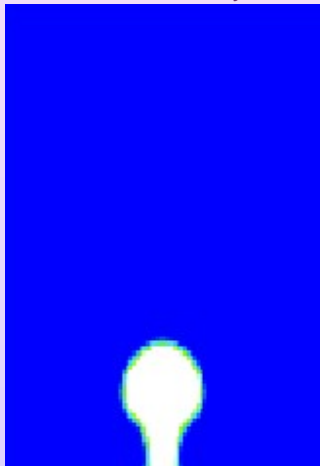
◀ Geometry

▶ Play

▶▶ Skip

NUCLEATING BUBBLE

Mass Fraction y



Temperature T



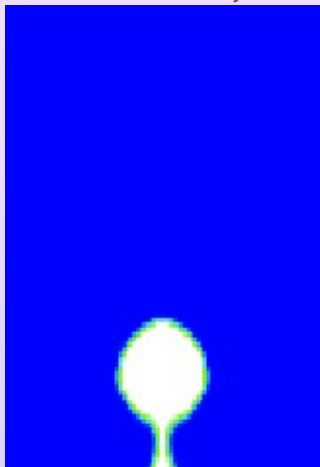
◀ Geometry

▶ Play

▶▶ Skip

NUCLEATING BUBBLE

Mass Fraction y



Temperature T



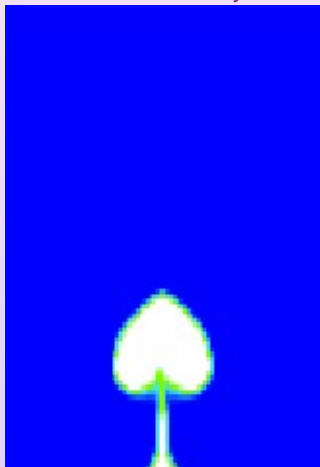
◀ Geometry

▶ Play

▶▶ Skip

NUCLEATING BUBBLE

Mass Fraction y



Temperature T



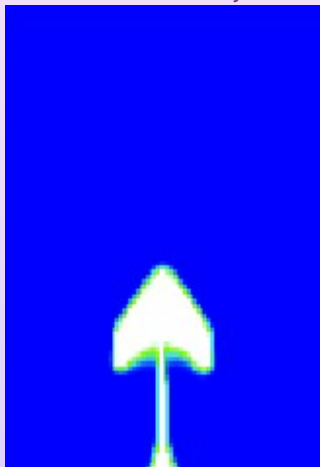
◀ Geometry

▶ Play

▶▶ Skip

NUCLEATING BUBBLE

Mass Fraction y



Temperature T



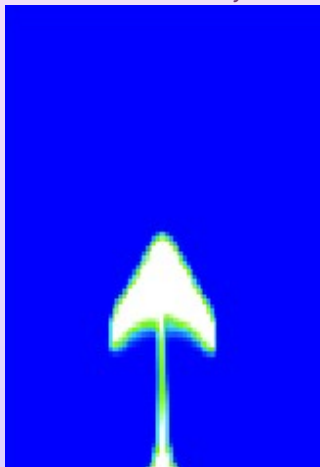
◀ Geometry

▶ Play

▶▶ Skip

NUCLEATING BUBBLE

Mass Fraction y



Temperature T



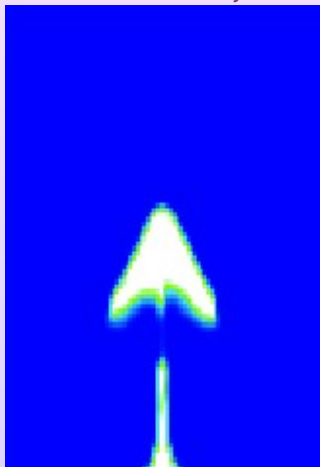
◀ Geometry

▶ Play

▶▶ Skip

NUCLEATING BUBBLE

Mass Fraction y



Temperature T



◀ Geometry

▶ Play

▶▶ Skip

NUCLEATING BUBBLE

Mass Fraction y



Temperature T



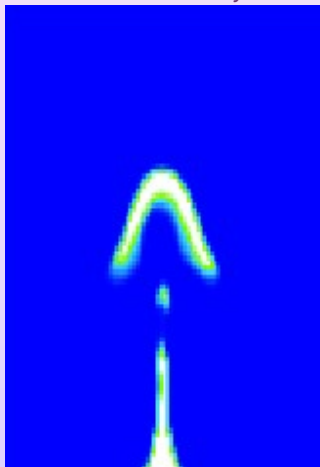
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▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



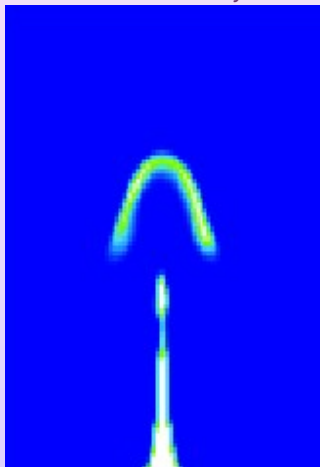
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▶ Play

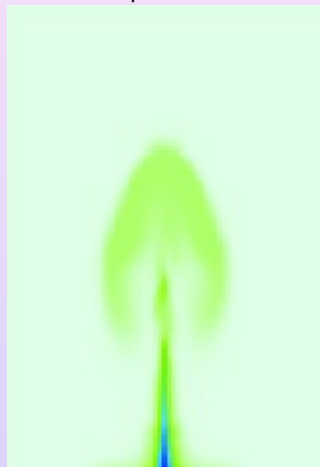
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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



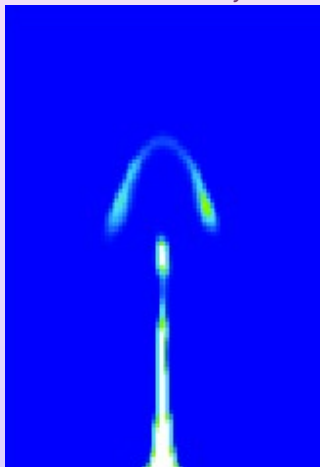
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



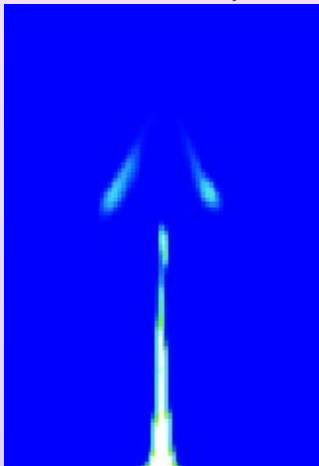
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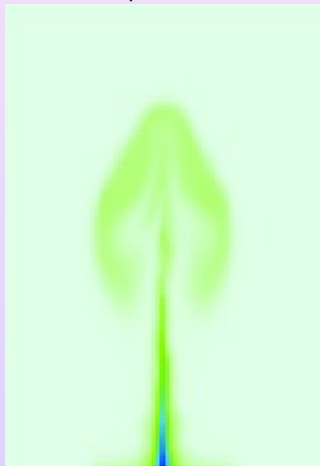
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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



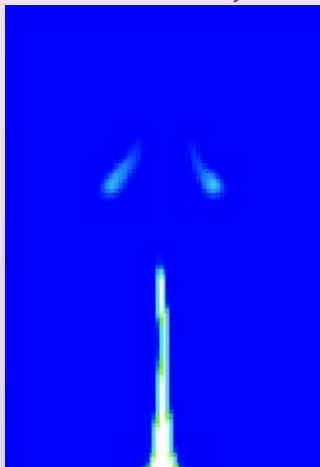
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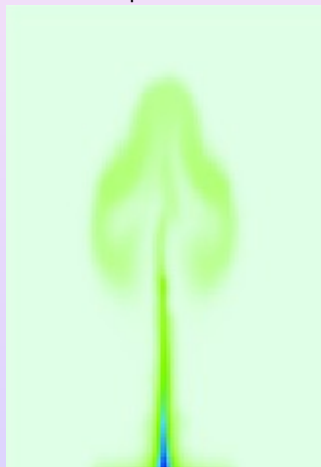
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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



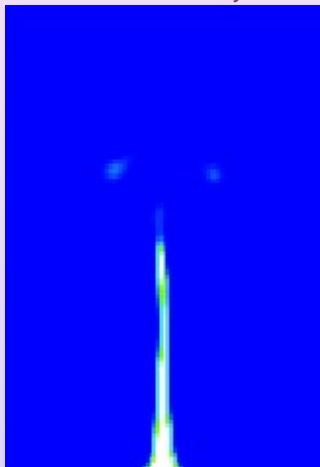
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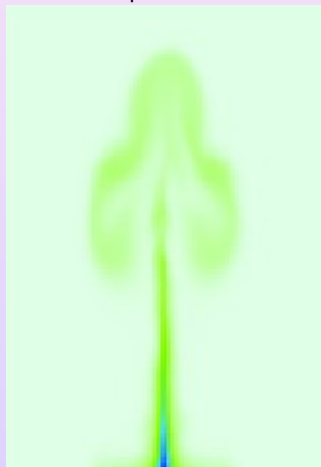
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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



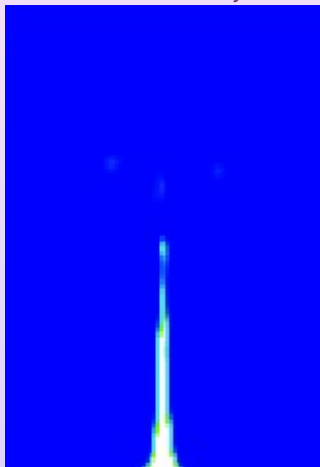
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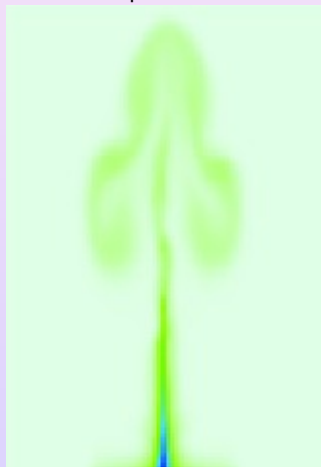
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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



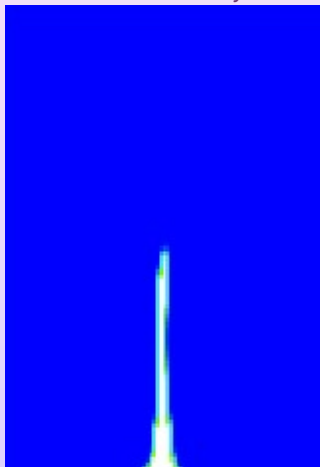
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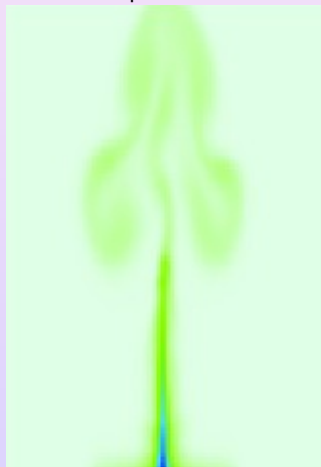
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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



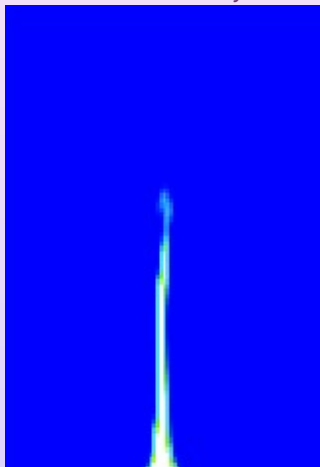
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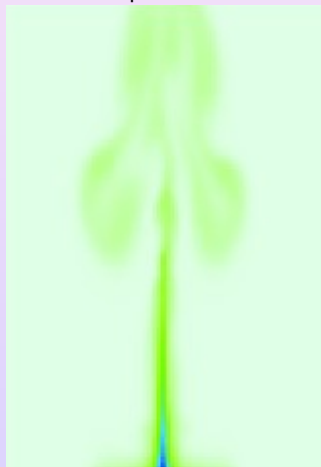
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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



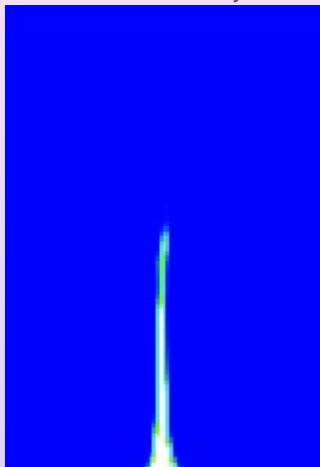
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▶ Play

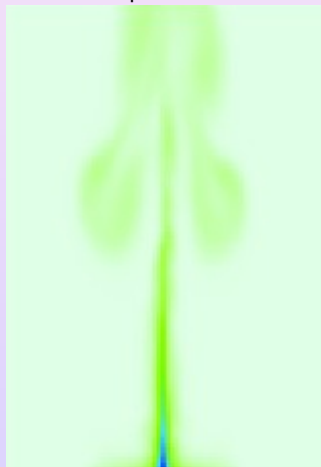
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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



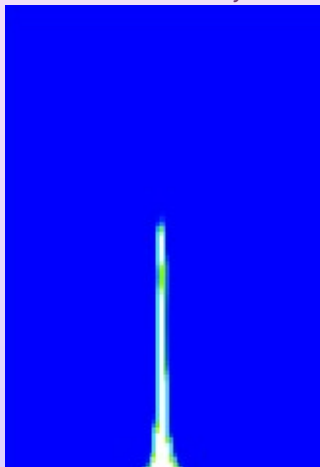
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



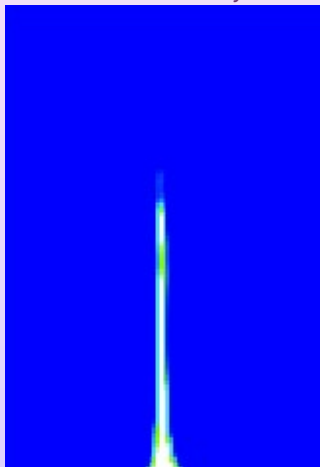
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



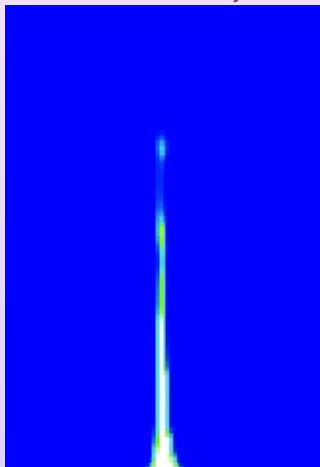
◀ Geometry

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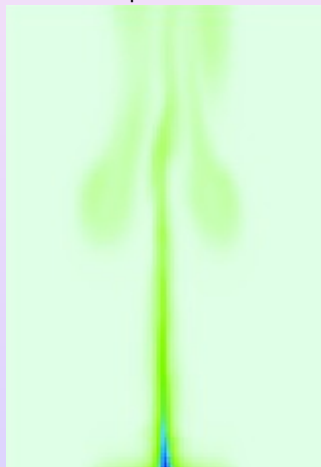
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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



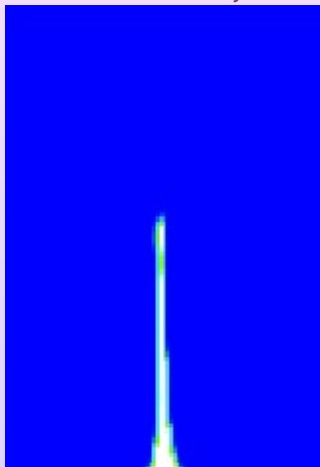
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▶ Play

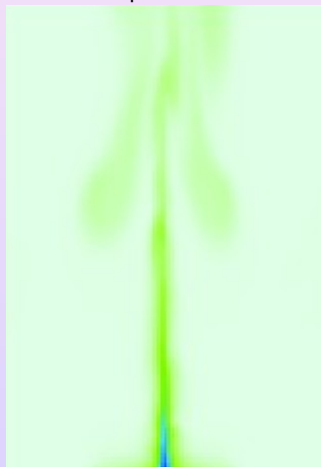
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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



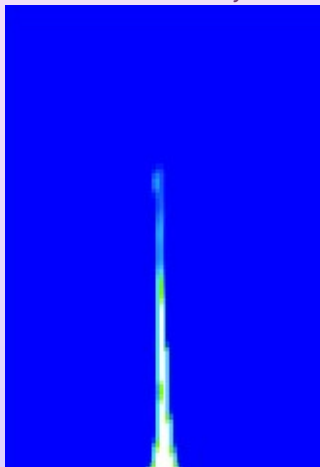
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



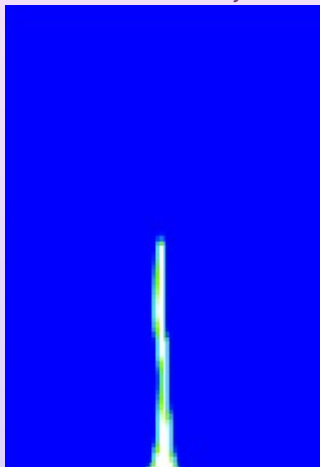
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



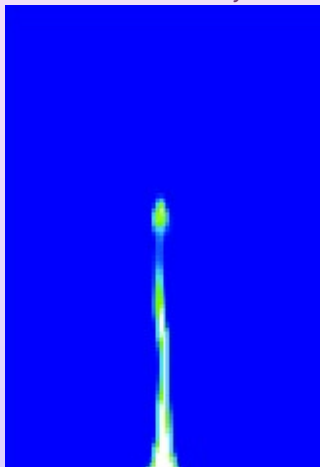
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



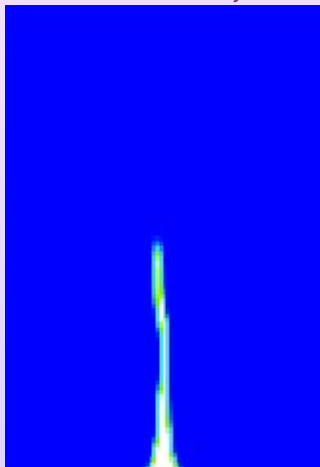
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



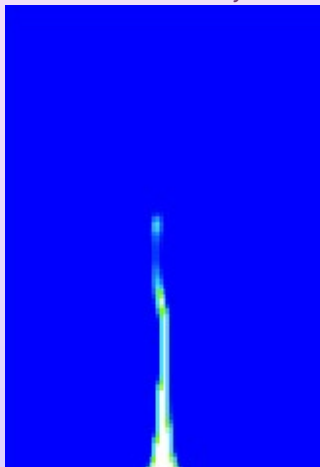
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



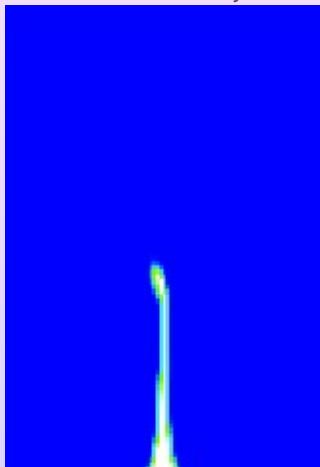
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▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



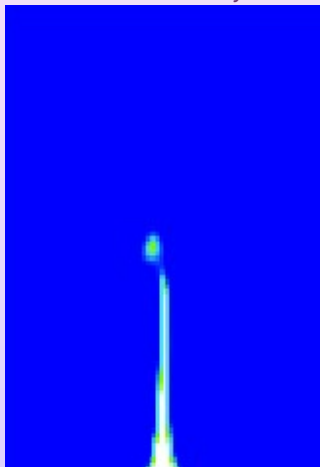
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



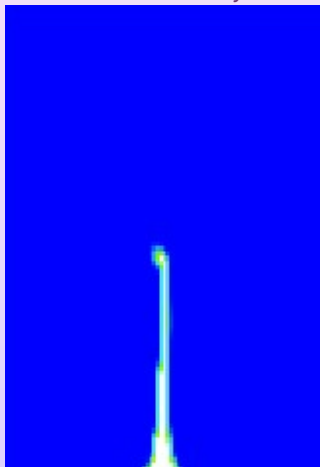
◀ Geometry

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



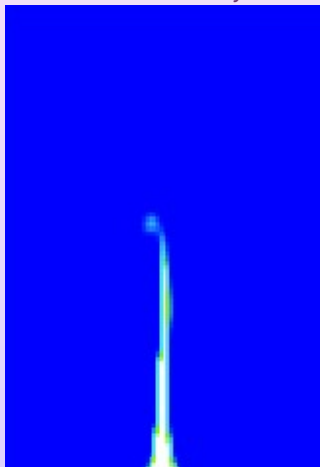
◀ Geometry

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



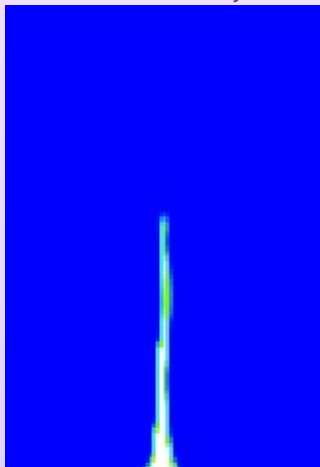
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▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



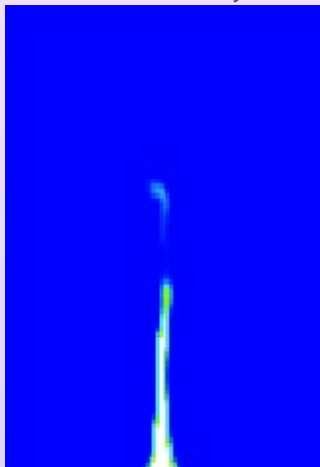
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



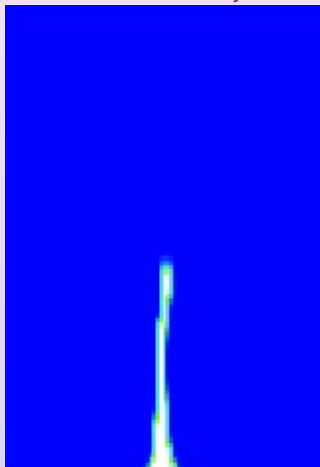
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▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



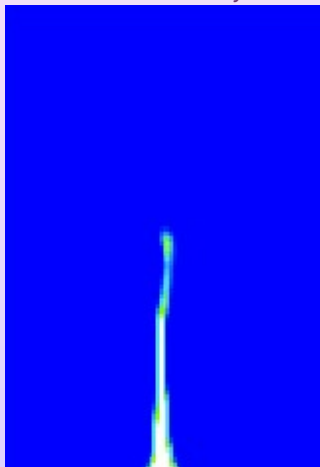
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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



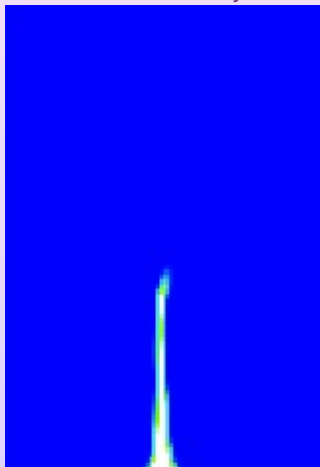
◀ Geometry

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



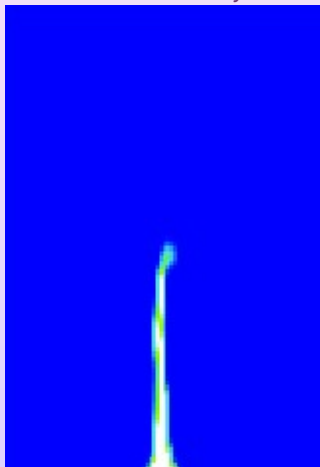
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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



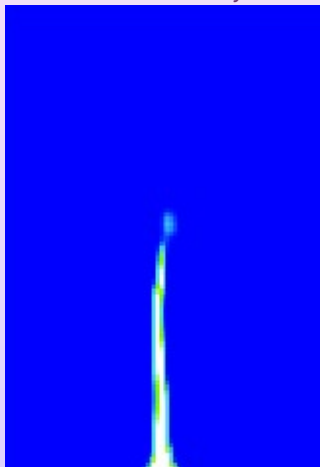
◀ Geometry

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



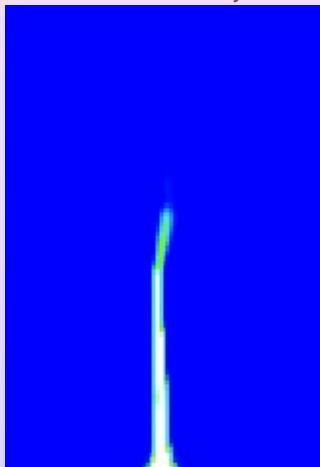
◀ Geometry

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



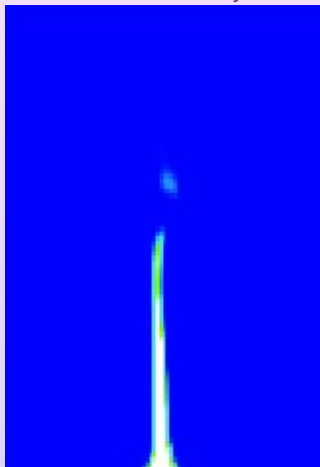
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



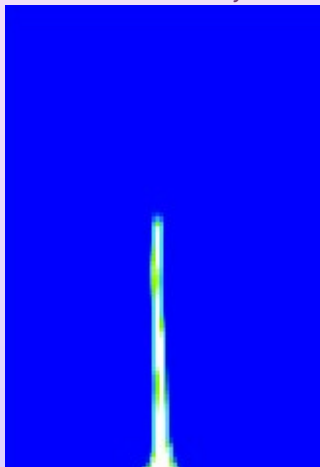
◀ Geometry

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



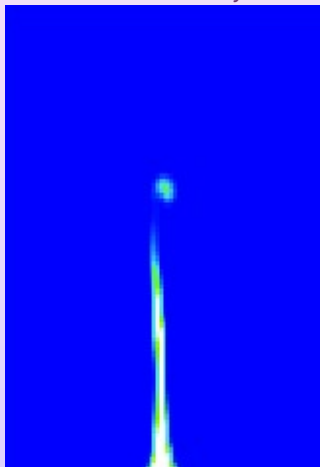
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



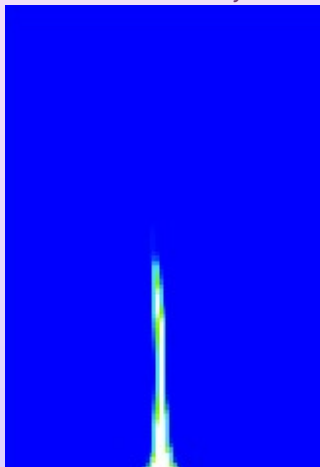
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



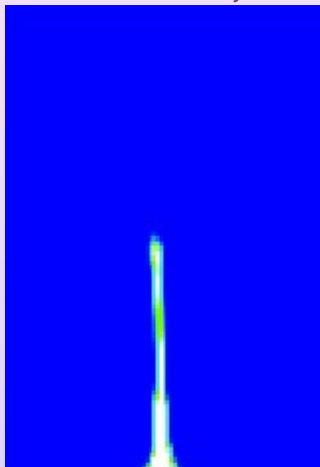
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



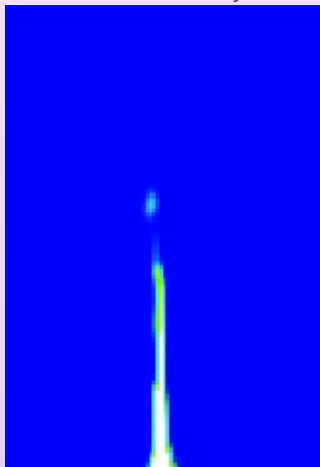
◀ Geometry

▶ Play

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T



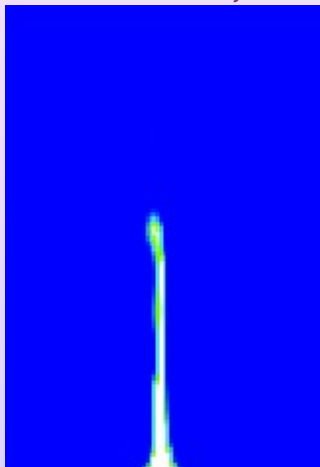
◀ Geometry

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NUCLEATING BUBBLE

Mass Fraction y



Temperature T

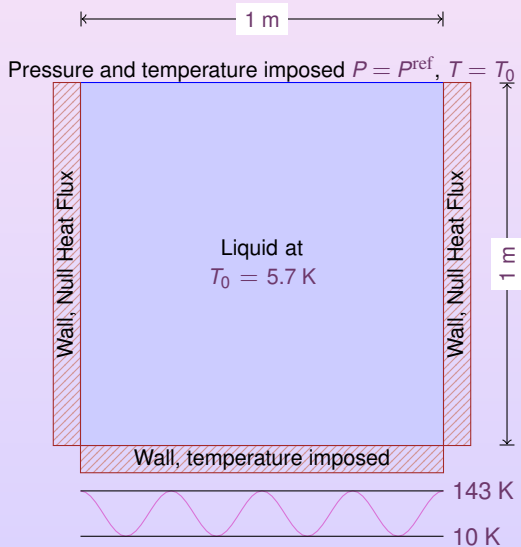


◀ Geometry

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FILM

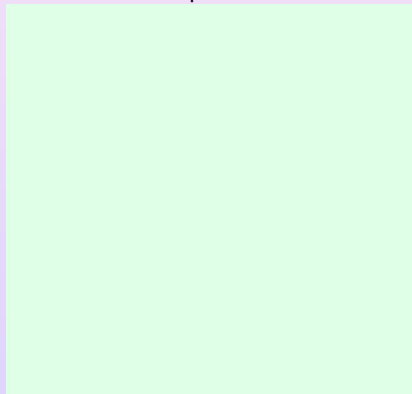


FILM

Mass Fraction y



Temperature T



◀ Geometry

▶ Play

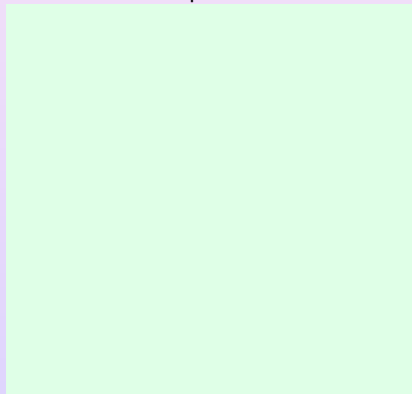
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FILM

Mass Fraction y



Temperature T

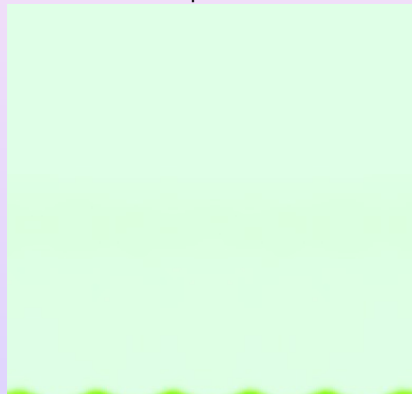


◀ Geometry

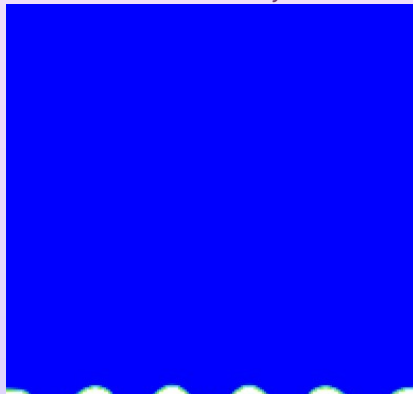
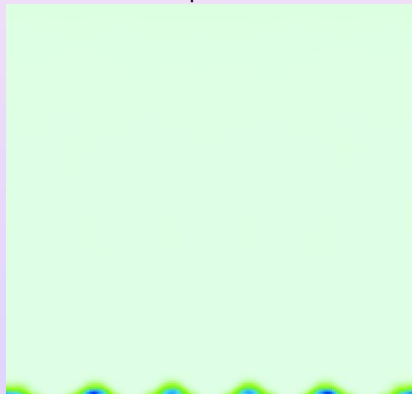
▶ Play

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Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

FILM

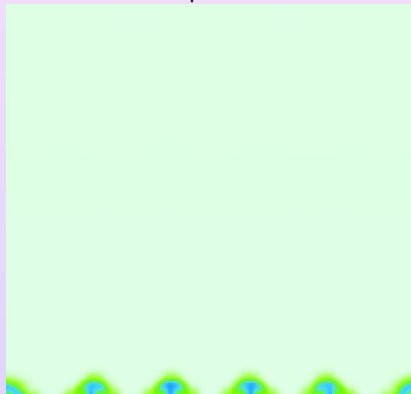
Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

FILM

Mass Fraction y



Temperature T



◀ Geometry

▶ Play

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FILM

Mass Fraction y



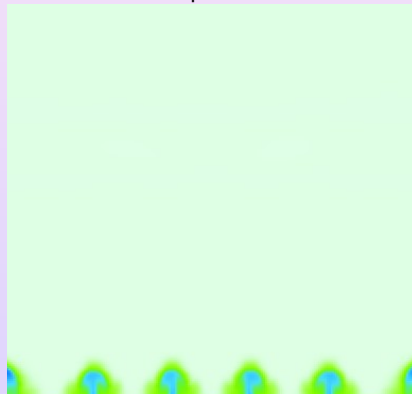
Temperature T



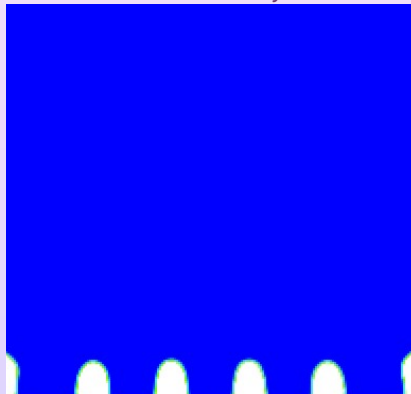
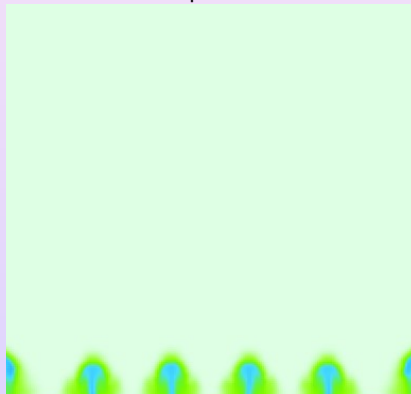
◀ Geometry ▶ Play ▶▶ Skip



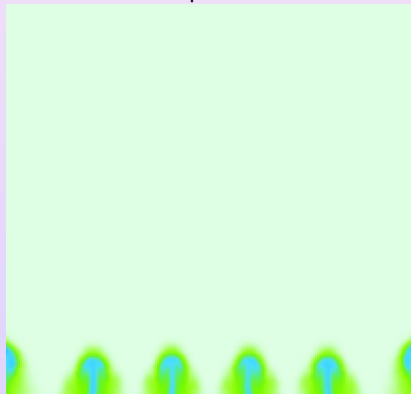
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Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

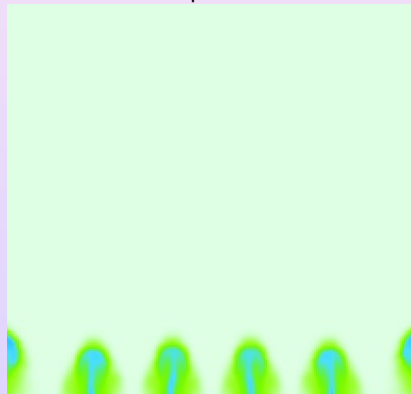
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Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

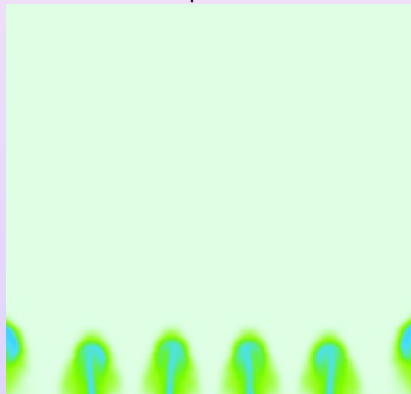
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Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

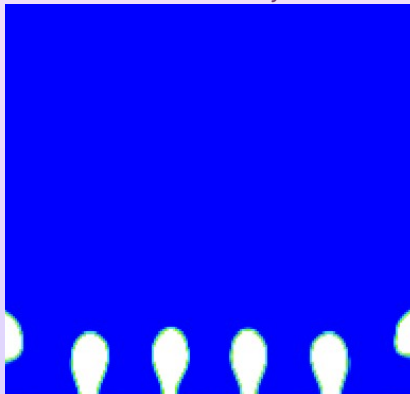
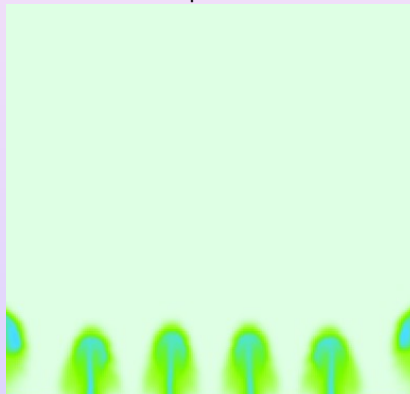
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Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

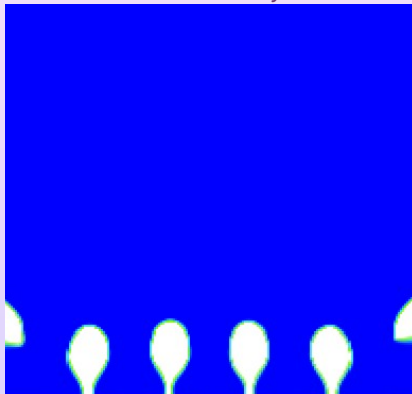
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Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

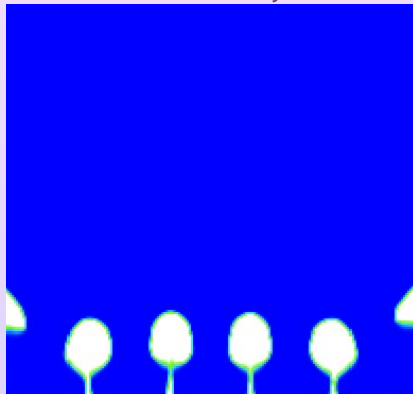
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Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

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Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

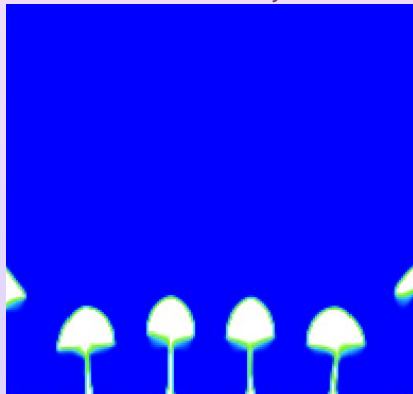
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Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

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Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

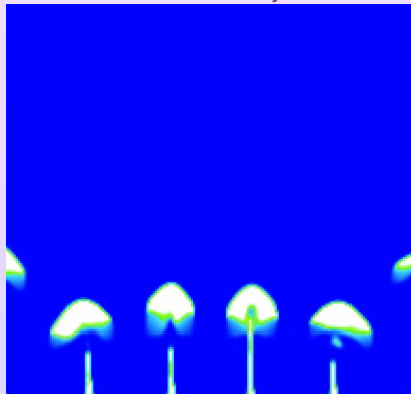
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Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

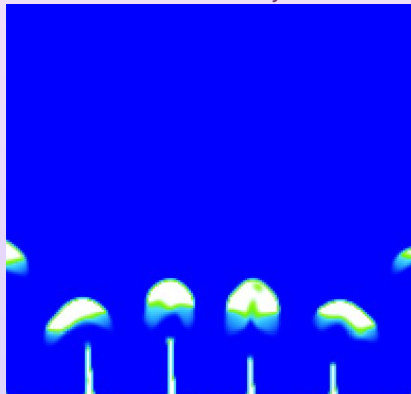
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Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

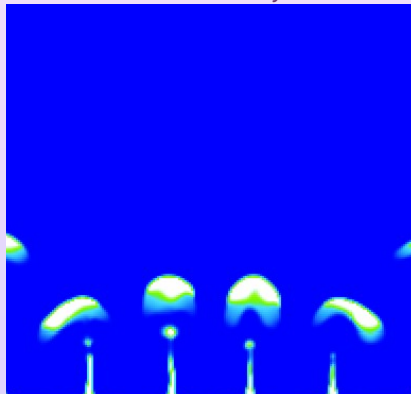
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Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

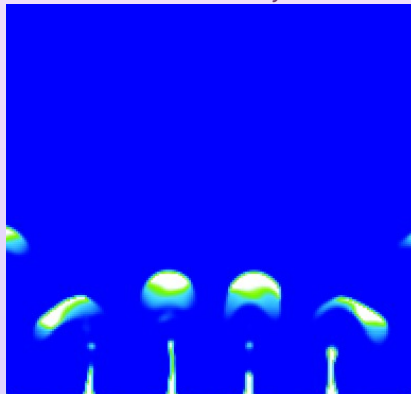
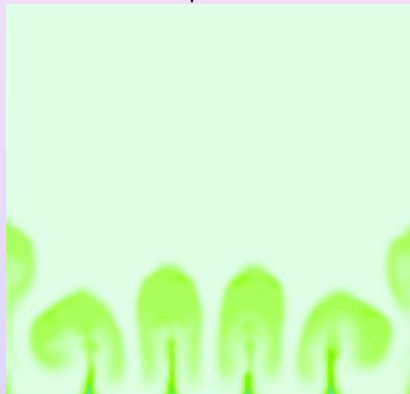
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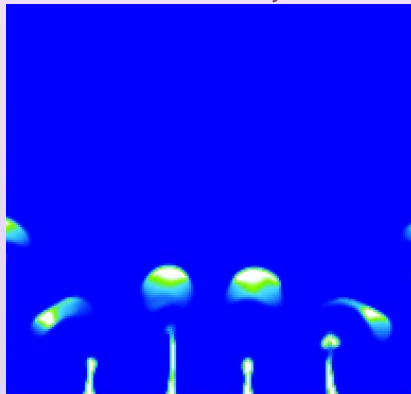
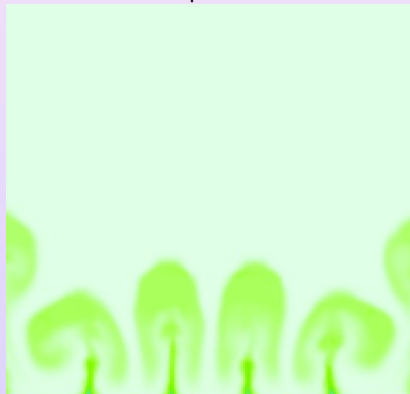
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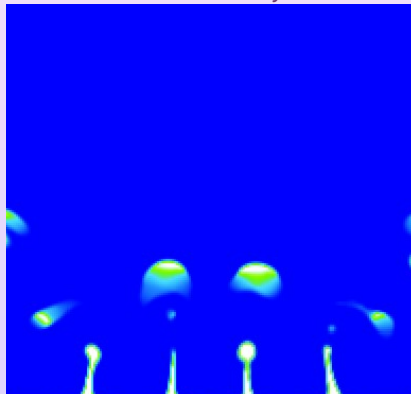
Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

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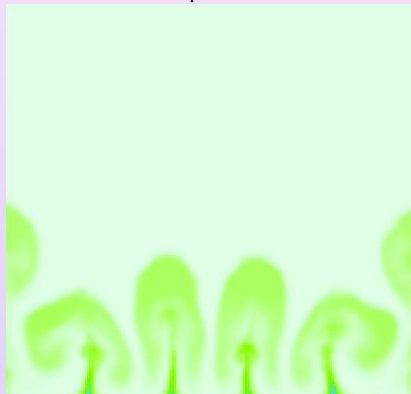
Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

FILM

Mass Fraction y



Temperature T

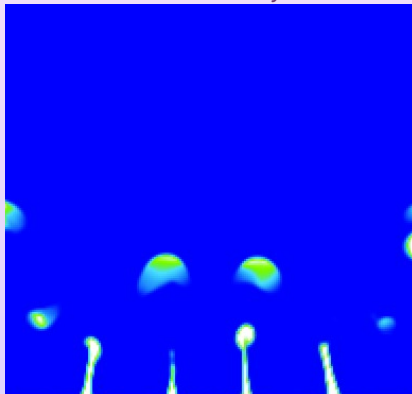
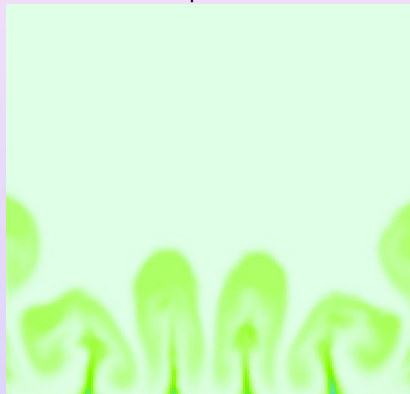


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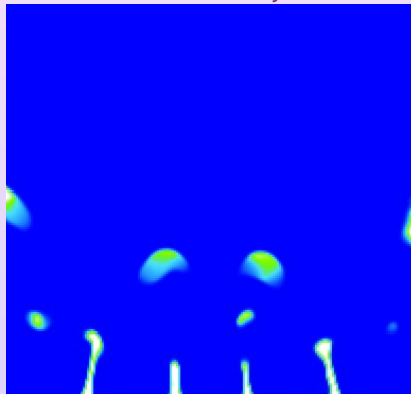
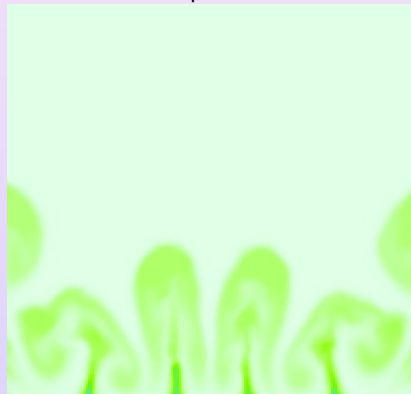
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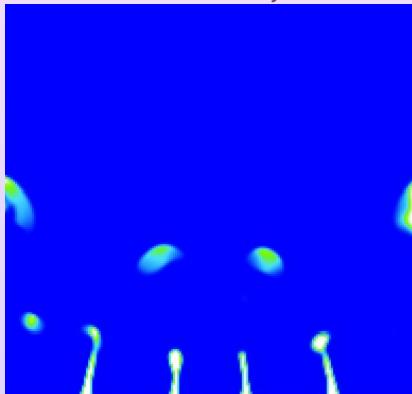
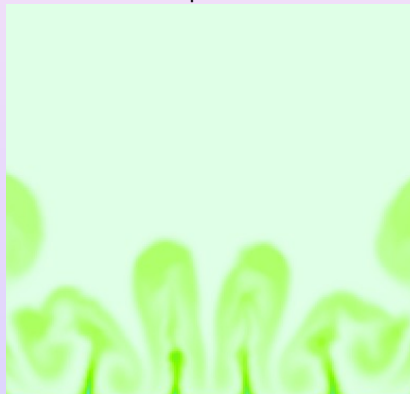
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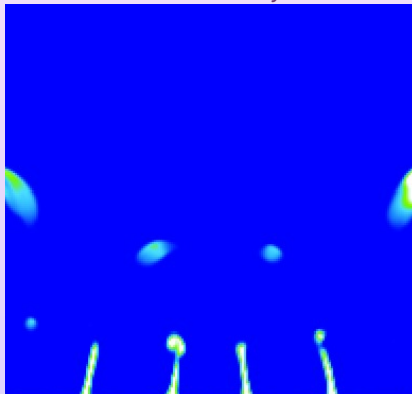
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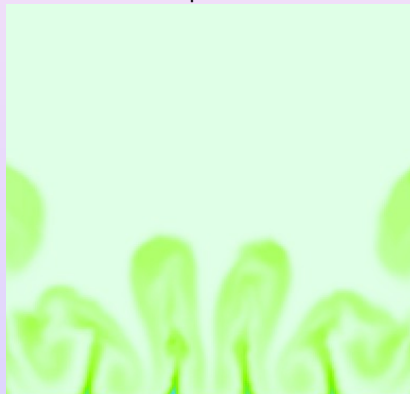
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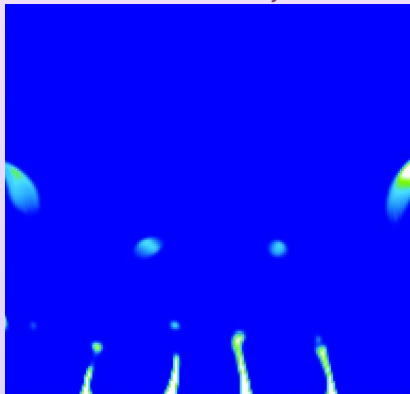
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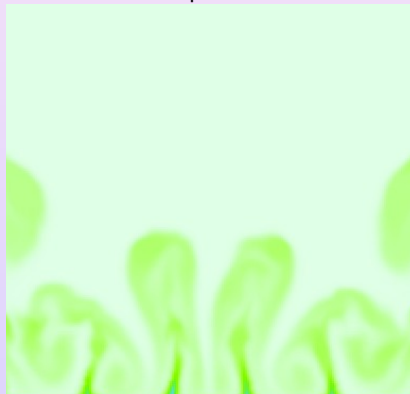
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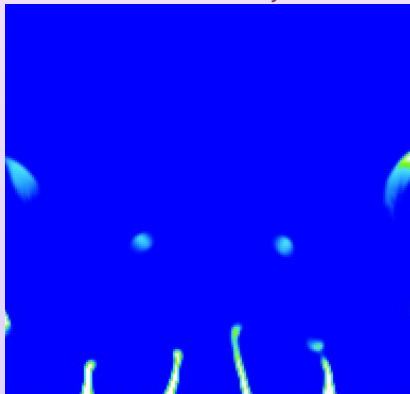
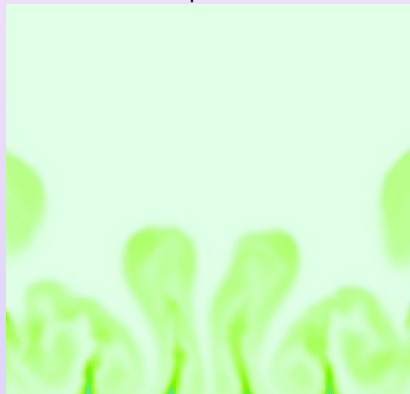


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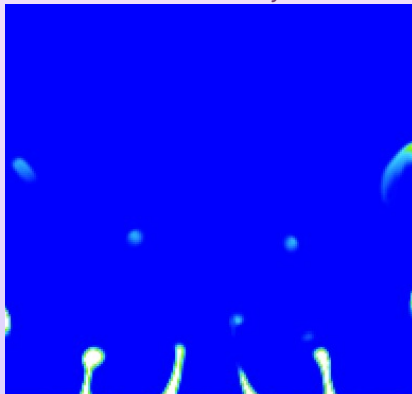
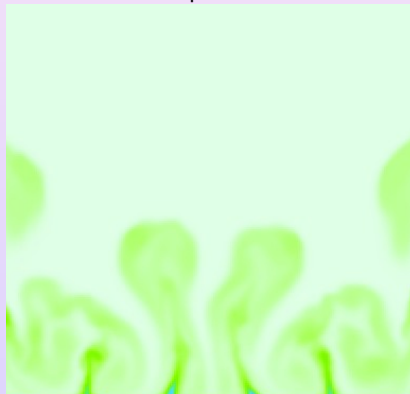
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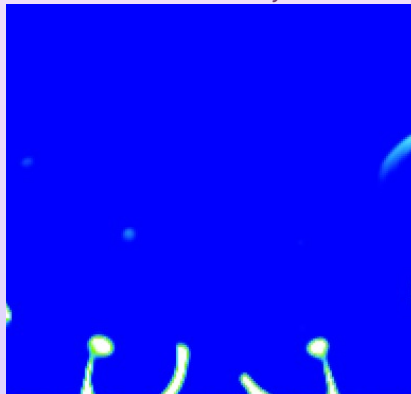
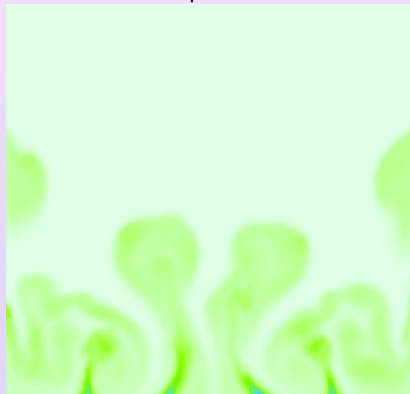
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Mass Fraction y Temperature T [◀ Geometry](#)[▶ Play](#)[▶▶ Skip](#)

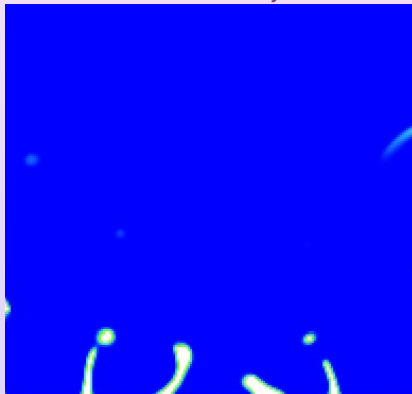
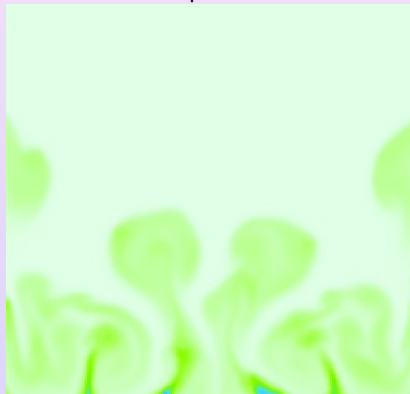
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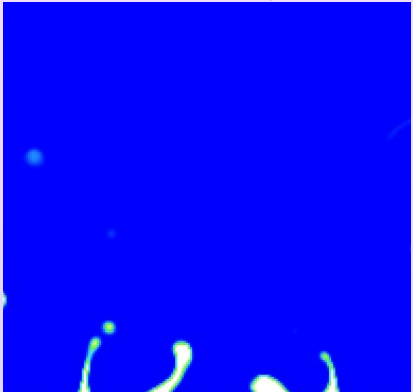
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Mass Fraction y



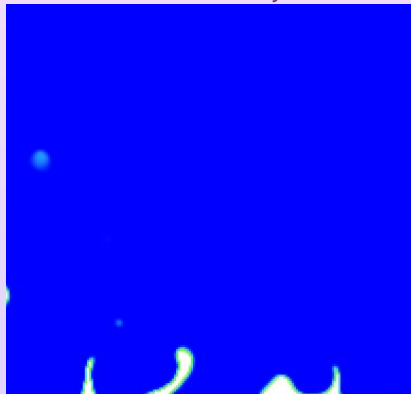
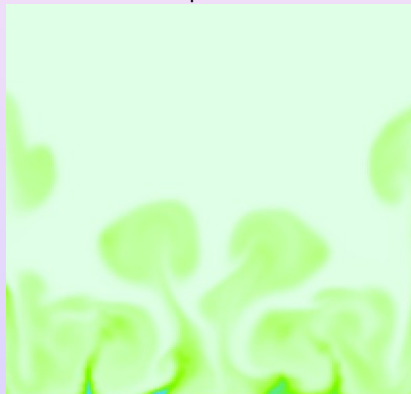
Temperature T



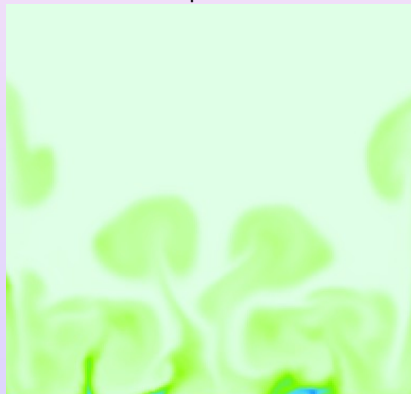
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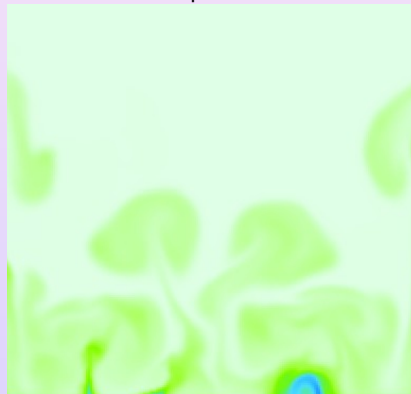
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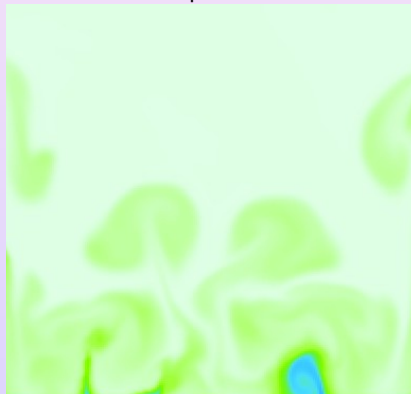
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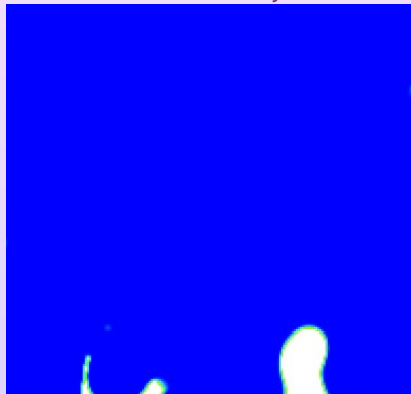
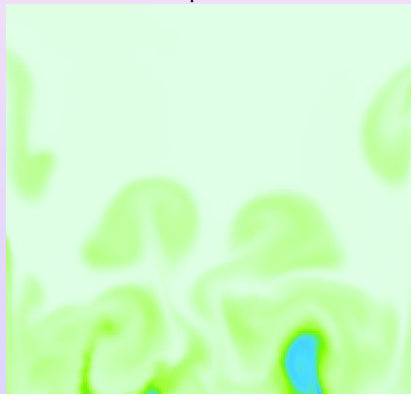
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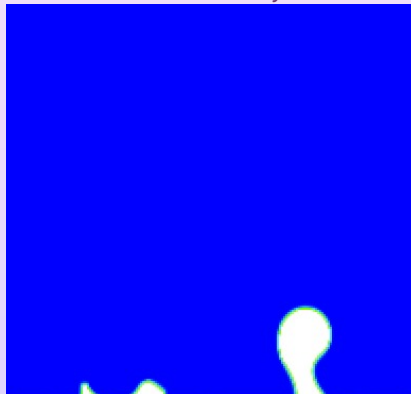
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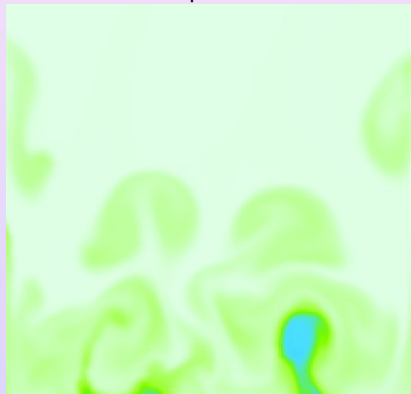
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Mass Fraction y



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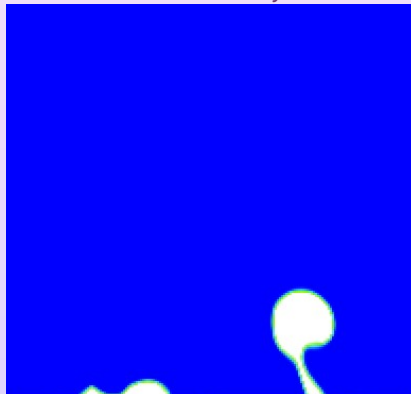
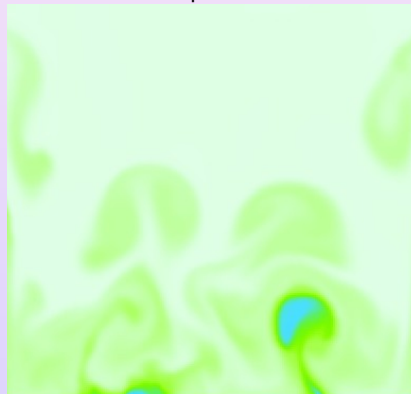


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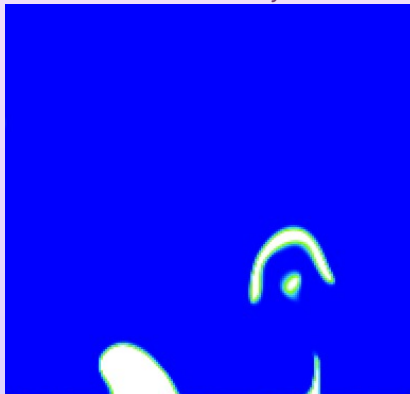
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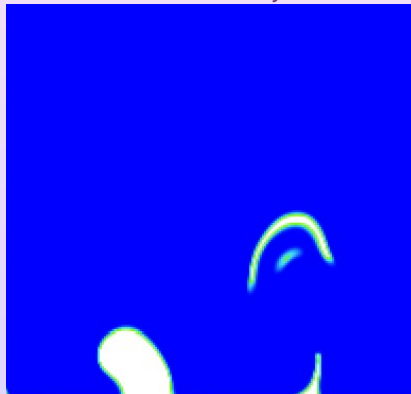
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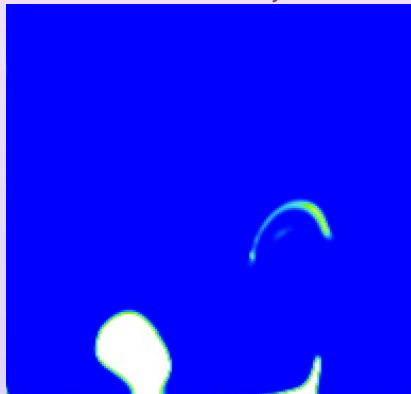
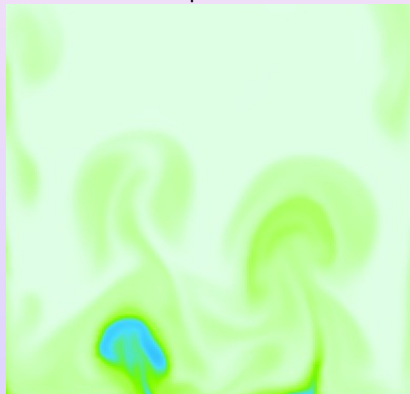
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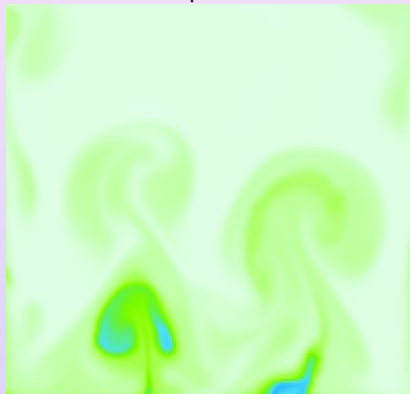
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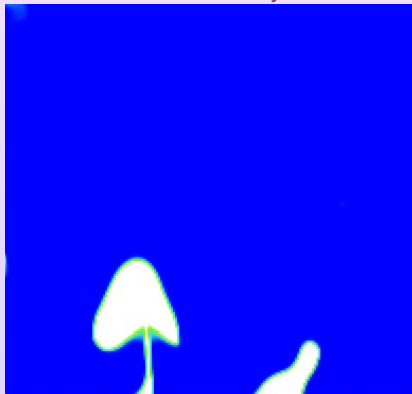
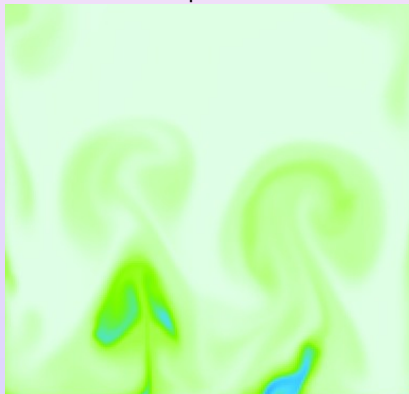


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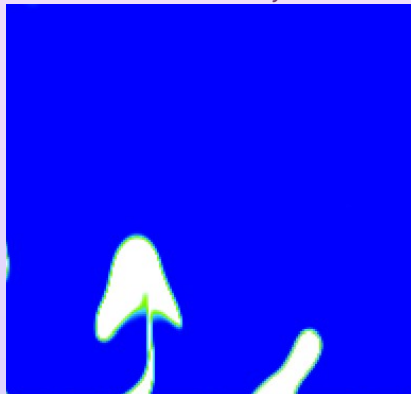
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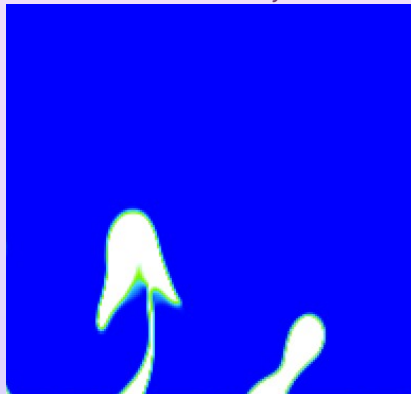
Mass Fraction y Temperature T 

◀ Geometry

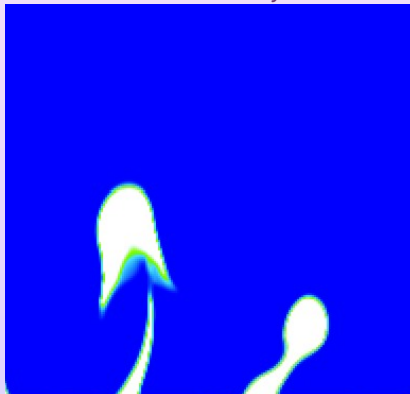
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OUTLINE

1 Context

2 Model

- Equation of state
- Movement Equations

3 Numerical Approximation

- Numerical Method
- Numerical Tests

4 Conclusion



LIQUID-VAPOR PHASE TRANSITION

- **Diffuse Interface Model**

- global EOS always at equilibrium (entropy maximization),
- strict hyperbolicity of the Euler system,
- uniqueness of Liu solution for the Riemann problem;

- Relaxation Approach

- 6 (or 5) equation system with relaxation terms;

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- operator splitting,
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STIFFENED GAS FOR WATER

$$(\tau_\alpha, \varepsilon_\alpha) \mapsto s_\alpha = c_{v\alpha} \ln(\varepsilon_\alpha - q_\alpha - \pi_\alpha \tau_\alpha) + c_{v\alpha} (\gamma_\alpha - 1) \ln \tau_\alpha + m_\alpha$$

Phase	c_v [J/(kg·K)]	γ	π [Pa]	q [J/kg]	m [J/(kg·K)]
Water	1816.2	2.35	10^9	-1167.056×10^3	-32765.55596
Steam	1040.14	1.43	0	2030.255×10^3	-33265.65947

Table: Parameters proposed by [Le Metayer] for water.

$$(P, T) \mapsto \varepsilon_\alpha = c_{v\alpha} T \frac{P + \pi_\alpha \gamma_\alpha}{P + \pi_\alpha} + q_\alpha, \quad (P, T) \mapsto \tau_\alpha = c_{v\alpha} (\gamma_\alpha - 1) \frac{T}{P + \pi_\alpha}.$$

$$\left. \begin{array}{l} T^i = 278\text{K} \dots 610\text{K}, \\ g_1(P, T^i) = g_2(P, T^i) \Rightarrow P^{\text{sat}}(T^i) \end{array} \right\} \Rightarrow \mathfrak{A} = \left\{ (T^i, P^{\text{sat}}(T^i)) \right\}_{i=0}^{83}$$

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$$T \mapsto P^{\text{sat}}(T) \approx \hat{P}^{\text{sat}}(T) \stackrel{\text{def}}{=} \exp \left(\sum_{k=-8}^{k=8} a_k T^k \right)$$

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WATER TABULATED EOS

T (K)	P^{sat} (MPa)	Volume (m^3/kg)		Internal Energy (kJ/kg)	
		$\tau_{\text{liq}}^{\text{sat}}$	$\tau_{\text{vap}}^{\text{sat}}$	$\epsilon_{\text{liq}}^{\text{sat}}$	$\epsilon_{\text{vap}}^{\text{sat}}$
275	0,00069845	0,0010001	181,60	7,7590	2377,5
278	0,00086349	0,0010001	148,48	20,388	2381,6
281	0,0010621	0,0010002	122,01	32,996	2385,7
284	0,0012999	0,0010004	100,74	45,586	2389,8
287	0,0015835	0,0010008	83,560	58,162	2393,9
290	0,0019200	0,0010012	69,625	70,727	2398,0
293	0,0023177	0,0010018	58,267	83,284	2402,1
296	0,0027856	0,0010025	48,966	95,835	2406,2
299	0,0033342	0,0010032	41,318	108,38	2410,3
302	0,0039745	0,0010041	35,002	120,92	2414,4
305	0,0047193	0,0010050	29,764	133,46	2418,4
308	0,0055825	0,0010060	25,403	146	2422,5
...

Source: <http://webbook.nist.gov/chemistry/fluid/>

WATER TABULATED EOS

$$\left. \begin{array}{l} T^i = 278\text{K} \dots 610\text{K}, \\ \epsilon_{\alpha}^{\text{sat}}(T^i), \tau_{\alpha}^{\text{sat}}(T^i) \text{ found in the tables} \end{array} \right\} \Rightarrow \left\{ \begin{array}{l} \mathfrak{A} = \left\{ \left(T_i, \frac{1}{\epsilon_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{B} = \left\{ \left(T_i, \frac{\epsilon_{\text{liq}}^{\text{sat}}(T_i)}{\epsilon_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{C} = \left\{ \left(T_i, \frac{1}{\tau_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \\ \mathfrak{D} = \left\{ \left(T_i, \frac{\tau_{\text{liq}}^{\text{sat}}(T_i)}{\tau_{\text{vap}}^{\text{sat}}(T_i)} \right) \right\}_i \end{array} \right.$$

$\widehat{\epsilon}_{\alpha}^{\text{sat}}$ and $\widehat{\tau}_{\alpha}^{\text{sat}}$ defined by using a least square approximation of \mathfrak{A} , \mathfrak{B} , \mathfrak{C} and \mathfrak{D} :

$$T \mapsto \epsilon_{\text{vap}}^{\text{sat}} \approx \widehat{\epsilon}_{\text{vap}}^{\text{sat}} \stackrel{\text{def}}{=} \frac{1}{\sum_{k=0}^6 a_k T^k}$$

$$T \mapsto \epsilon_{\text{liq}}^{\text{sat}} \approx \widehat{\epsilon}_{\text{liq}}^{\text{sat}} \stackrel{\text{def}}{=} \widehat{\epsilon}_{\text{vap}}^{\text{sat}}(T) \sum_{k=0}^6 b_k T^k$$

$$T \mapsto \tau_{\text{vap}}^{\text{sat}} \approx \widehat{\tau}_{\text{vap}}^{\text{sat}} \stackrel{\text{def}}{=} \frac{1}{\sum_{k=0}^8 c_k T^k}$$

$$T \mapsto \tau_{\text{liq}}^{\text{sat}} \approx \widehat{\tau}_{\text{liq}}^{\text{sat}} \stackrel{\text{def}}{=} \widehat{\tau}_{\text{vap}}^{\text{sat}}(T) \sum_{k=0}^9 d_k T^k$$

SPEED OF SOUND

$$c^2 \stackrel{\text{def}}{=} \tau^2 \left(P^{\text{eq}} \frac{\partial P^{\text{eq}}}{\partial \varepsilon} \Big|_{\tau} - \frac{\partial P^{\text{eq}}}{\partial \tau} \Big|_{\varepsilon} \right) = \overset{0}{-\tau^2 T^{\text{eq}}} \begin{bmatrix} P^{\text{eq}}, & -1 \end{bmatrix} \begin{bmatrix} S_{\varepsilon\varepsilon}^{\text{eq}} & S_{\tau\varepsilon}^{\text{eq}} \\ S_{\tau\varepsilon}^{\text{eq}} & S_{\tau\tau}^{\text{eq}} \end{bmatrix} \begin{bmatrix} P^{\text{eq}} \\ -1 \end{bmatrix} \leq 0$$

HESSIAN MATRIX OF $\mathbf{w} \mapsto s^{\text{eq}}$

- for all \mathbf{w} pure phase state

$$\mathbf{v}^T d^2 s^{\text{eq}}(\mathbf{w}) \mathbf{v} < 0 \quad \forall \mathbf{v} \neq 0,$$

- for all \mathbf{w} equilibrium mixture state

$$\exists \mathbf{v}(\mathbf{w}) \neq 0 \text{ s.t. } (\mathbf{v}(\mathbf{w}))^T d^2 s^{\text{eq}}(\mathbf{w}) \mathbf{v}(\mathbf{w}) = 0.$$

SPEED OF SOUND

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SPEED OF SOUND

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$$\forall \mathbf{w} \text{ equilibrium mixture state, } \mathbf{v}(\mathbf{w}) \stackrel{?}{\not\propto} [P^{\text{eq}}(\mathbf{w}), -1]$$

ISENTROPIC CURVES

